

# Studying the Effects of Solution Processing Conditions on Morphology of Studtite and $UO_3$

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## Summary

Nuclear forensic signatures are useful in the determination of origin and processing conditions of illicitly trafficked nuclear materials. In this investigation,  $UO_3$  was examined (as a product of heating studtite starting material  $[(UO_2)(O_2)(H_2O)_2] \cdot 2H_2O$ ). Based on previous screening experiments, relationships and interactions between processing variables were studied for their effects on the characteristics of studtite and  $UO_3$  powder.

## Background and Aims

### Screening Experiments

Initial screening experiments helped to establish the processing conditions that may affect the physical and chemical properties of  $UO_3$  product. A potential relationship between solution concentration and powder morphology (shape and form) was found, leading to further investigation by a fractional factorial matrix.

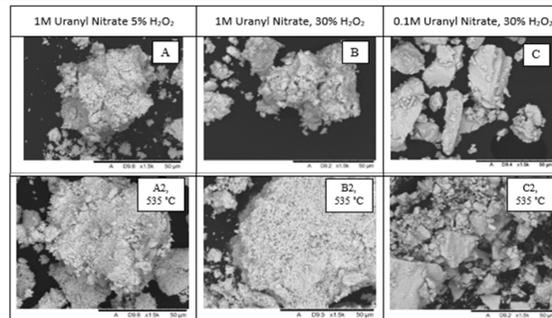
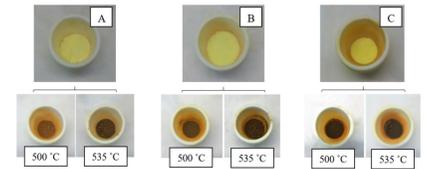


Figure 1:  $UO_3$  powders produced from studtite (A-C) samples.

### Aims

To further establish the relationships that exist between solution processing parameters (e.g. concentration, strike order, etc) and finished  $UO_3$  powder morphology.



## Material Preparation

### Studtite and $UO_3$ powder synthesis

Synthetic studtite was prepared by mixing aqueous uranyl nitrate (0.1 and 1 M) and hydrogen peroxide ( $H_2O_2$ , 5 and 30 w/w%) via forward ( $H_2O_2$  added to U nitrate) or reverse addition (U nitrate added to  $H_2O_2$ ). All mixing was performed robotically by a Metrohm Titrosampler, filtered under vacuum and dried for 48 hours.  $UO_3$  was obtained directly by heating studtite powder to 535 °C in nitrogen ( $N_2$ ) at 10 °C/min.

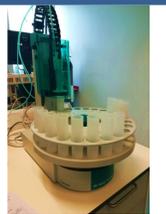


Figure 2: Metrohm Titrosampler

## Factorial Matrix and Images

### Design of Experiments

To test for relationships and/or interactions between effects of processing variables, a  $2^{4-1}$  fractional factorial experiment was used, requiring a total of 8 experimental runs.

Conc. U Nitrate (M)	Conc. $H_2O_2$ (w/w%)	Strike	Washing
0.1	5	Forward	W
0.1	5	Reverse	UnW
0.1	30	Forward	UnW
0.1	30	Reverse	W
1	5	Forward	UnW
1	5	Reverse	W
1	30	Forward	W
1	30	Reverse	UnW

### Scanning Electron Microscopy (SEM)

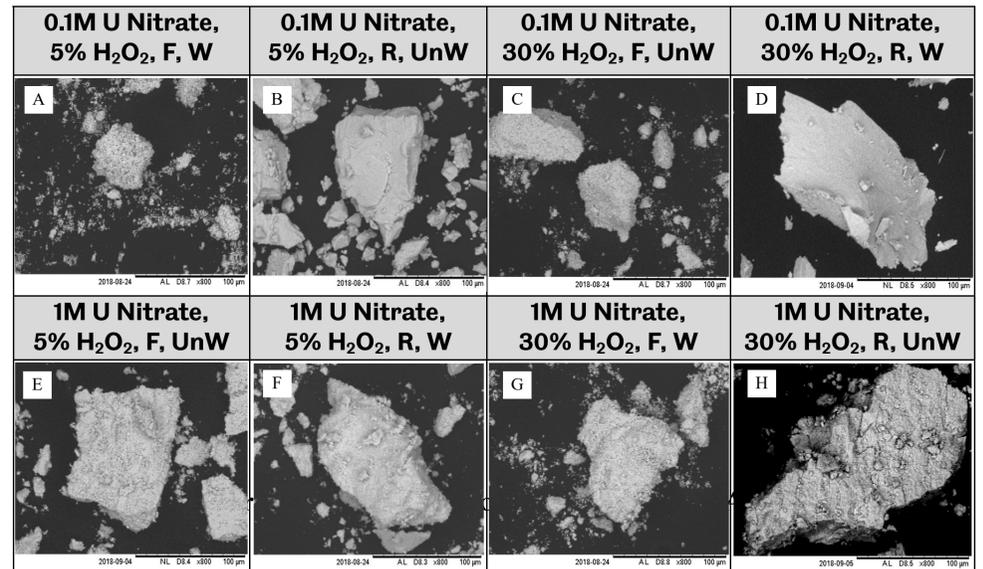


Figure 3: SEM images of ground studtite precipitates (R=Reverse, UnW=Unwashed)

## Particle Morphology Discussion

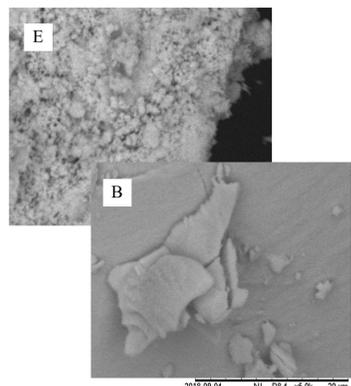


Figure 4: Samples E and B at 20  $\mu m$  scale

Particles generally appeared faceted and angular when produced by reverse-strike addition, particularly at low U nitrate concentrations.

**Reverse-strike** precipitation will occur with slower growth rate than forward, due to immediate excess dilution in  $H_2O_2$ . Washing appears to make little difference to morphology.

**Forward-strike** samples appeared rounded and clumped when either i) nitrate:peroxide concentration levels were equal and ii) washing had occurred after precipitation. Further work will be considered to discern the main effect contributing to these observations.

## $UO_3$ Morphology

Heating studtite to 535 °C in  $N_2$  at a rate of 10 °C/min appeared to have no effect on the particle morphology. This result may prove relevant to nuclear forensic applications, where

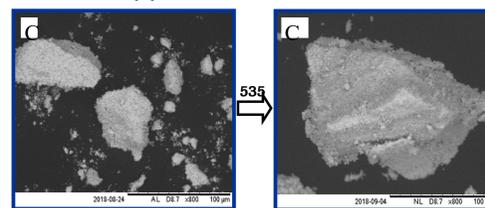


Figure 6: 0.1M 30% R, W at RT (C) and 535 °C (C1)

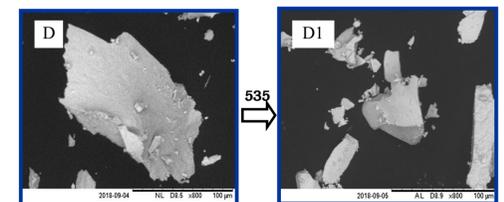


Figure 5: 0.1M 30% F UnW at RT (D) and 535 °C (D1)

a sample of  $UO_3$  (or other thermal product of studtite) may be traced to its starting material using the  $UO_3$  morphology, compared to a set of known standards.

## Conclusion

Initial screening experiments demonstrated that it is possible to obtain different morphologies of studtite, and therefore  $UO_3$ , from different solution processing conditions. By running a  $2^{4-1}$  fractional factorial matrix, it was found that the morphology of studtite and its heat products are affected by a combination of concentration, concentration ratio and strike order of reagent during the studtite precipitation stages.

## Acknowledgements

Special thanks go to project supervisors Professor Neil C. Hyatt and Dr. Matthew Gilbert (AWE). Additionally to Dr. Martin C. Stennett and all group members of the Sheffield ISL. This research was performed in part at the MIDAS Facility, at the University of Sheffield, which was established with support from the Department of Energy and Climate Change.