

Supporting Information

N-Nitrosodimethylamine (NDMA) Degradation by the UV/peroxodisulfate Process

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Text S1. Method for N-nitrosodimethylamine determination in aqueous solution

The procedure for NDMA analysis ¹ was modified from the headspace method proposed by Grebel et al. (2006) ². GC-QqQ analysis was performed by Trace GC Ultra gas chromatograph equipped with a TriPlusTM autosampler coupled to a TSQ Quantum triple quadrupole mass spectrometer system (Thermo Fisher Scientific). 5 mL of the sample were placed in an amber vial containing 1.8 g of sodium chloride. Finally 100 µL of d₆NDMA 10 µg/L were added as internal standard. Carboxen/polydimethylsiloxane (CAR/PDMS) fibres from Supelco were selected for the extraction. The fibres were first conditioned to remove contaminants in the GC inlet prior to use as recommended by the manufacturer. Extraction was achieved by heating up and stirring the sample at 80°C during 45 min. The fibre was exposed to the head-space generated in the sample vial. Once extraction and pre-concentration steps were achieved, the fibre was pulled out of the sample vial and injected into the GC. Desorption was conducted at 250°C during 4 minutes. Blanks were run periodically during the analysis to confirm the absence of carry over. Chromatographic separation was performed using a Trace GOLD TG-5SILMS from Thermo Fisher Scientific (30m x 0.25mm x 0.25µm). The injector was operated in splitless mode. The oven temperature program was as follows: 50°C hold for 3 minutes, ramp to 180°C at 25°C/min, hold for 0.5 minutes, ramp to 230°C at 40°C/min, and finally hold for 1 minute. The limit of quantification (LOQ) was 20 ng/L, which allows a good observation of the degradation kinetics, which were carried out with an initial concentration of 500 ng/L.

The peak area of a standard prepared at 1000 ng/L in dichloromethane and injected directly was compared to the peak area of a standard prepared at 1000 ng/L in water and extracted with SPME. We observed that the area of the standard extracted with SPME was 100 times higher than the standard prepared in dichloromethane and injected directly, meaning that there is a factor of 100 enrichment during SPME. When calculating the recovery using quality control standards and using the calibration curve, we observed recoveries between 90-95%.

Mass spectrometric ionization was carried out in electron impact (EI) ionization mode with and EI voltage of 70 eV and a source temperature of 250°C. Detection was performed in Selected Reaction Monitoring (SRM) mode. NDMA was monitored by using the m/z 74 parent ion and 42 and 43 daughter ions as quantification and qualification transitions, respectively. The internal standard d₆NDMA was quantified by using the m/z 80 parent ion and 46 daughter ion. Acquired data were processed by TracerFinder EFS 3.1 software.

Text S2. Evaluation of fluence and fluence-based rate constants

The UV-fluence and the incident photon irradiance of the polychromatic lamp were determined as previously described by Bolton et. al.³ in the range of **200-300 nm**. This range was considered due as it contains the main absorption band of NDMA (peak at 227 nm). The value of average fluence rate was determined experimentally from the incident photon irradiance in the centre of the reactor and correction factors such as Petri Factor (PF), Reflection Factor (RF), and Water Factor (WF)³.

The data of the **lamp irradiance** (W cm^{-2}) that was applied to determine the different parameters was taken at the center of the beam at the water surface. In addition, radiometer measurements were taken across the surface area at the level of the water surface in the Petri dish in a manner that allows the calculation of the average irradiance over that surface area. With these results, the **PF** was calculated by dividing the average irradiance across the water surface by the measure in the center of the Petri dish. The PF value was 0.97 and the incident photon irradiance was 4.16 W m^{-2} . The **WF** represents the absorbance of the water and is calculated from an integration of Beer's Law from the top to the bottom of the solution³. The applied data of **RF** for water at a given wavelength was taken from the bibliography^{3, 4}. Analyzing the photon fluence-degradation of NDMA, an additional factor is required as a **NDMA-factor**, which defined the photolysis effectiveness of photons of a certain wavelength relative to those at 254 nm. With these data, the **average photon irradiance** and the **equivalent average irradiance** at 254 nm were calculated for each experiment using the Excel spreadsheet provided in their supplementary information by Bolton et. al.³. The evaluation of **UV fluence** (J m^{-2}) was done by multiplying the exposure time (second) by the equivalent average irradiance at 254 nm (W m^{-2}) of each experiment conditions. According with this setting, the equivalent average irradiance at 254 nm (table S1, exp. 5) was 5.25 W m^{-2} . On the other hand, the uncorrected average photon irradiance between 200 and 300 nm was 3.54 W cm^{-2} . These values increased less than 1% when the $\text{K}_2\text{S}_2\text{O}_8$ concentration was decreased to zero.

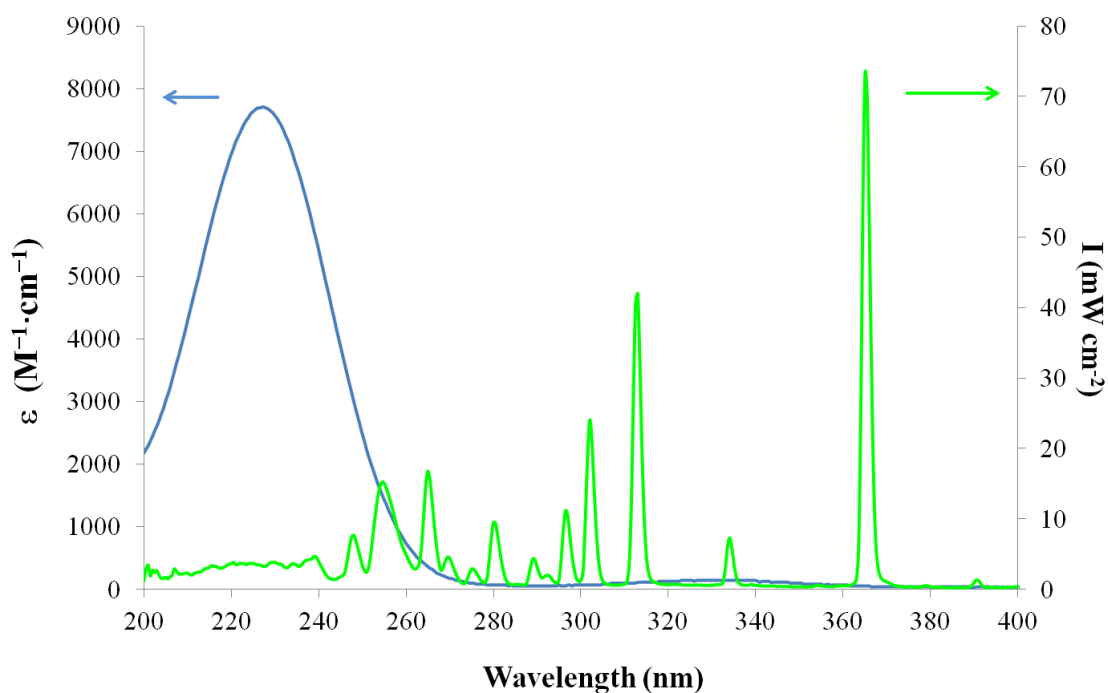


Figure S1. Emission spectrum of UV Medium Pressure Lamp and absorption spectra of NDMA

Text S3. Results supporting the description of experimental reaction kinetics

Table S1. Results obtained for NDMA photodegradation processes. $[\text{NDMA}]_0 = 6.75 \times 10^{-9} \text{ M}$. pH = 6

N° exp.	UV-MP	$\text{S}_2\text{O}_8^{2-}$ (μM)	IC (mM)	Cl^- (mM)	SO_4^{2-} (mM)	NDMA Degradation (%) $4.7 \times 10^3 \text{ J m}^{-2}$ (15 min)	$*k_{\text{obs}} \times 10^{-4}$ ($\text{m}^2 \text{ J}^{-1}$)	R square
1	✓	0	0	0	0	73.1	2.56 ± 0.32	0.97
2	✗	33.6	0	0	0	13.1	$(0.83 \pm 0.06) \times 10^{-2} \text{ min}^{-1}$	0.99
3	✓	6.72	0	0	0	77.5	3.18 ± 0.95	0.95
4	✓	20.2	0	0	0	95.2	6.68 ± 0.96	0.99
5	✓	33.6	0	0	0	100	9.30 ± 1.92	0.98
6	✓	33.6	0.25	0	0	83.5	3.89 ± 0.86	0.97
7	✓	33.6	0.5	0	0	78.8	3.29 ± 0.68	0.97
8	✓	33.6	0.75	0	0	73.8	2.72 ± 0.51	0.98
9	✓	33.6	1	0	0	64.8	2.34 ± 0.53	0.97
10	✓	33.6	0	0.25	0	90.4	4.90 ± 0.88	0.98
11	✓	33.6	0	0.5	0	76.5	3.11 ± 0.82	0.96
12	✓	33.6	0	0.75	0	80.0	3.58 ± 0.83	0.97
13	✓	33.6	0	1	0	77.5	3.36 ± 0.85	0.96
14	✓	33.6	0	0	1	97.4	7.71 ± 0.91	0.99
15	✓	33.6	1	1	1	75.3	2.93 ± 0.65	0.97
16	✓	33.6	0.5	0.5	0.5	79.9	3.36 ± 0.24	0.99

* The fluence-based rate constants (k_{obs} , $\text{m}^2 \text{ J}^{-1}$) were determined from the first-order plot of the natural logarithm of the normalized NDMA concentration versus the UV-fluence. The data were fitted by a first-order kinetic and the slopes of the lines represent the observed fluence-based rate constants k_{obs} . The error values for k_{obs} correspond to the 95% confidence interval of the linear fit.

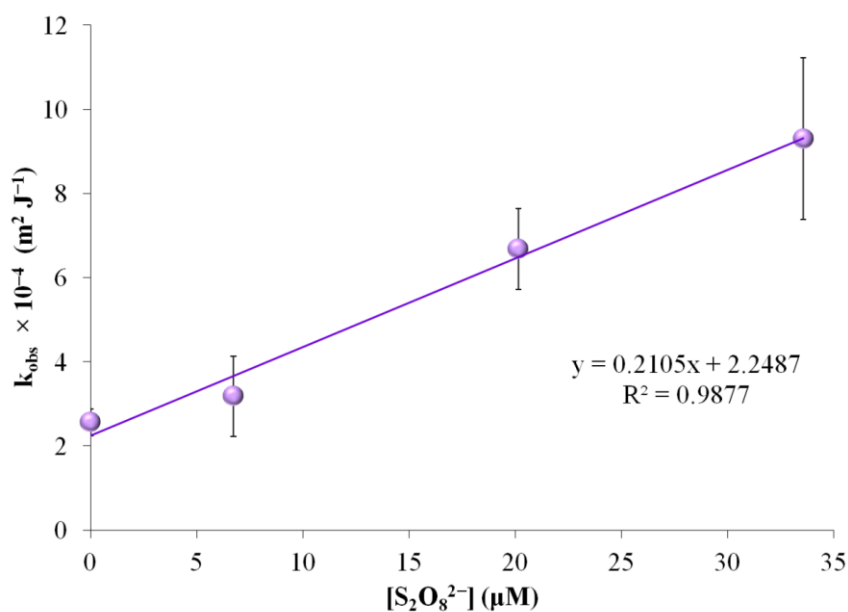


Figure S2. Linear increase in the NDMA degradation rate constant value as a function of the $\text{S}_2\text{O}_8^{2-}$ concentration in MP-UV processes.

Text S4. Kinetic modelling approach

The kinetic modelling was conducted using the modelling package Kintecus® v6.70. In the course of the kinetic modelling study we estimated the reaction rate constant for the reactions of NDMA with the sulfate, carbonate and dichloride anion radicals based on our experimental data, changing the values of the estimated constants and studying the impact on the evolution of the system.

The experiments 1, 3, 4 and 5 (table S1) were used for the fit of the estimation of the reaction rate constant between NDMA and the sulfate radical. In the case of the rate constant with the carbonate radical, the fit was made using the previously fitted rate constant for NDMA and sulfate radical to fit the results of the experiments num. 6 – 9, 15 and 16 (table S1) by adjusting the reaction rate of the carbonate radical with NDMA. Finally, to obtain the k value of NDMA with the dichloride anion radical, the adjustment was made using experiments 10 – 16.

Table S2. Principal reactions in kinetic model

Reaction	Rate constant	No. Ref.
$S_2O_8^{2-} + h\nu \rightarrow 2SO_4^{\bullet-}$	$\Phi = 0.70$	(1a) ⁵
$NDMA + h\nu \rightarrow \text{product}$	$\Phi = 0.30$	(1b) ⁶
$SO_4^{\bullet-} + SO_4^{\bullet-} \rightarrow S_2O_8^{2-}$	$k = 8.10 \times 10^8 \text{ M}^{-1} \text{ s}^{-1}$	(2) ⁷
$SO_4^{\bullet-} + S_2O_8^{2-} \rightarrow SO_4^{2-} + S_2O_8^{\bullet-}$	$k = 1.50 \times 10^5 \text{ M}^{-1} \text{ s}^{-1}$	(3) ⁷
$SO_4^{\bullet-} + H_2O \rightarrow SO_4^{2-} + H^+ + \bullet OH$	$k = 0.002 \text{ M}^{-1} \text{ s}^{-1}$	(4) ⁸
$\bullet OH + H_2O_2 \rightarrow HO_2^{\bullet} + H_2O$	$k = 2.70 \times 10^7 \text{ M}^{-1} \text{ s}^{-1}$	(5) ⁹
$\bullet OH + \bullet OH \rightarrow H_2O_2$	$k = 5.50 \times 10^9 \text{ M}^{-1} \text{ s}^{-1}$	(6) ⁹
$SO_4^{\bullet-} + \bullet OH \rightarrow HSO_4^- + \frac{1}{2}O_2$	$k = 1.00 \times 10^{10} \text{ M}^{-1} \text{ s}^{-1}$	(7) ¹⁰
$S_2O_8^{2-} + \bullet OH \rightarrow HSO_4^- + SO_4^{\bullet-} + \frac{1}{2}O_2$	$k = 1.20 \times 10^7 \text{ M}^{-1} \text{ s}^{-1}$	(8) ¹¹
$NDMA + SO_4^{\bullet-} \rightarrow \text{products}$	$k = 1.20 \times 10^7 \text{ M}^{-1} \text{ s}^{-1}$	(9) ^{this study}
$NDMA + \bullet OH \rightarrow \text{products}$	$k = 3.80 \times 10^8 \text{ M}^{-1} \text{ s}^{-1}$	(10) ¹²
$NDMA + CO_3^{\bullet-} \rightarrow \text{products}$	$k = 2.00 \times 10^4 \text{ M}^{-1} \text{ s}^{-1}$	(11) ^{this study}
$NDMA + Cl_2^{\bullet-} \rightarrow \text{products}$	$k = 3.00 \times 10^5 \text{ M}^{-1} \text{ s}^{-1}$	(12) ^{this study}

Reactions added to reactions 1-8 for the estimation of k (NDMA + $SO_4^{\bullet-}$) (reaction 9)

$HO_2^{\bullet} + H_2O_2 \rightarrow O_2 + \bullet OH + H_2O$	$k = 3.00 \text{ M}^{-1} \text{ s}^{-1}$	(13) ⁹
$HO_2^{\bullet} + HO_2^{\bullet} \rightarrow O_2 + H_2O_2$	$k = 8.30 \times 10^9 \text{ M}^{-1} \text{ s}^{-1}$	(14) ⁹
$\bullet OH + HO_2^{\bullet} \rightarrow O_2 + H_2O$	$k = 6.60 \times 10^9 \text{ M}^{-1} \text{ s}^{-1}$	(15) ⁹
$SO_4^{\bullet-} + OH^- \rightarrow SO_4^- + \bullet OH$	$k = 7.70 \times 10^7 \text{ M}^{-1} \text{ s}^{-1}$	(16) ¹³
$S_2O_8^{\bullet-} + OH^- \rightarrow S_2O_8^{2-} + \bullet OH$	$k = 6.50 \times 10^7 \text{ M}^{-1} \text{ s}^{-1}$	(17) ¹³
$H^+ + OH^- \rightarrow H_2O$	$k = 1.00 \times 10^{11} \text{ M}^{-1} \text{ s}^{-1}$	(18) ¹⁴
$MeOH + SO_4^{\bullet-} \rightarrow \text{products}$	$k = 1.00 \times 10^7 \text{ M}^{-1} \text{ s}^{-1}$	(19) ¹⁵
$MeOH + \bullet OH \rightarrow \text{products}$	$k = 9.70 \times 10^8 \text{ M}^{-1} \text{ s}^{-1}$	(20) ⁹

Reaction	Rate constant	No. Ref.
Additional reactions added for the estimation of k (NDMA + CO₃^{•-}) (reaction 11)		
SO ₄ ^{•-} + HCO ₃ ⁻ → CO ₃ ^{•-} + H ⁺ + SO ₄ ²⁻	k = 2.80 × 10 ⁶ M ⁻¹ s ⁻¹	(21) ¹⁶
SO ₄ ^{•-} + CO ₃ ²⁻ → CO ₃ ^{•-} + SO ₄ ²⁻	k = 2.50 – 6.10 × 10 ⁶ M ⁻¹ s ⁻¹	(22) ¹⁶
CO ₃ ^{•-} + •OH → products	k = 3.00 × 10 ⁹ M ⁻¹ s ⁻¹	(23) ¹⁷
H ₂ CO ₃ + •OH → products + H ₂ O + H ⁺	k = 1.00 × 10 ⁶ M ⁻¹ s ⁻¹	(24) ⁹
CO ₃ ^{•-} + S ₂ O ₈ ²⁻ → CO ₃ ²⁻ + S ₂ O ₈ ^{•-}	k = 3.00 × 10 ⁴ M ⁻¹ s ⁻¹	(25) ¹⁴
HCO ₃ ⁻ + Cl [•] → H ₂ O + CO ₃ ^{•-}	k = 2.40 × 10 ⁹ M ⁻¹ s ⁻¹	(26) ¹⁸
CO ₃ ²⁻ + Cl [•] → OH ⁻ + CO ₃ ^{•-}	k = 5.00 × 10 ⁸ M ⁻¹ s ⁻¹	(27) ¹⁸
HCO ₃ ⁻ + Cl ₂ ^{•-} → 2Cl ⁻ + H ⁺ + CO ₃ ^{•-}	k = 8.00 × 10 ⁷ M ⁻¹ s ⁻¹	(28) ¹⁹
CO ₃ ²⁻ + Cl ₂ ^{•-} → 2Cl ⁻ + CO ₃ ^{•-}	k = 1.60 × 10 ⁸ M ⁻¹ s ⁻¹	(29) ¹⁹
CO ₃ ²⁻ + •OH → CO ₃ ^{•-} + OH ⁻	k = 3.90 × 10 ⁸ M ⁻¹ s ⁻¹	(30) ⁹
HCO ₃ ⁻ + •OH → CO ₃ ^{•-} + H ₂ O	k = 8.60 × 10 ⁶ M ⁻¹ s ⁻¹	(31) ⁹
CO ₃ ²⁻ + H ⁺ → HCO ₃ ⁻	k = 5.00 × 10 ¹⁰ M ⁻¹ s ⁻¹	(32) ¹⁴
Additional reactions added for the estimation of k (NDMA + Cl₂^{•-}) (reaction 12)		
SO ₄ ^{•-} + Cl ⁻ → Cl [•] + SO ₄ ²⁻	k = 3.00 × 10 ⁸ M ⁻¹ s ⁻¹	(33) ¹⁰
Cl [•] + Cl [•] → Cl ₂	k = 8.80 × 10 ⁷ M ⁻¹ s ⁻¹	(34) ²⁰
Cl ⁻ + Cl [•] ↔ Cl ₂ ^{•-}	k = 6.50 × 10 ⁹ M ⁻¹ s ⁻¹	(35) ²¹
Cl ₂ ^{•-} + Cl ₂ ^{•-} → Cl ₂ + 2Cl ⁻	k = 9.00 × 10 ⁸ M ⁻¹ s ⁻¹	(36) ²²
Cl ₂ ^{•-} + Cl [•] → Cl ₂ + Cl ⁻	k = 2.10 × 10 ⁹ M ⁻¹ s ⁻¹	(37) ²²
Cl [•] + S ₂ O ₈ ²⁻ → products	k = 8.80 × 10 ⁶ M ⁻¹ s ⁻¹	(38) ²³
Cl ₂ ^{•-} + S ₂ O ₈ ²⁻ → products	k = 1.00 × 10 ⁴ M ⁻¹ s ⁻¹	(39) ²³
•OH + Cl ⁻ → ClOH ⁻	k = 4.30 × 10 ⁹ M ⁻¹ s ⁻¹	(40) ²⁴
ClOH ⁻ → •OH + Cl ⁻	k = 6.10 × 10 ⁹ M ⁻¹ s ⁻¹	(41) ²¹
Cl ₂ ^{•-} + •OH → HOCl + Cl ⁻	k = 1.00 × 10 ⁹ M ⁻¹ s ⁻¹	(42) ²⁵
Cl ₂ ^{•-} + HO ₂ [•] → O ₂ + 2Cl ⁻ + H ⁺	k = 3.00 × 10 ⁹ M ⁻¹ s ⁻¹	(43) ²⁵
Cl [•] + HOCl → ClO [•] + Cl ⁻ + H ⁺	k = 3.00 × 10 ⁹ M ⁻¹ s ⁻¹	(44) ²⁶
Cl [•] + H ₂ O ₂ → HO ₂ [•] + Cl ⁻ + H ⁺	k = 2.00 × 10 ⁹ M ⁻¹ s ⁻¹	(45) ²²
ClOH ⁻ + Cl ⁻ → Cl ₂ ^{•-} + OH ⁻	k = 2.10 × 10 ¹⁰ M ⁻¹ s ⁻¹	(46) ²⁷
ClOH ⁻ + H ⁺ → Cl [•] + H ₂ O	k = 1.00 × 10 ⁴ M ⁻¹ s ⁻¹	(47) ²⁴
HOCl + •OH → ClO [•] + H ₂ O	k = 2.00 × 10 ⁹ M ⁻¹ s ⁻¹	(48) ¹⁹
SO ₄ ²⁻ + Cl [•] → SO ₄ ^{•-} + Cl ⁻	k = 2.50 × 10 ⁸ M ⁻¹ s ⁻¹	(49) ¹⁰
MeOH + Cl [•] → products	k = 1.00 × 10 ⁹ M ⁻¹ s ⁻¹	(50) ²⁸

Text S5. Comparison of the results of kinetic modelling and experimental observation

Incident photon irradiance is $I = 4.16 \text{ W m}^{-2}$ and error bars represent the mean deviation of experimental duplicate values in all subsequent figures.

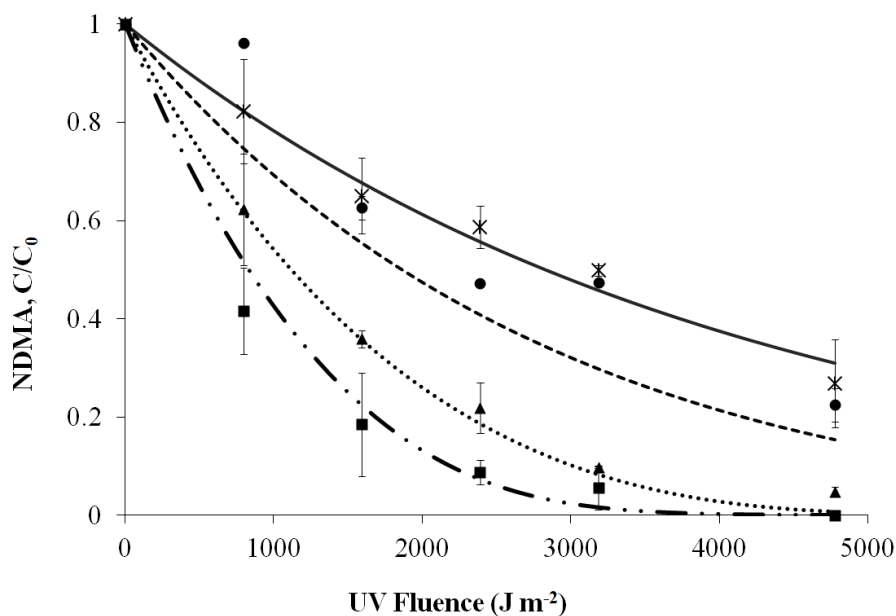


Figure S3. Kinetic modelling of the impact of the $\text{K}_2\text{S}_2\text{O}_8$ concentration in the NDMA degradation during MP-UV irradiation (table S1, exp. 1, 3 – 5). $[\text{S}_2\text{O}_8^{2-}]_0$ (μM) = 0 (—*—); 6.72 (—●—); 20.2 (··▲··); 33.6 (—■—). $[\text{NDMA}]_0 = 6.75 \times 10^{-9} \text{ M}$. pH = 6.

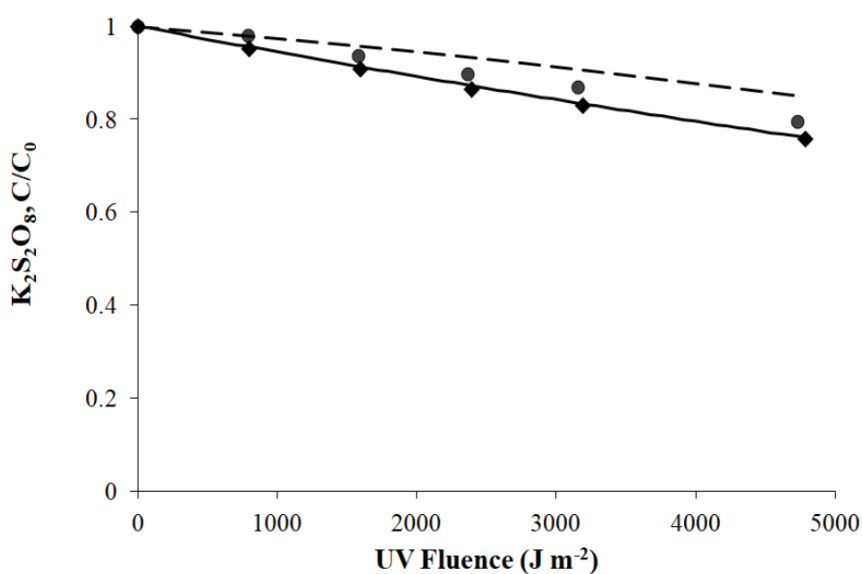


Figure S4. Kinetic modelling of the $\text{K}_2\text{S}_2\text{O}_8$ concentration in the MP-UV system with $33.6 \mu\text{M}$ as initial concentration of the oxidant, in HPLC water (—●—) and water with 1 mM of sulfate, bicarbonate and chloride anions (—◆—) (table S1, exp. 5 and 15).

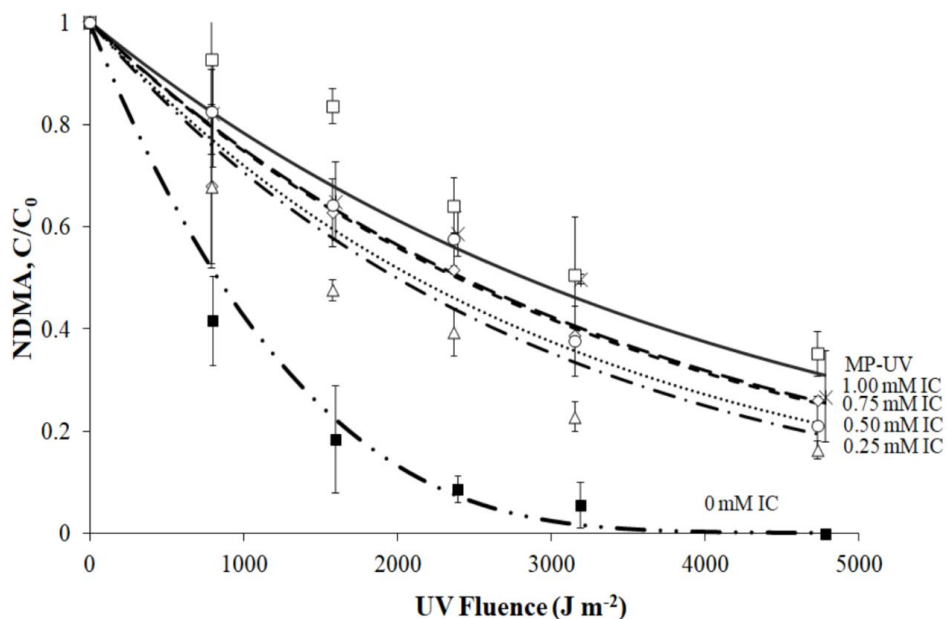


Figure S5. Kinetic modelling of the effect of the IC concentration on the NDMA degradation during MP-UV irradiation with $33.6 \mu\text{M}$ of $\text{S}_2\text{O}_8^{2-}$ initial concentration (table S1, exp. 1, 5 – 9). Degradation processes: UV (—*—); UV/ $\text{S}_2\text{O}_8^{2-}$ with $[\text{IC}] = 0 \text{ mM}$ (---■---), 0.25 mM (---△---), 0.5 mM (··○··), 0.75 mM (--◇--), 1 mM (- -□- -). $[\text{NDMA}]_0 = 6.75 \times 10^{-9} \text{ M}$. pH = 6.

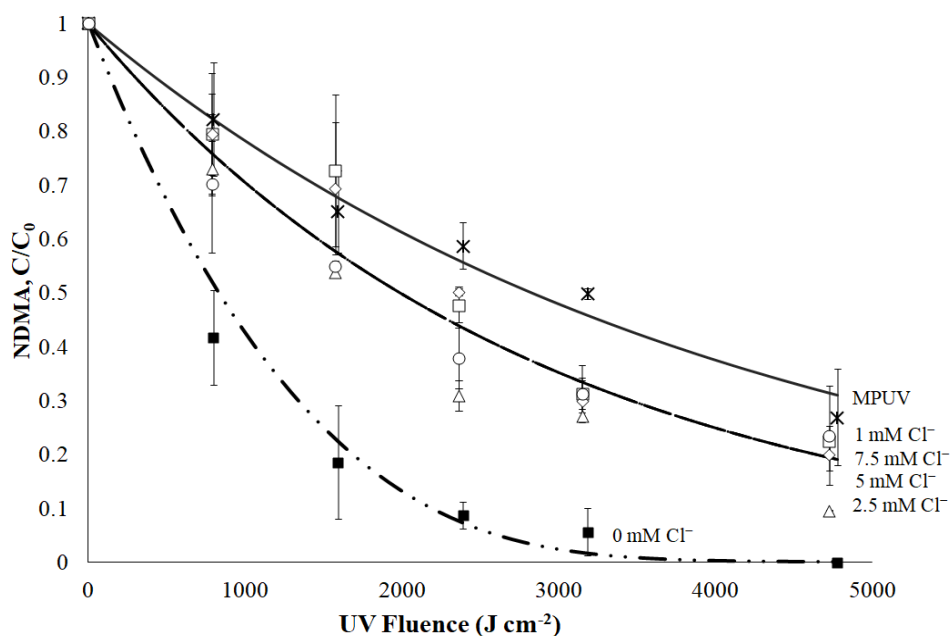


Figure S6. Kinetic modelling of the effect of the Cl^- concentration on the NDMA degradation during MP-UV irradiation with $33.6 \mu\text{M}$ of $\text{S}_2\text{O}_8^{2-}$ initial concentration (table S1, exp. 1, 5, 10 – 13). Degradation processes: UV (—*—); UV/ $\text{S}_2\text{O}_8^{2-}$ with $[\text{Cl}^-] = 0 \text{ mM}$ (---■---), 0.25 mM (---△---), 0.5 mM (··○··), 0.75 mM (--◇--), 1 mM (- -□- -). $[\text{NDMA}]_0 = 6.75 \times 10^{-9} \text{ M}$. pH = 6.

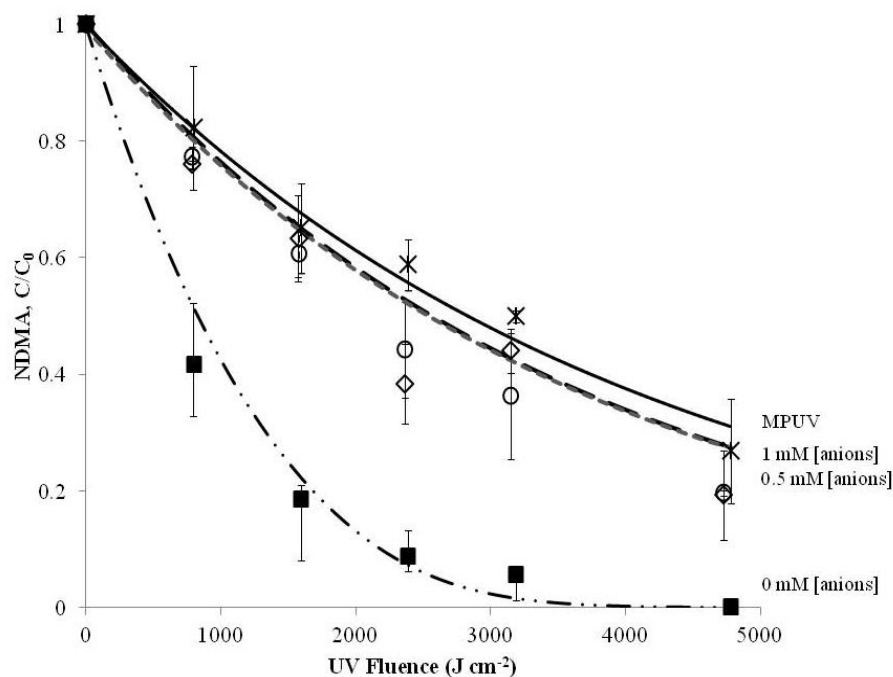


Figure S7. Kinetic modelling of the effect of the simultaneous presence of IC, SO_4^{2-} , and Cl^- on the NDMA degradation during MP-UV irradiance with $33.6 \mu\text{M}$ of $\text{S}_2\text{O}_8^{2-}$ initial concentration (table S1, exp. 1, 5, 15, 16). Degradation processes: UV ($—*—$); UV/ $\text{S}_2\text{O}_8^{2-}$ with [anions] = 0 mM each ($- \cdot \cdot - \blacksquare - \cdot \cdot -$), 0.5 mM each ($--\bigcirc--$), 1mM each ($- - \diamond - -$). $[\text{NDMA}]_0 = 6.75 \times 10^{-9}$ M. pH = 6.

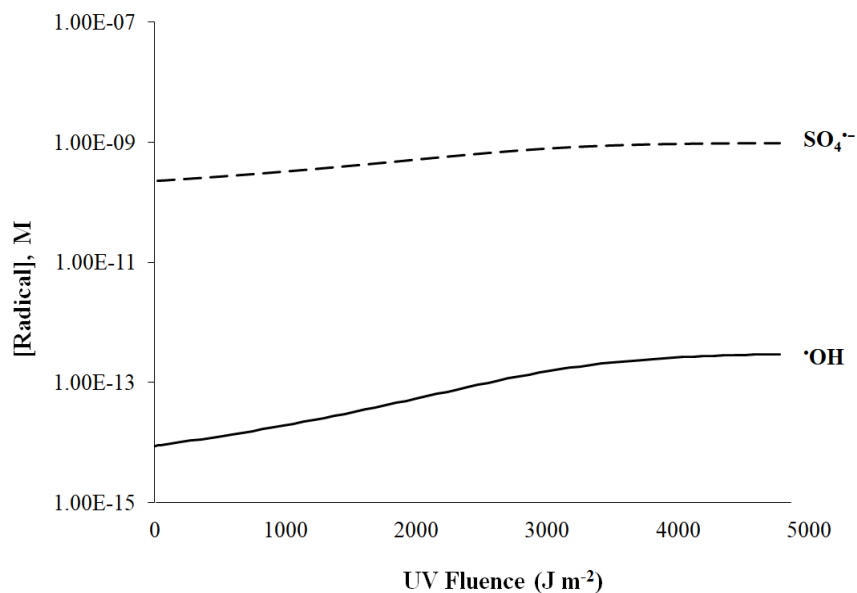


Figure S8. Oxidant species distribution obtained by kinetic modelling in the UV/ $\text{K}_2\text{S}_2\text{O}_8$ system in HPLC water during MP-UV irradiation. $[\text{S}_2\text{O}_8^{2-}]_0 = 33.6 \mu\text{M}$.

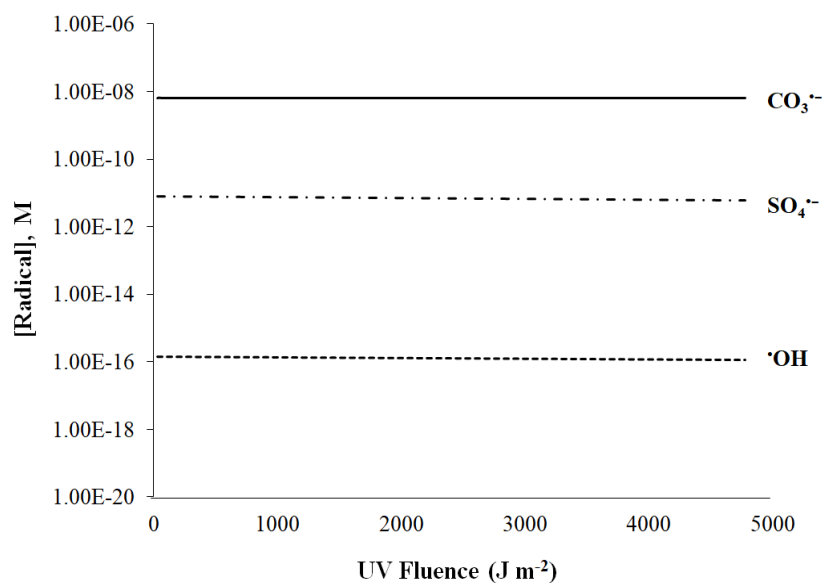


Figure S9. Oxidant species distribution obtained by kinetic modelling in the UV/ $\text{K}_2\text{S}_2\text{O}_8$ system in water with 1mM of IC during MP-UV irradiation. $[\text{S}_2\text{O}_8^{2-}]_0 = 33.6 \mu\text{M}$.

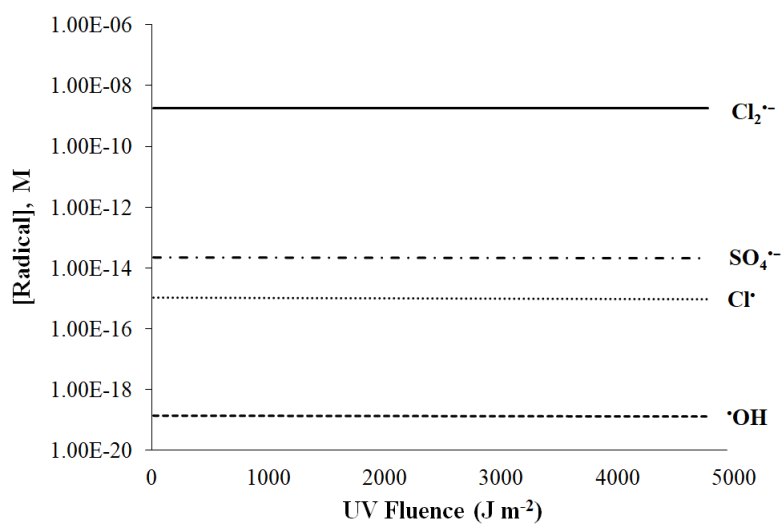


Figure S10. Oxidant species distribution obtained by kinetic modelling in the UV/ $\text{K}_2\text{S}_2\text{O}_8$ system in water with 1mM of Cl^- during MP-UV irradiation. $[\text{S}_2\text{O}_8^{2-}]_0 = 33.6 \mu\text{M}$.

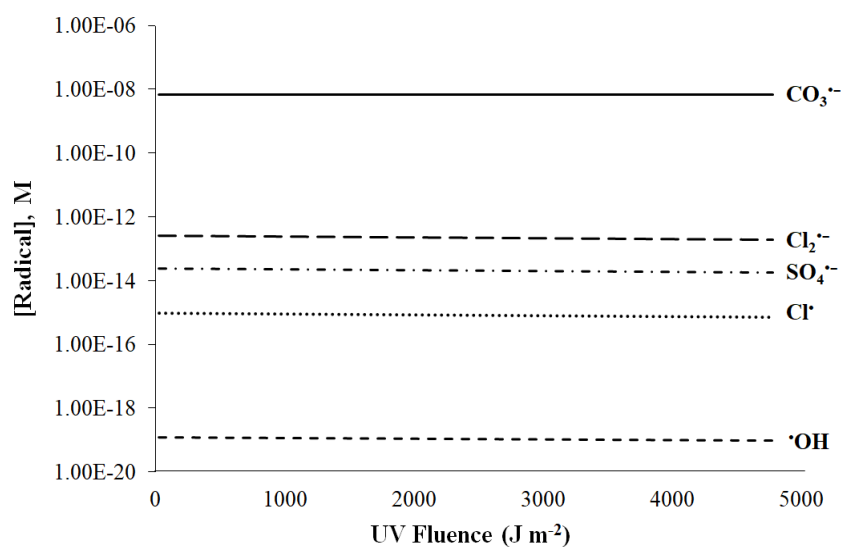


Figure S11. Oxidant species distribution during MP-UV irradiation obtained by kinetic modelling in the UV/ $\text{K}_2\text{S}_2\text{O}_8$ system in water with simultaneous presence of IC, SO_4^{2-} , and Cl^- at 1mM concentration of each of them. $[\text{S}_2\text{O}_8^{2-}]_0 = 33.6 \mu\text{M}$.

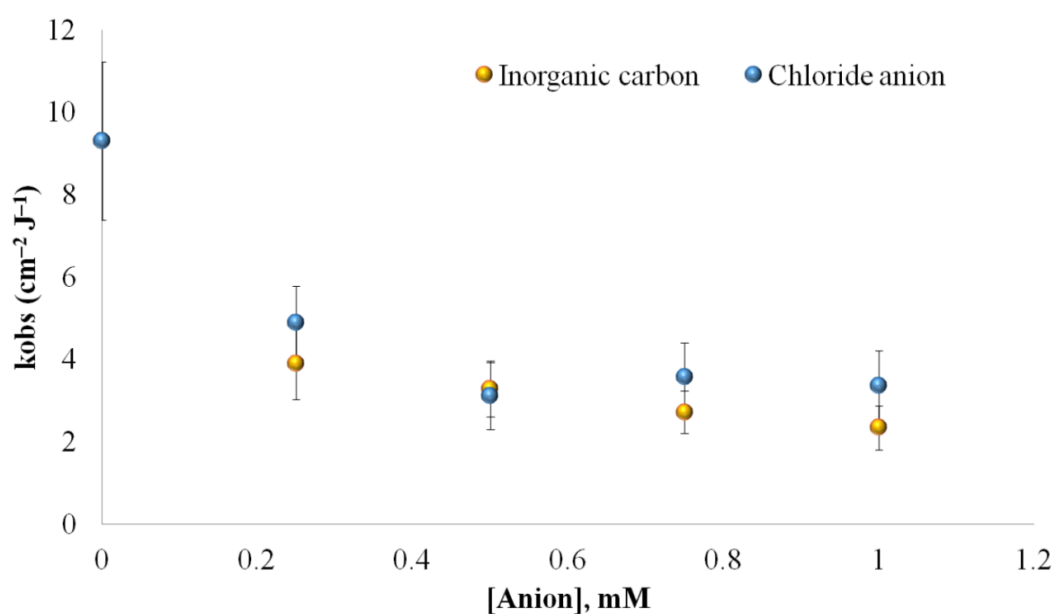


Figure S12. Effect of concentration of chloride and IC on the rate of NDMA degradation by UV/ $\text{K}_2\text{S}_2\text{O}_8$ during MP-UV irradiation. $[\text{S}_2\text{O}_8^{2-}]_0 = 33.6 \mu\text{M}$.

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