

ACFAMP

Aircraft Cartridge Filter Analysis Modelling Program

User's Manual

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OVERVIEW – ABOUT ACFAMP

Aircraft Cartridge Filter Analysis Modelling Program (ACFAMP) is a **Finite Element Based (FEM) FORTRAN** computer code designed to simulate the hydrodynamics and design parameters for pleated filter cartridge fabrication. It allows the user to enter the cartridge filter specifications, filtration operating conditions such as inlet volumetric flow rates, physical properties of the fluids used in filter testing and the filter media characteristics in order to evaluate critical parameters such as optimal pressure drop. **ACFAMP** also quantifies the compression effects and apparent losses in cartridge filtration area, which are of prime importance in cartridge design, sizing and manufacture.

TECHNICAL SPECIFICATIONS

1. **ACFAMP** is written in FORTRAN 90.
2. **ACFAMP** is a 2 - dimensional Porous flow and combined Free/Porous flow simulation package. The solution scheme for **ACFAMP** is based on the **U-V-P** finite element method. Porous flow simulation is based on **Artificial Compressibility Method** whilst the combined flow simulator employs both the **Artificial Compressibility** and **Taylor-Hood** schemes.
3. **ACFAMP** solves the **DARCY** and **STOKES** momentum balance equations and the **CONTINUITY** equation for incompressible flow problems in the Cartesian co-ordinate system using the Weighted Residual Standard Galerkin Finite Element Method (**WRSGFEM**).
4. **ACFAMP** can program the solution of non-Newtonian and non-isothermal incompressible transient and steady flow problems.
5. **ACFAMP** has inbuilt mathematical permeability models (based on actual experimental test data) for different filter media.
6. **ACFAMP** can perform “**2-D hydrodynamic simulation for a pleated cartridge without any compression effects**” and also “**simulates compression factors and apparent losses in filtration area**” for a given filter cartridge.
7. Algebraic equations in **ACFAMP** are solved by a frontal method.
8. Post-processing files generated by **ACFAMP** can directly be exported to **SURFER**, **TECPLOT** and **COSMOS** for purposes of visualisation.
9. **AFCAMP** has 23 subroutines that are directly accessible to the user and can be easily modified depending on the modelling requirements.

SYSTEM REQUIREMENTS & INSTALLATION

1. System Requirements (Essential)

- a. The recommended hardware for the system consists of a **Desktop PC** with a **Pentium** type processor having at least **32MB RAM**. However, we would specifically recommend a **Pentium - 4 (3.2 GHz)** processor with **512 MB RAM** for faster computations.
- b. **Microsoft Windows 95, 98, ME, NT, XP or 2000** operating system.
- c. **Compaq Visual Fortran 6.6** for **ACFAMP** compilation and execution.

2. System Requirements (Auxiliary)

- a. Installed **COSMOS/M 2.6** for mesh generation and visualisation
- b. Installed **TECHPLOT 8.0** for visualisation.
- c. Installed **GOLDEN SOFTWARE SURFER** for visualisation.

3. Installation Procedure

- a. Make a sub-directory for **ACFAMP** in the main **WINDOWS** directory and position the **ACFAMP** program with accompanying **Input data files** for comprehensive cartridge filter analysis in the sub-directory.
- b. Right click on the **ACFAMP** program and open it with **COMPAQ VISUAL FORTRAN 6.6** compiler.
- c. Go to the **COMPAQ VISUAL FORTRAN 6.6** main menu, click on **Build command Compile ACFAMP Execute ACFAMP**

GETTING STARTED

Working Step 1

Use the auxiliary FORTRAN program *FILTERdataprep.f* to prepare the information data file containing the geometrical characteristics and operational experimental data pertaining to a specific filter cartridge. It should be noted that approximate loss in area factors are required for performing simulations using ACFAMP and should be manually referred from the filter database PLEBASE.

Working Step 2

For the execution of ACFAMP three data files are the requisites

File created using the auxiliary program *FILTERdataprep.f*

GFM file created after the mesh generation step using COSMOS 2.6/M

Default file *df.dat* containing the elemental connectivity of the filter mesh

Once ACFAMP is executed it prompts the user to input the names of the three files and thereafter the number crunching starts.

Working Step 3

The simulated results are presented in three separate files which can be directly used for post-processing procedures,

Aerout.txt contains the data for finite element simulations in form of nodal velocities and pressures which can be visualised in COSMOS 2.6/M, TECHPLOT and SURFER

Excel.txt contains cartridge design parameters such as apparent losses in filtration area, medium compression and pressure gradients inclusive and exclusive of medium compression and loss in area effects.

PROGRAM SUBROUTINES - HEIRARCHY

SUBROUTINES, LEVEL 1

1.	AREALOSS	:	Called by ACFAMP
2.	CARTRIDGE	:	Called by ACFAMP
3.	EXCELPRINT	:	Called by ACFAMP
4.	GETELM	:	Called by ACFAMP
5.	GETMAT	:	Called by ACFAMP
6.	GETNOD	:	Called by ACFAMP
7.	GFMFEM	:	Called by ACFAMP
8.	HYDROFILTER	:	Called by ACFAMP
9.	PLEATBC	:	Called by ACFAMP

SUBROUTINES, LEVEL 2

1.	CLEAN	:	Called by HYDROFILTER
2.	CONTOL	:	Called by HYDROFILTER
3.	FLOW	:	Called by HYDROFILTER
4.	OUTPUT	:	Called by HYDROFILTER
5.	PUTBCV	:	Called by HYDROFILTER
6.	SECINV	:	Called by HYDROFILTER
7.	SETPRM	:	Called by HYDROFILTER

SUBROUTINES, LEVEL 3

1.	DERIV	:	Called by FLOW
2.	FRONT	:	Called by FLOW
3.	GAUSSP	:	Called by FLOW
4.	PERM	:	Called by FLOW
5.	SHAPE	:	Called by FLOW
6.	VISCA	:	Called by FLOW
7.	MINIMAX	:	Called by OUTPUT

SUBROUTINES, LEVEL 4

1.	BACSUB	:	Called by FRONT
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Please note that all the subroutines at a particular level have been listed alphabetically

PROGRAM SUBROUTINES - FUNCTIONS

AREALOSS	Evaluates the loss in filtration area factor for velocity correction and the apparent percentage loss in filtration area at a given flow rate
BACSUB	Uses the Back substitution method for finding the final solution vector
CARTRIDGE	Reads the cartridge specifications such as number of pleats, height of the filter element, length of the pleat, diameter of the inner core, total filtration area, different inlet flow rates, viscosity of the fluid coordinates of the cartridge filter mesh
CLEAN	Cleans the arrays and prepares them for solution
CONTOL	Makes a check for the convergence of variables
DERIV	Calculates the Jacobean matrix, the determinant of the Jacobean matrix and global derivatives of the shape functions used in finite element calculations
EXCELPRINT	Prints the simulated pressure drop values with no compression and no loss in area, with compression and no loss in area, and with compression effects and loss in filtration area; percentage compression and apparent loss in filtering area at a given flow rate
FLOW	Calculates the velocities and pressures based on finite element method
FRONT	Employs the frontal method for solving the final set of equations
GAUSSP	Specifies the gauss points and weights for quadrature integration

PROGRAM SUBROUTINES - FUNCTIONS

GETELM	Specifies the nodal connectivity array for every element
GETMAT	Reads the material parameters
GETNOD	Reads the coordinates of the filter mesh from the MESH.FEM file
GFMFEM	Generates the mesh coordinates of the filter to be used in finite element simulations
HYDROFILTER	Simulates the 2-D hydrodynamic field in a filter without any compression and loss in area effect, with compression effects and with compression effects and apparent losses in filtration area
OUTPUT	Prints the final solution in form of 2 - dimensional velocities (x and y components) and the pressure field at different times
PERM	Calculates the permeability of the filter cartridge media used in analysis at different pressure drop values
PLEATBC	Generates the inlet velocity boundary conditions for filter cartridge simulation from the specified inlet volumetric flow rates
PUTBCV	Imposes the primary boundary conditions for velocity
SECINV	Calculates the second invariant of rate of deformation stress tensor, which depends on the velocity gradients for a particular time step

PROGRAM SUBROUTINES - FUNCTIONS

SETPRM	Sets the location data for nodal degrees of freedom that are the velocities and the pressures associated with each node in the cartridge mesh
SHAPE	Calculates the shape functions and their derivatives used in finite element calculations
VISCA	Calculates the viscosity according to the power law model valid for shear thickening hydraulic fluids used in aircraft filters

LIST OF PRIME VARIABLES - AFCAMP

aa:	Left hand side finite element stiffness matrix
actpress:	Normalised value of nodal pressure
alpha:	Time-stepping parameter
ak:	Right hand side finite element stiffness matrix
areabase:	Percentage loss in area factor
b:	Measure of Gaussian integration
bc:	Array for storing boundary constraint value
cartrid:	Reference ID for each filter cartridge element
cg:	Weighting functions for Gauss integration
comfactor:	Compression factor for filter medium
cord:	Array storing coordinate values of each nodal point
da:	Global derivative of shape function
del:	Local derivatives of shape function
deltap:	Experimental pressure drop
deltat:	Value of time step used in calculation iterations
density:	Density of fluid used for each set of experiment
detj:	Determinant of Jacobian matrix
di:	Diameter of inner core of the filter cartridge element
el:	Length of pleat
enp:	Number of pleats in each filter cartridge element
errp:	Square of discrepancy between pressure values calculated in two successive iterations
errv:	Square of discrepancy between velocity values calculated in two successive iterations
eta:	y-coordinate in local coordinate system
excel:	Array for storing simulated values of pressure drop in each step of calculation procedure
farea:	Filtering surface area of cartridge
frate:	Flow rate values for each experiment

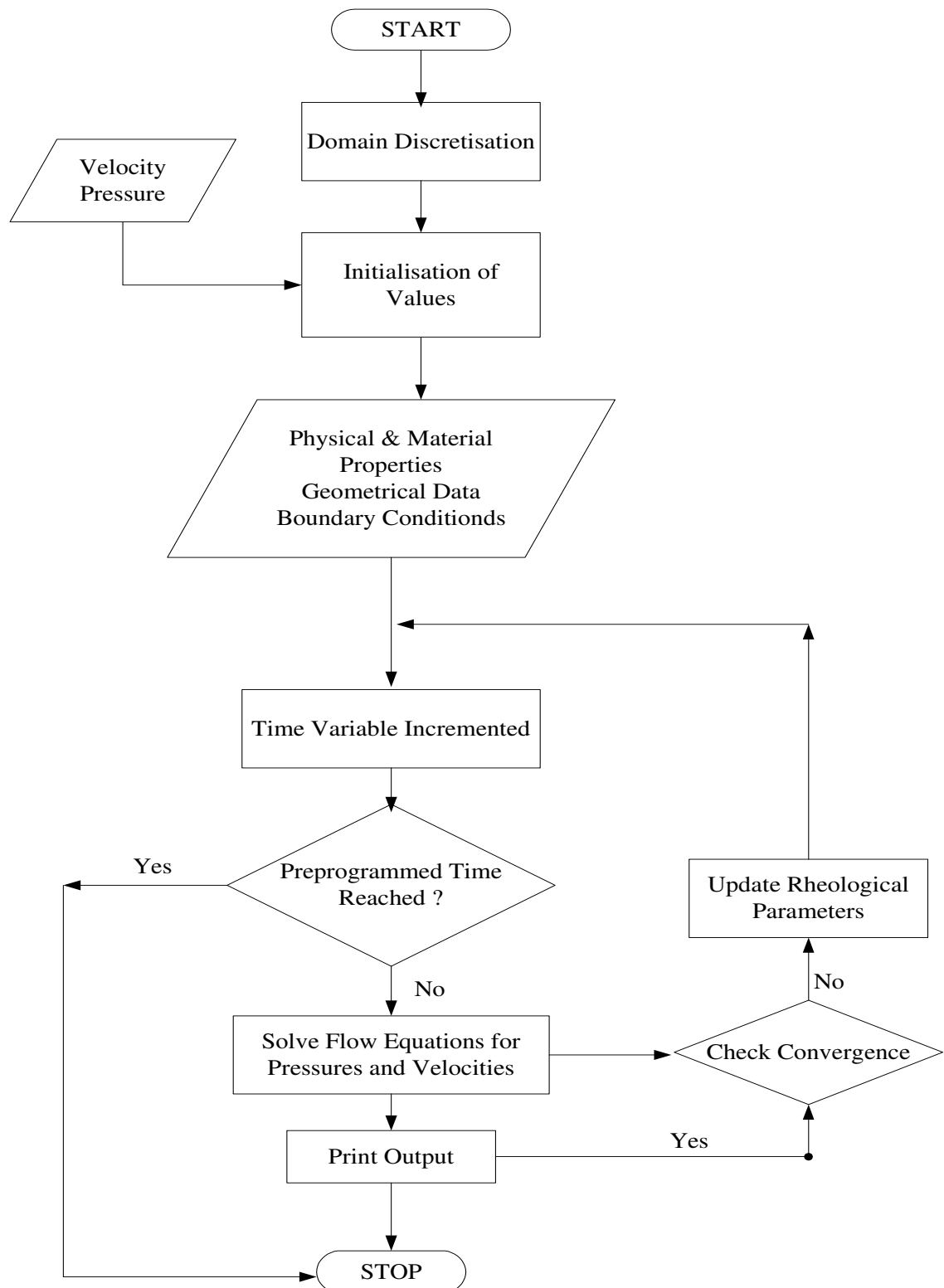
LIST OF PRIME VARIABLES - AFCAMP

gamad:	Rate of deformation of viscous stress tensor
guessp:	Pressure with compression and loss in area
hp:	Height of filter cartridge element
icord:	Switch for changing the coordinate system of equations
maxbc:	Limit for maximum number of boundary constraints that can be specified
maxdf:	Limit for maximum number of nodal degrees of freedom
maxel:	Limit for maximum number of elements in mesh
maxnp:	Limit for maximum number of nodal points in mesh
maxst:	Maximum dimension of finite element stiffness matrix
nb:	Total number of boundary-node constraints
ncn:	Number of nodes associated with each finite element
ncod:	Array for constraint switch defined for every degree of freedom
ndf:	Total number of nodal degrees of freedom
ndim:	Dimensions of the solution domain
nel:	Total number of elements in pleated cartridge mesh
ngaus:	Number of quadrature points required for Gaussian integration
nmat:	Total number of fluids
nnp:	Total number of nodal points in pleated cartridge mesh
node:	Array for nodal connectivity of elements
ntd:	Number of sets of experiment
nter:	Number of solution iterations
num:	Number of integration points per element
p:	Finite element shape or interpolation functions
pd:	Experimental pressure value for each set of data
percomp:	Percentage value of filter medium compression
permstep1:	Permeability of filter medium without compression
permstep2:	Permeability of filter medium with compression
permx:	Permeability of the filter medium in x-direction
permy:	Permeability of the filter medium in y-direction
pmat:	Array storing values of physical properties of the fluid

LIST OF PRIME VARIABLES - AFCAMP

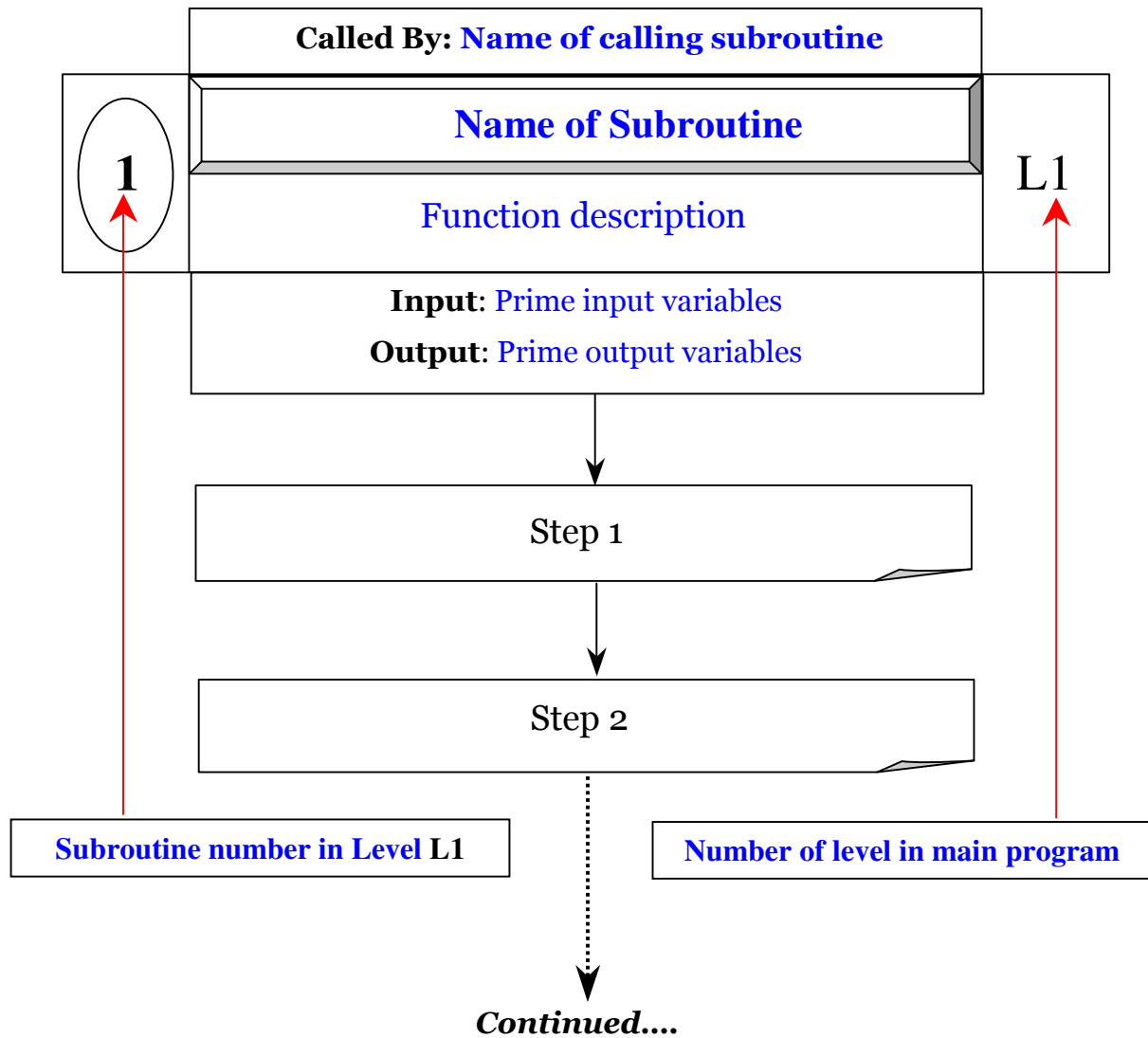
power:	Power law index for the fluid viscosity
press:	Array for nodal pressure
pressexp:	Experimental pressure drop
rpef:	Reference pressure
rr:	Array for storing the elemental load vector
rtem:	Reference temperature
rvisc:	Consistency coefficient for viscosity of fluid
sinv:	Array storing components of second invariant of rate of deformation of stress tensor
soln:	Array for storing solution values calculated by Frontal Solver
step:	Stage of the calculation procedure
taco:	Coefficient a in the power law model
tbco:	Coefficient b in the power law model
time:	Amount of time for iterations
tolv:	Maximum allowable tolerance for fluctuation in velocity value
tolp:	Maximum allowable tolerance for fluctuation in pressure value
vel:	Array for nodal velocities
velsound:	Velocity of sound in fluid
viisc:	Viscosity of fluid used for each set of experiment
visc:	Updated value of viscosity according to power law model
xg:	Coordinates of Gauss quadrature points for integration
xi:	x-coordinate in local coordinate system

SOLUTION ALGORITHM - AFCAMP



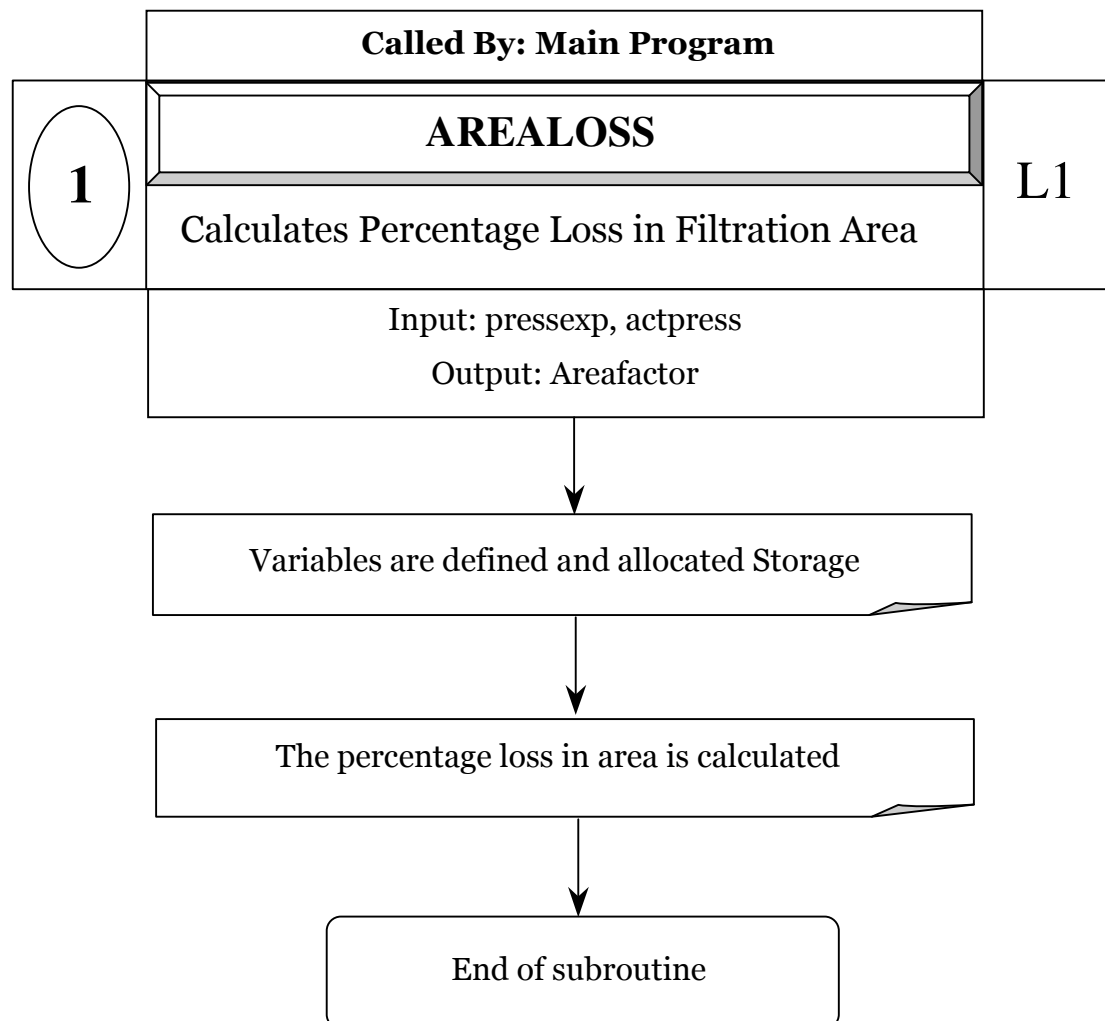
PROGRAM SUBROUTINES - INTERACTIONS

A PROTOTYPE CONVENTION



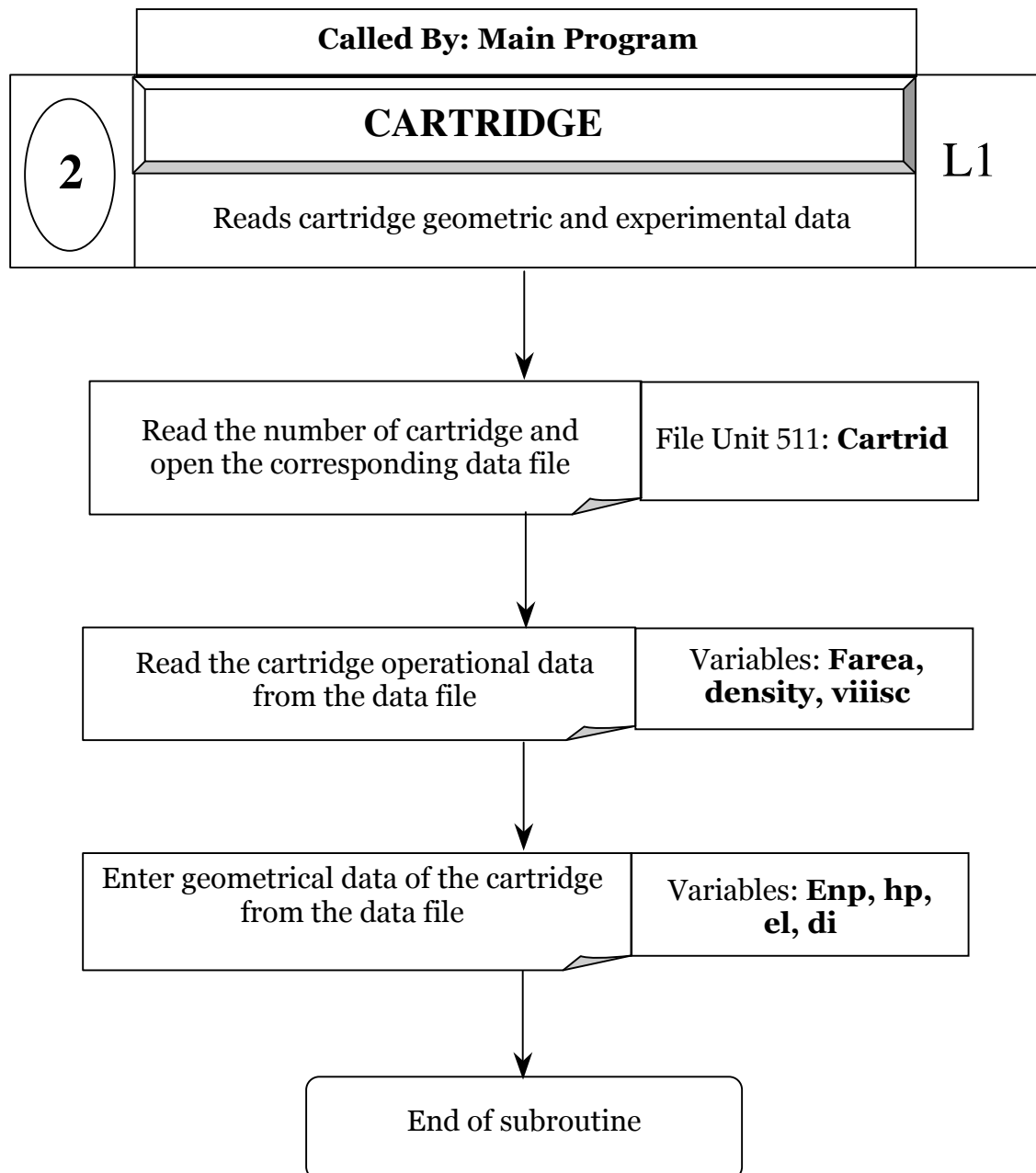
PROGRAM SUBROUTINES - INTERACTIONS

SUBROUTINE AREALOSS, LEVEL 1



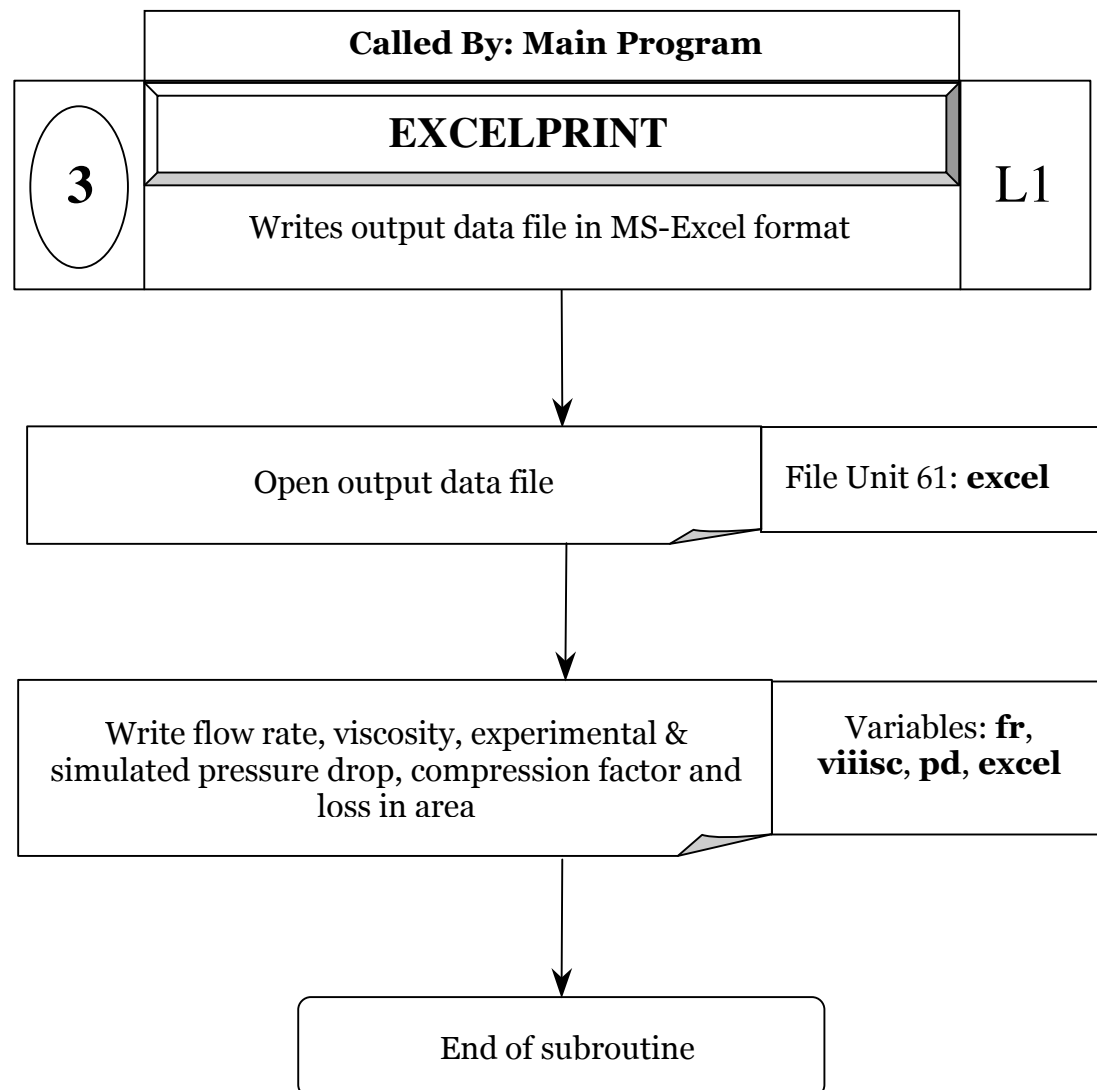
PROGRAM SUBROUTINES - INTERACTIONS

SUBROUTINE CARTRIDGE, LEVEL 1



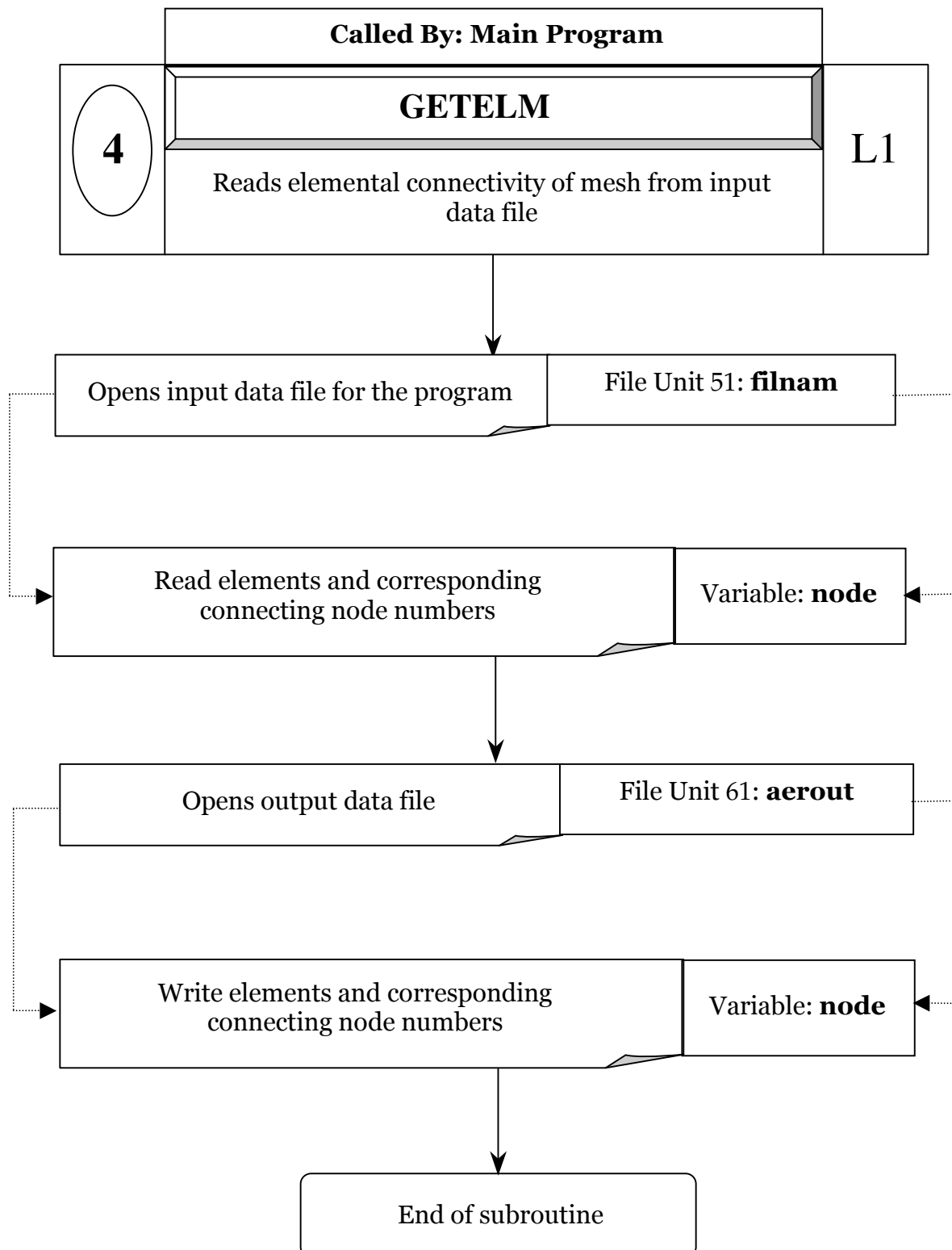
PROGRAM SUBROUTINES - INTERACTIONS

SUBROUTINE EXCELPRINT, LEVEL 1



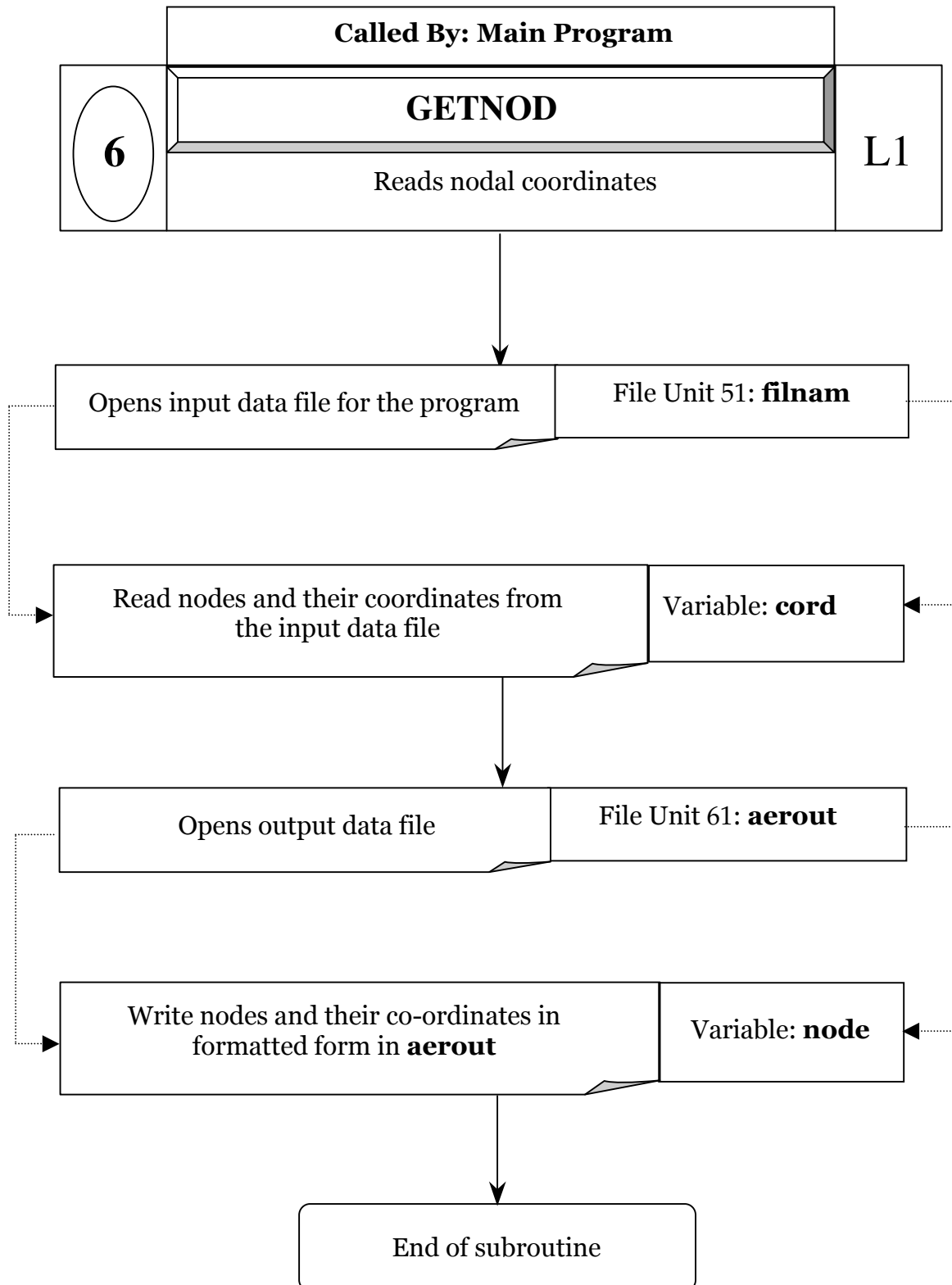
PROGRAM SUBROUTINES - INTERACTIONS

SUBROUTINE GETELM, LEVEL 1



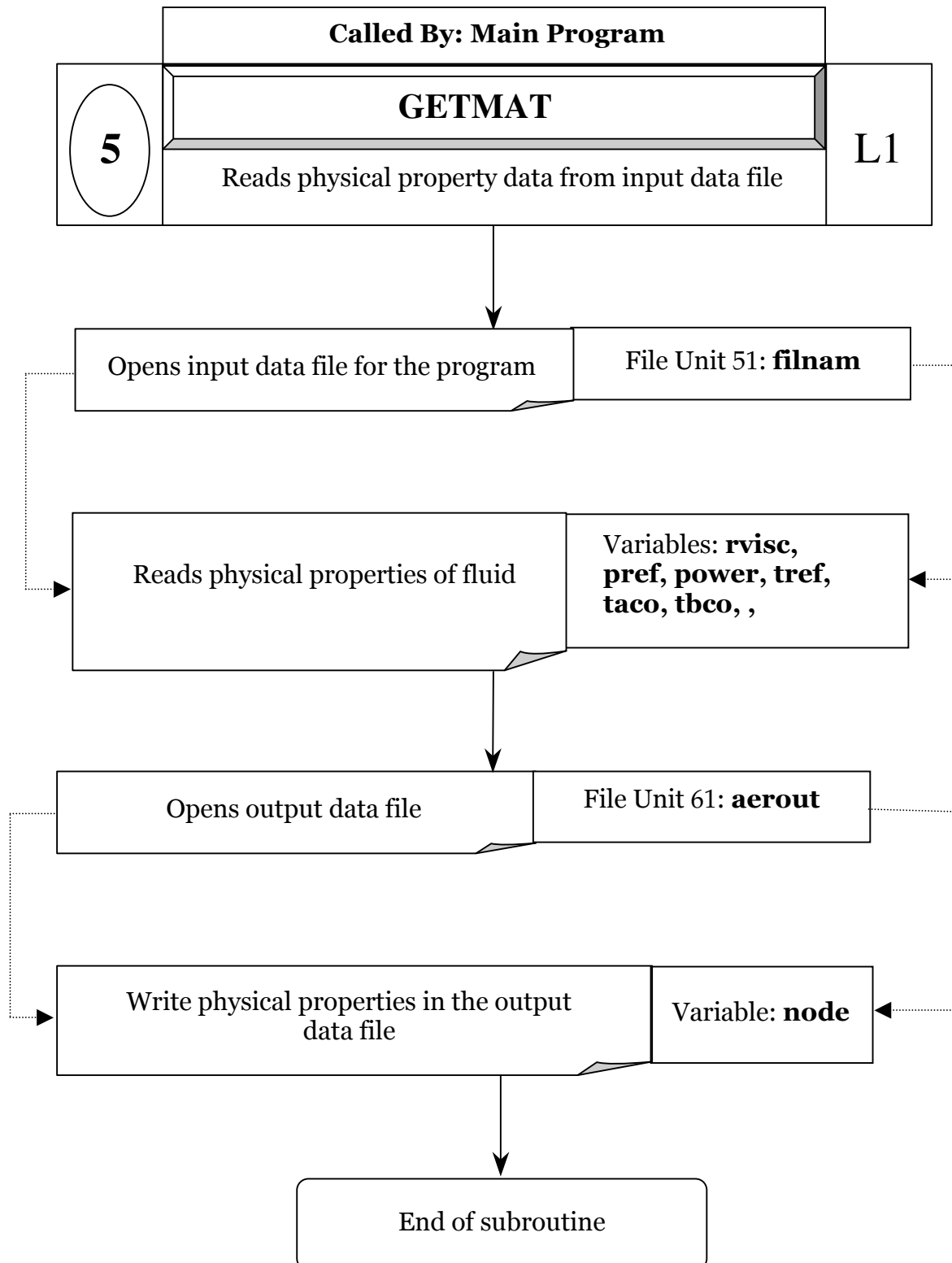
PROGRAM SUBROUTINES - INTERACTIONS

SUBROUTINE GETNOD, LEVEL 1



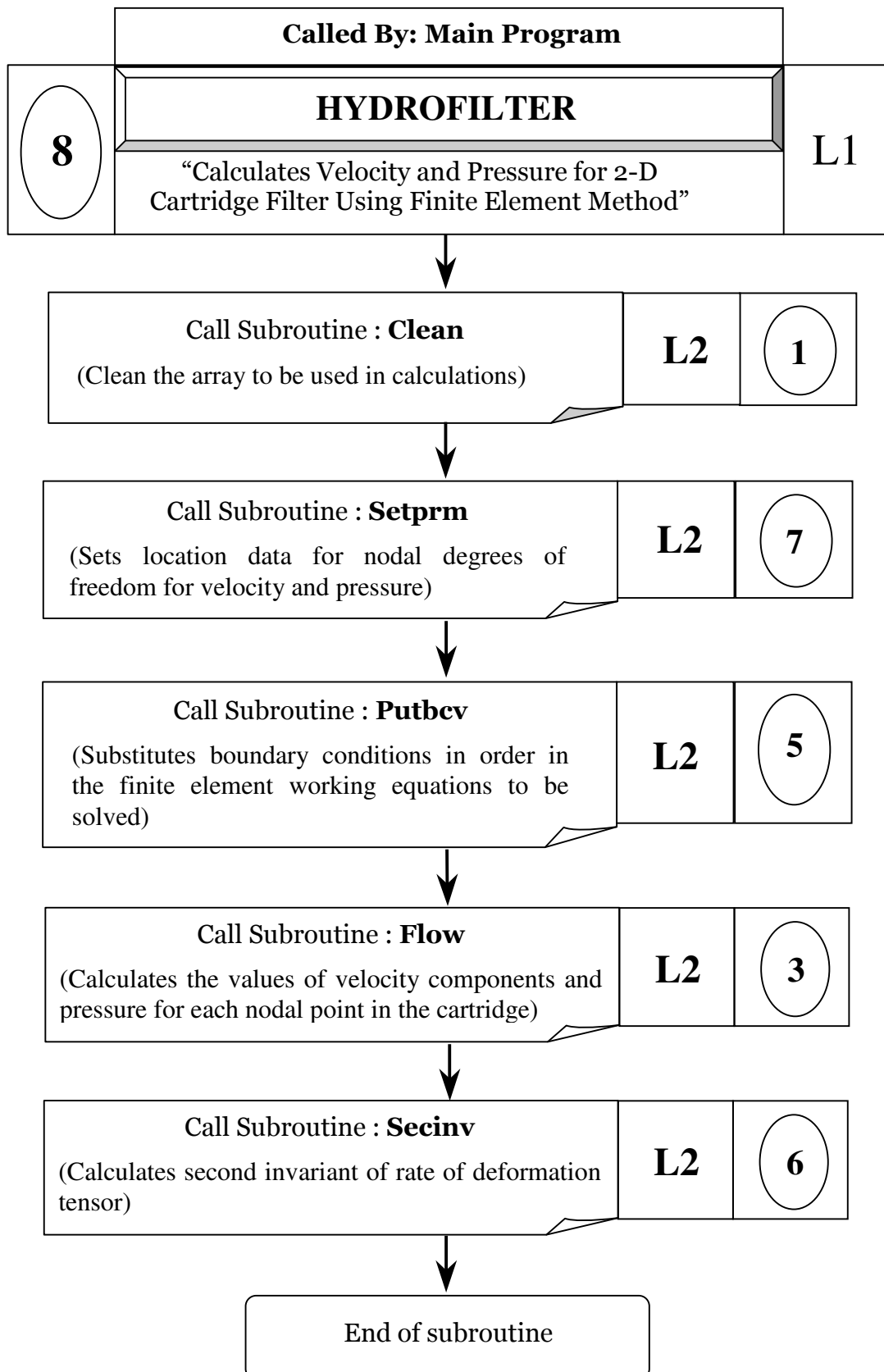
PROGRAM SUBROUTINES - INTERACTIONS

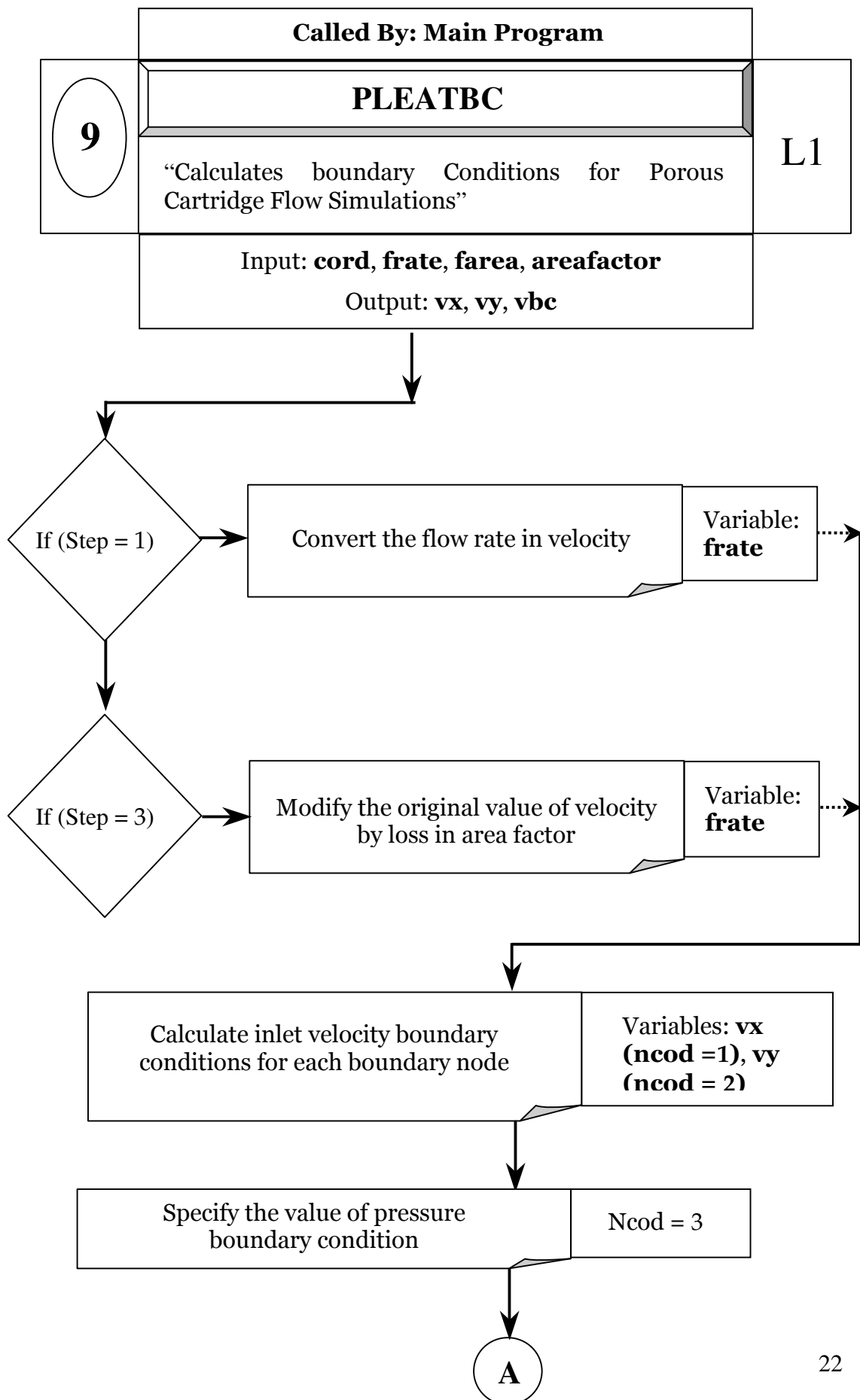
SUBROUTINE GETMAT, LEVEL 1

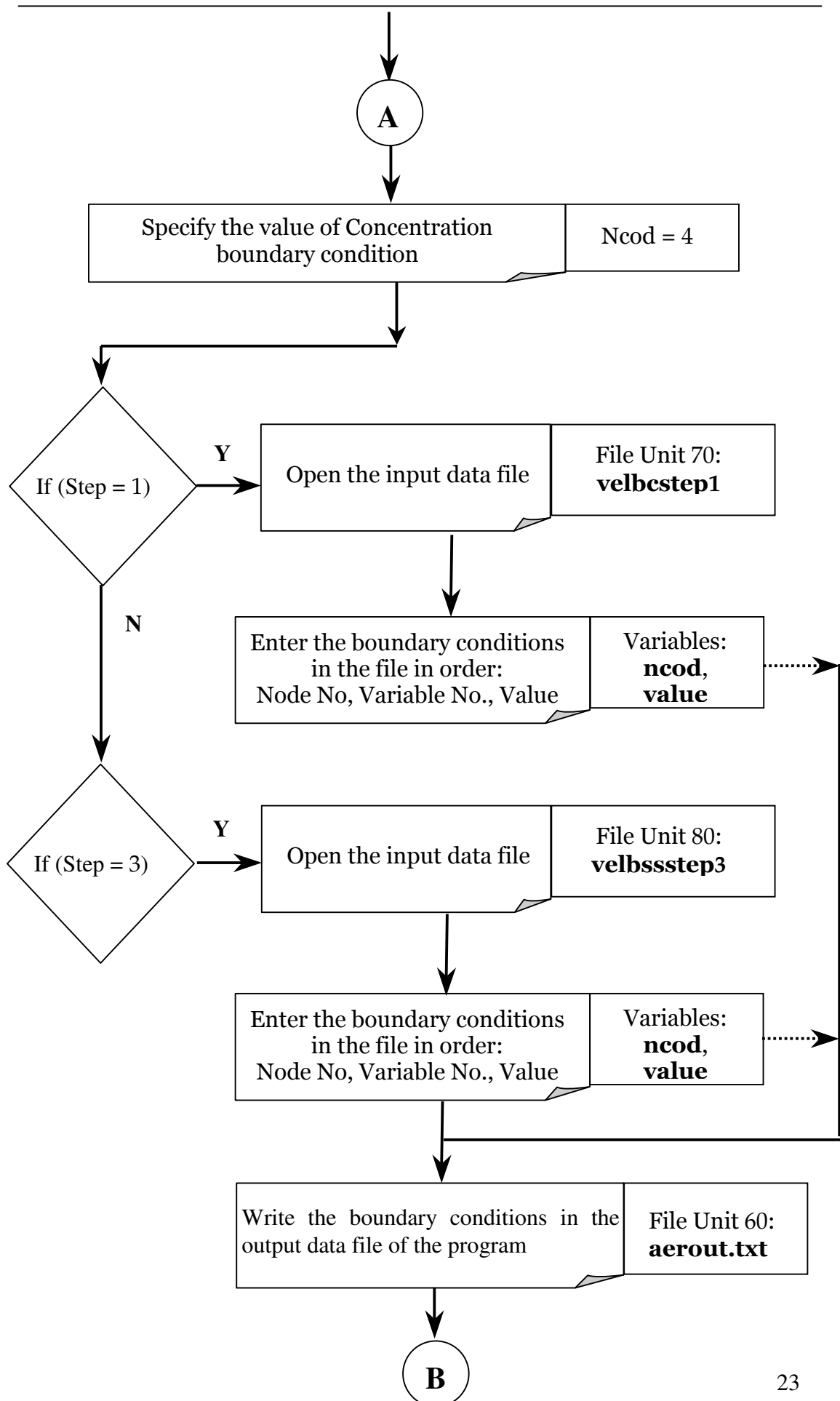


PROGRAM SUBROUTINES - INTERACTIONS

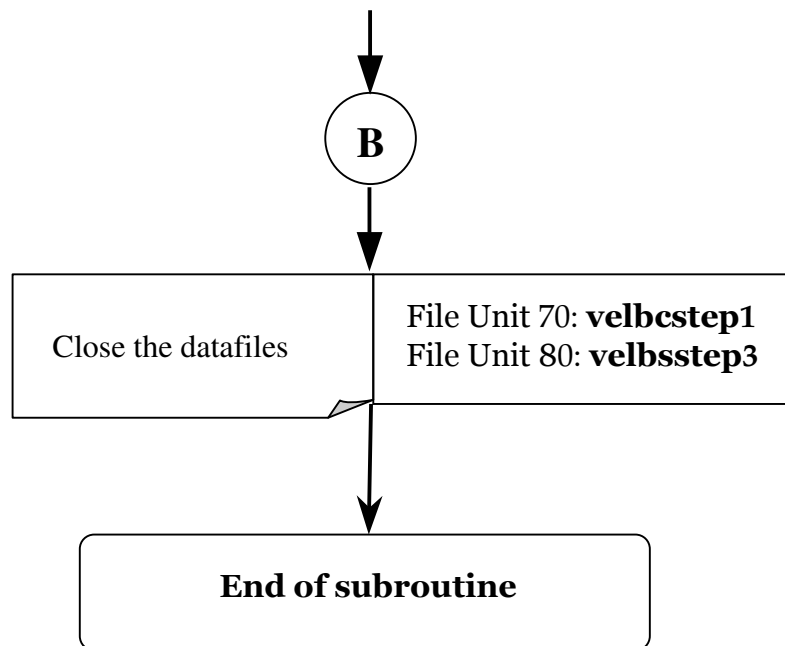
SUBROUTINE HYDROFILTER, LEVEL 1



PROGRAM SUBROUTINES - INTERACTIONS**SUBROUTINE PLEATBC, LEVEL 1**

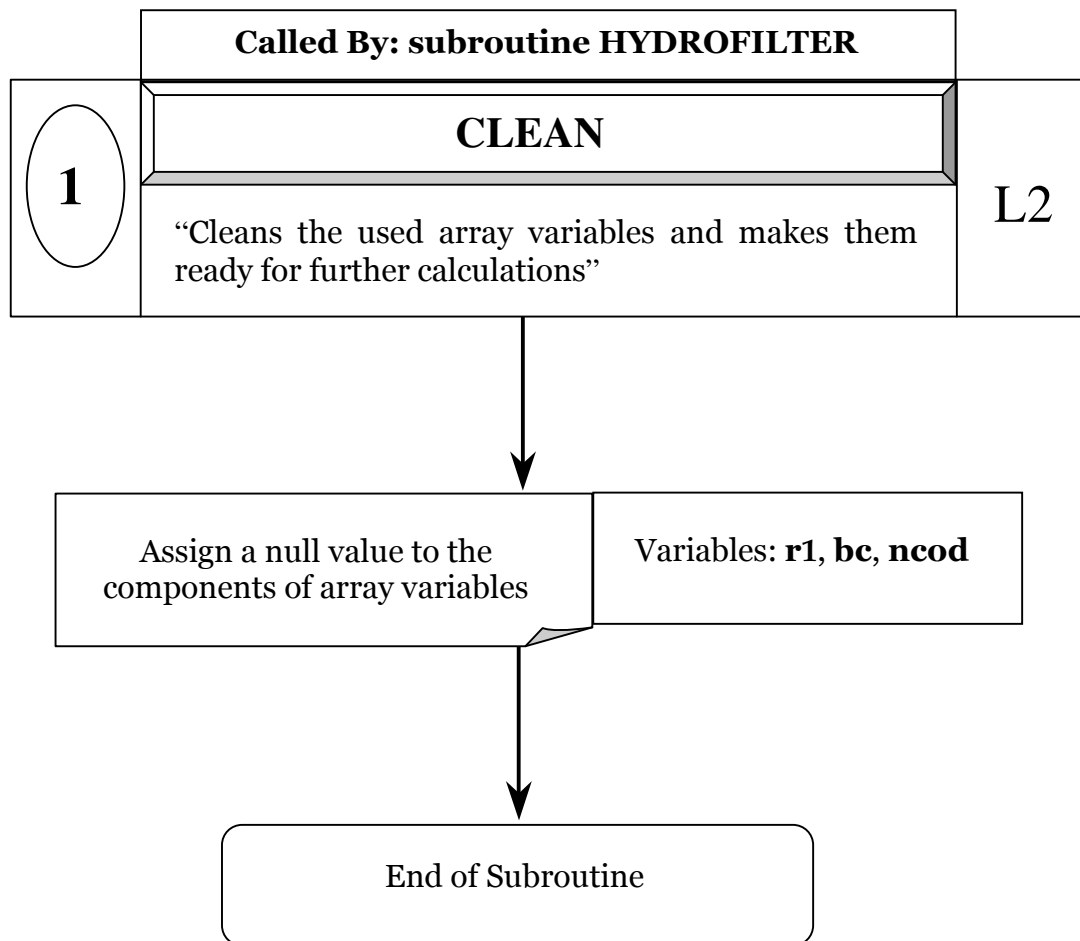
PROGRAM SUBROUTINES - INTERACTIONS

PROGRAM SUBROUTINES - INTERACTIONS



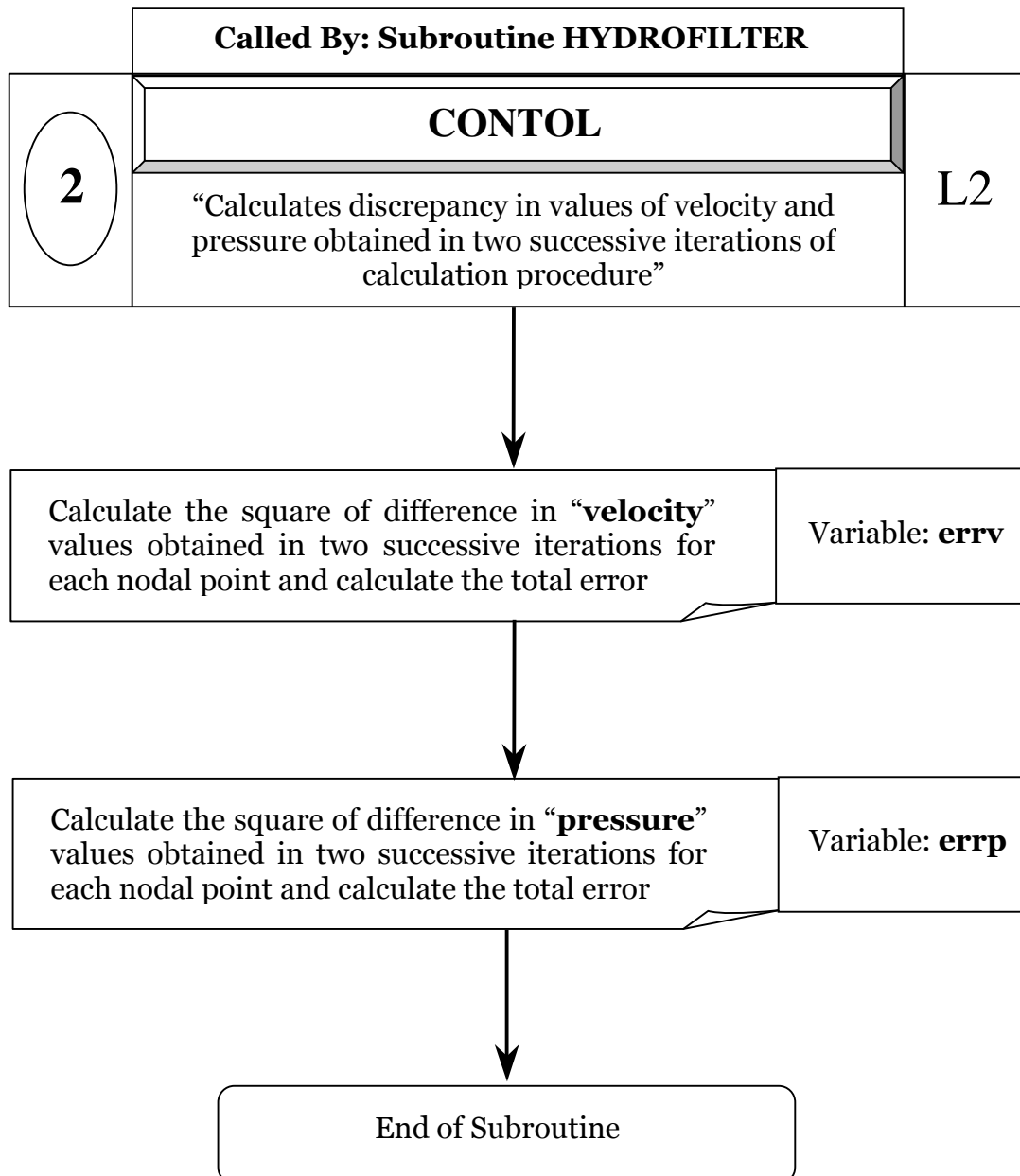
PROGRAM SUBROUTINES - INTERACTIONS

SUBROUTINE CLEAN, LEVEL 2



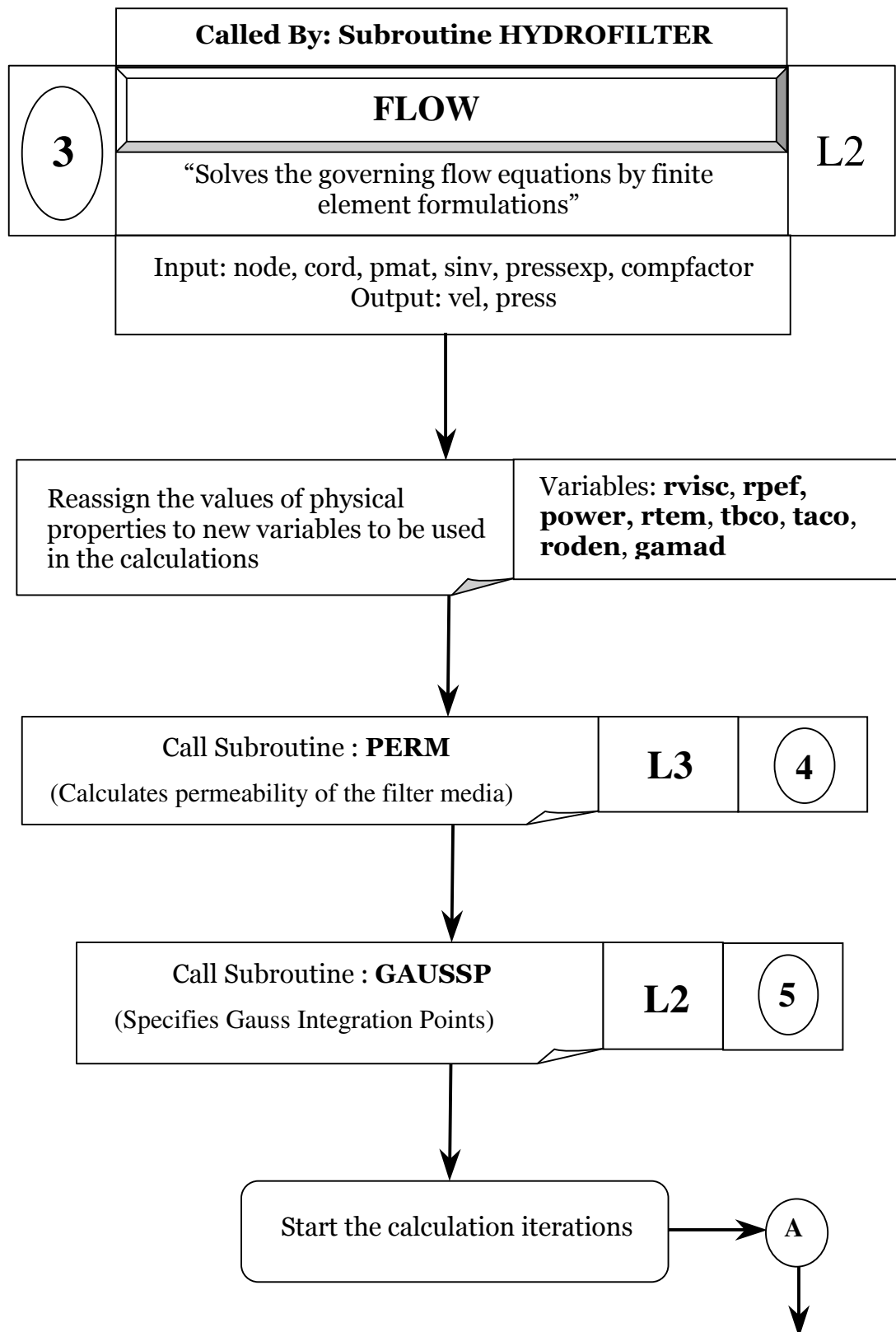
PROGRAM SUBROUTINES - INTERACTIONS

SUBROUTINE CONTOL, LEVEL 2

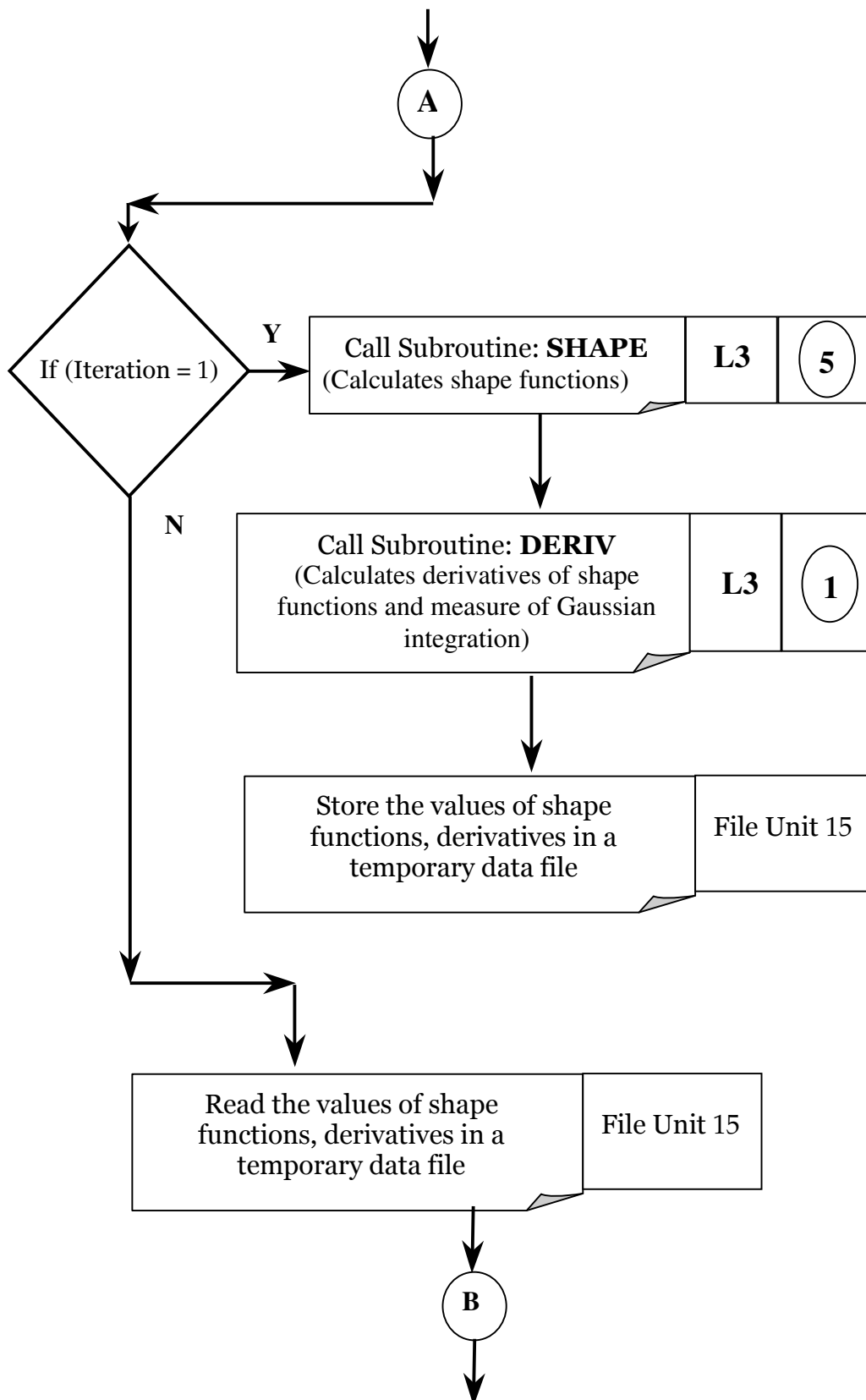


PROGRAM SUBROUTINES - INTERACTIONS

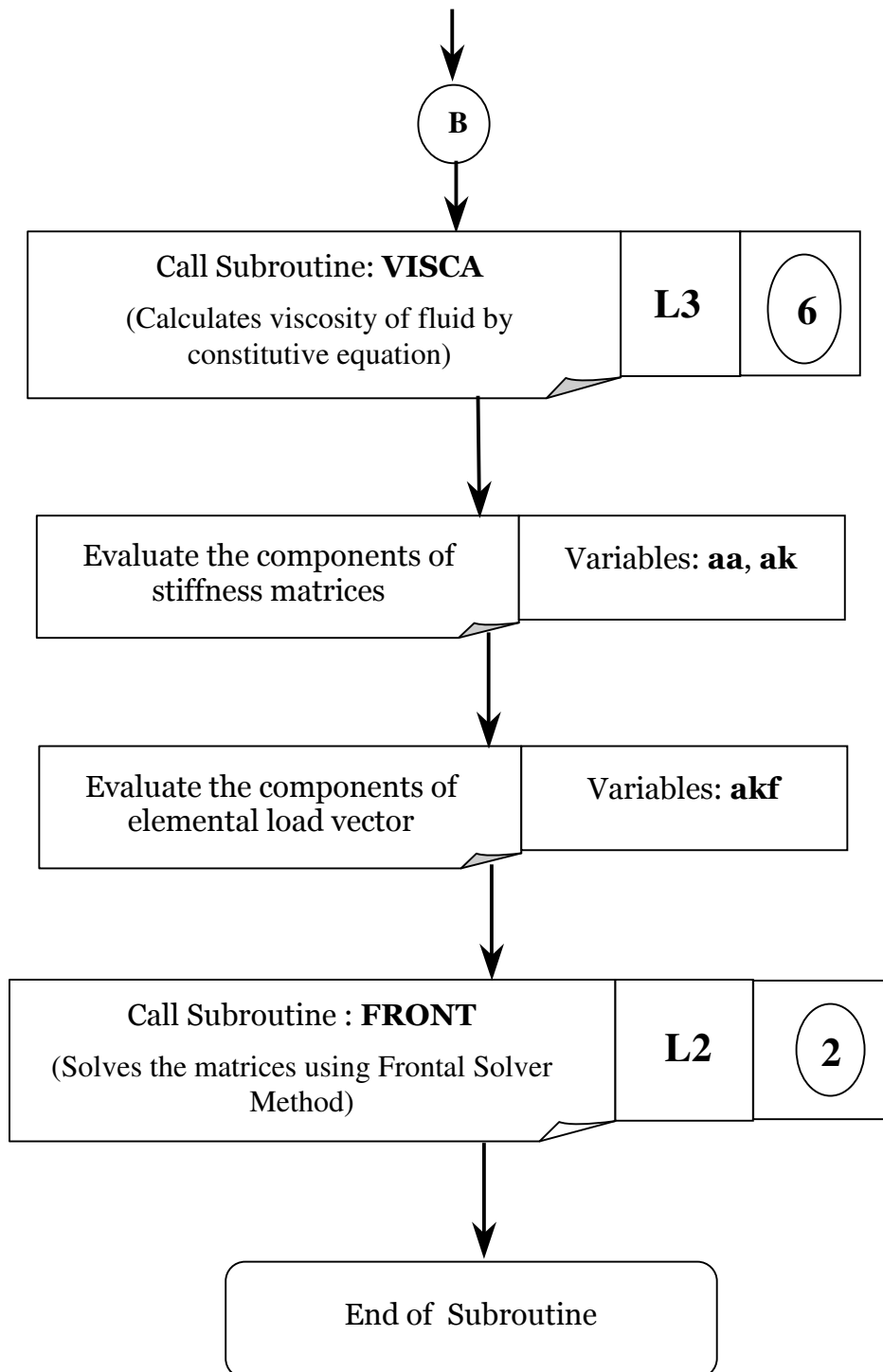
SUBROUTINE FLOW, LEVEL 2



PROGRAM SUBROUTINES - INTERACTIONS

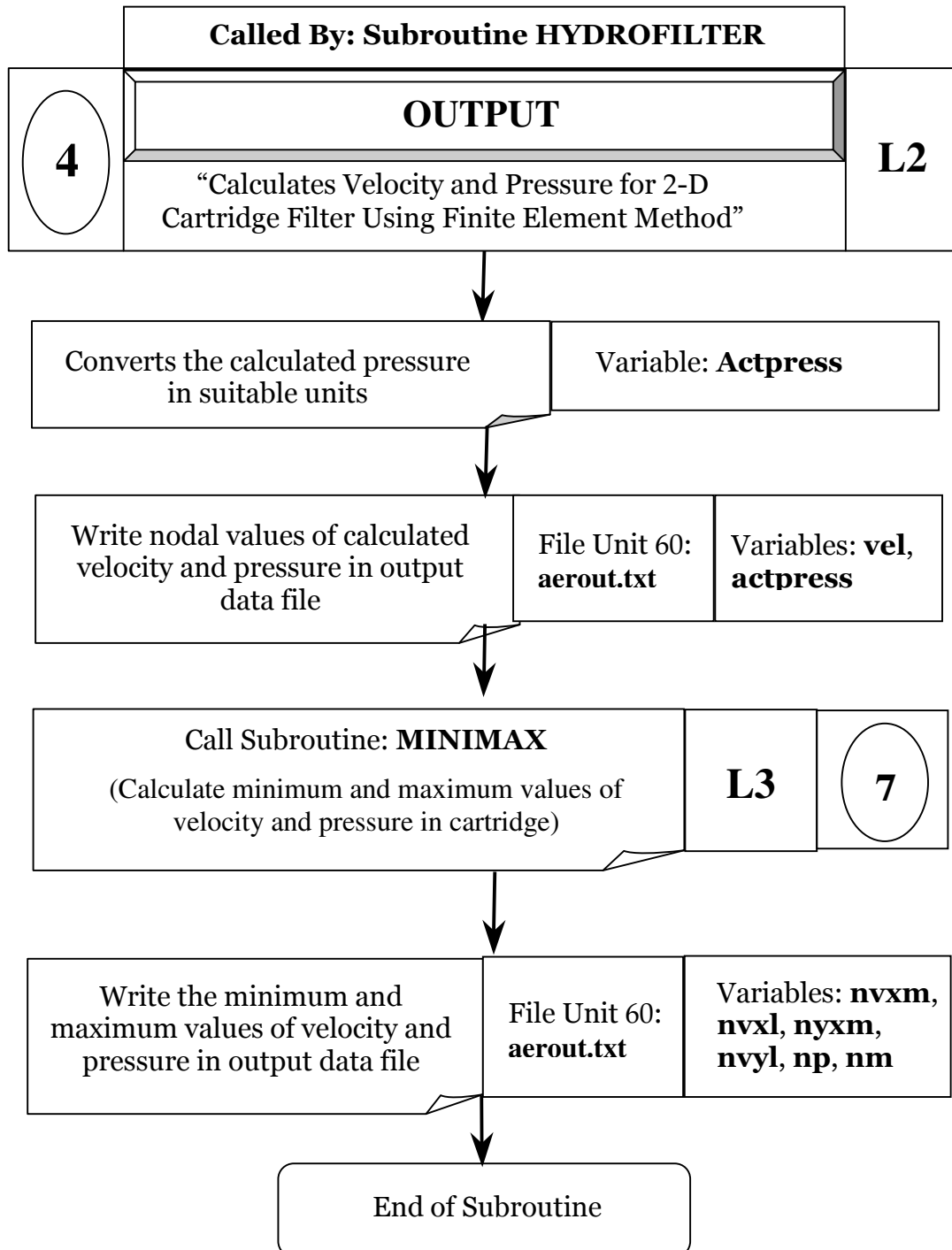


PROGRAM SUBROUTINES - INTERACTIONS



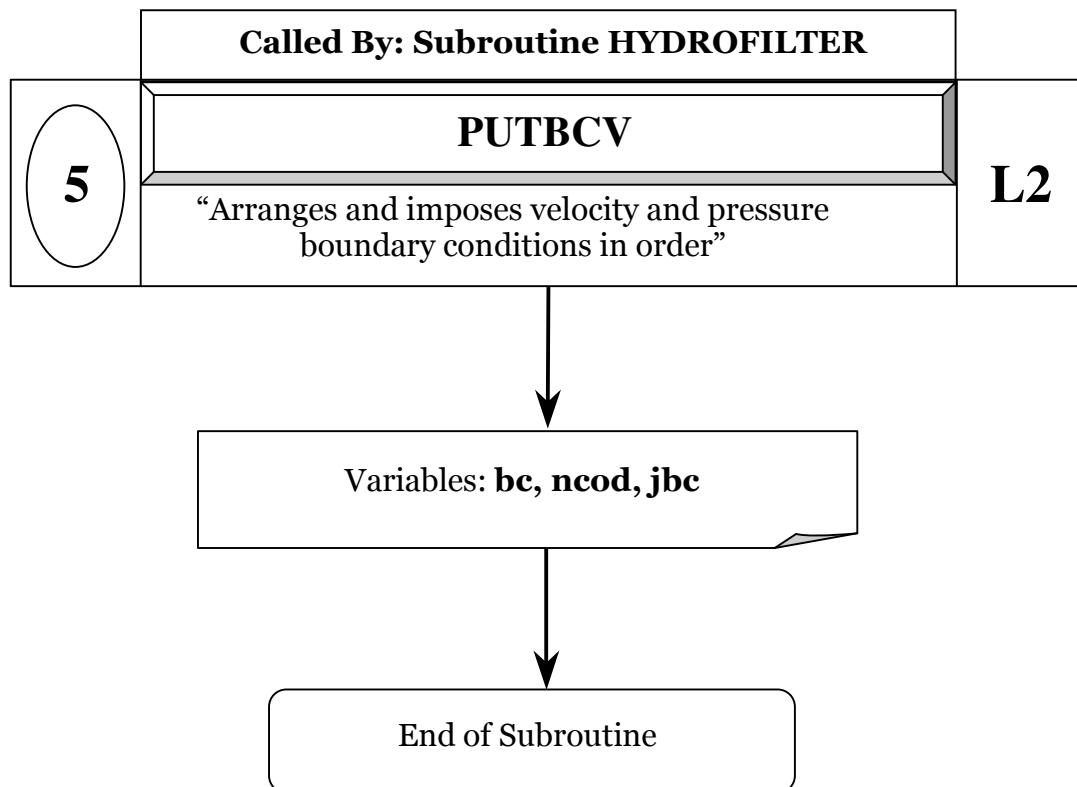
PROGRAM SUBROUTINES - INTERACTIONS

SUBROUTINE OUTPUT, LEVEL 2



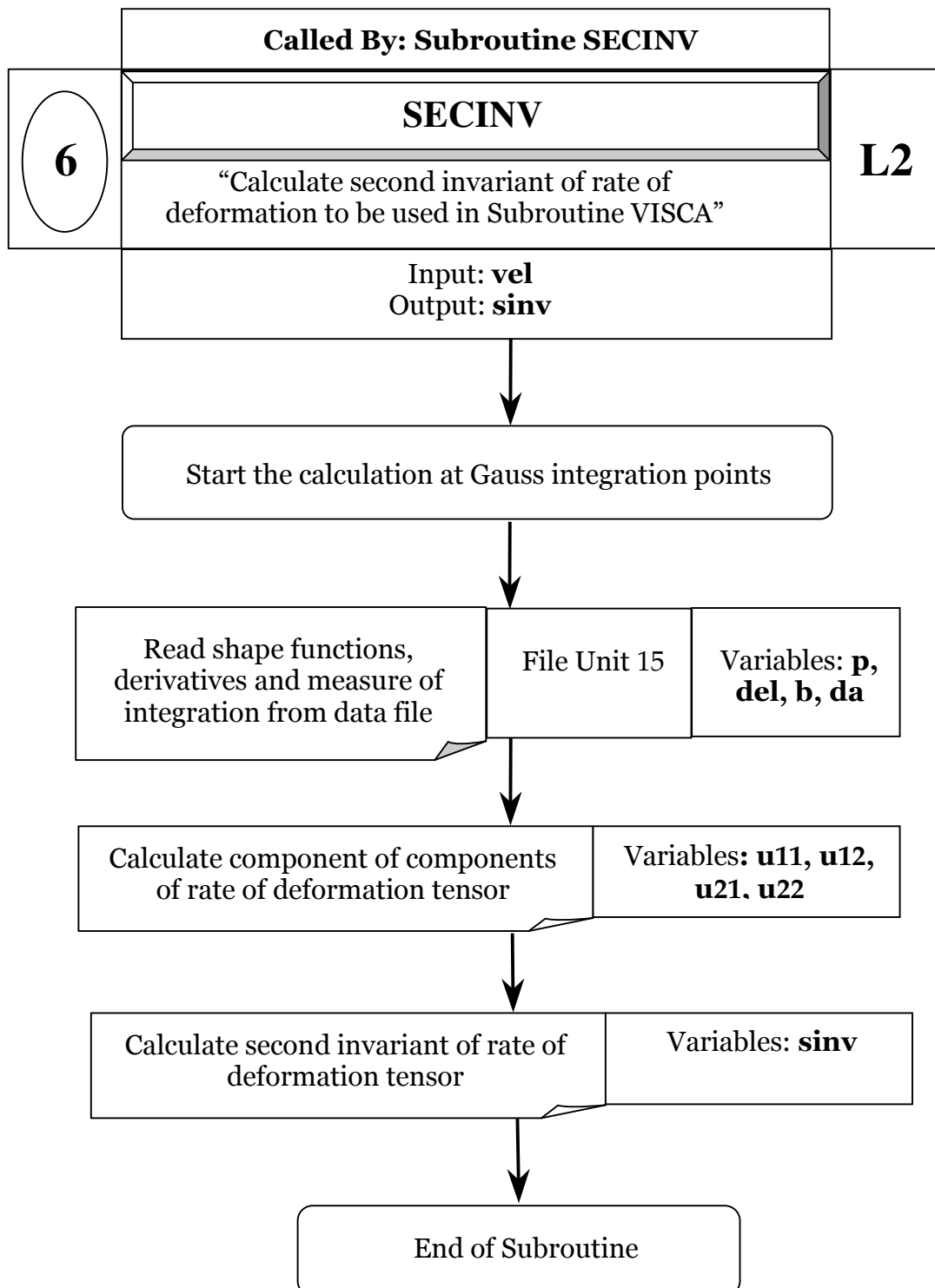
PROGRAM SUBROUTINES - INTERACTIONS

SUBROUTINE PUTBCV, LEVEL 2



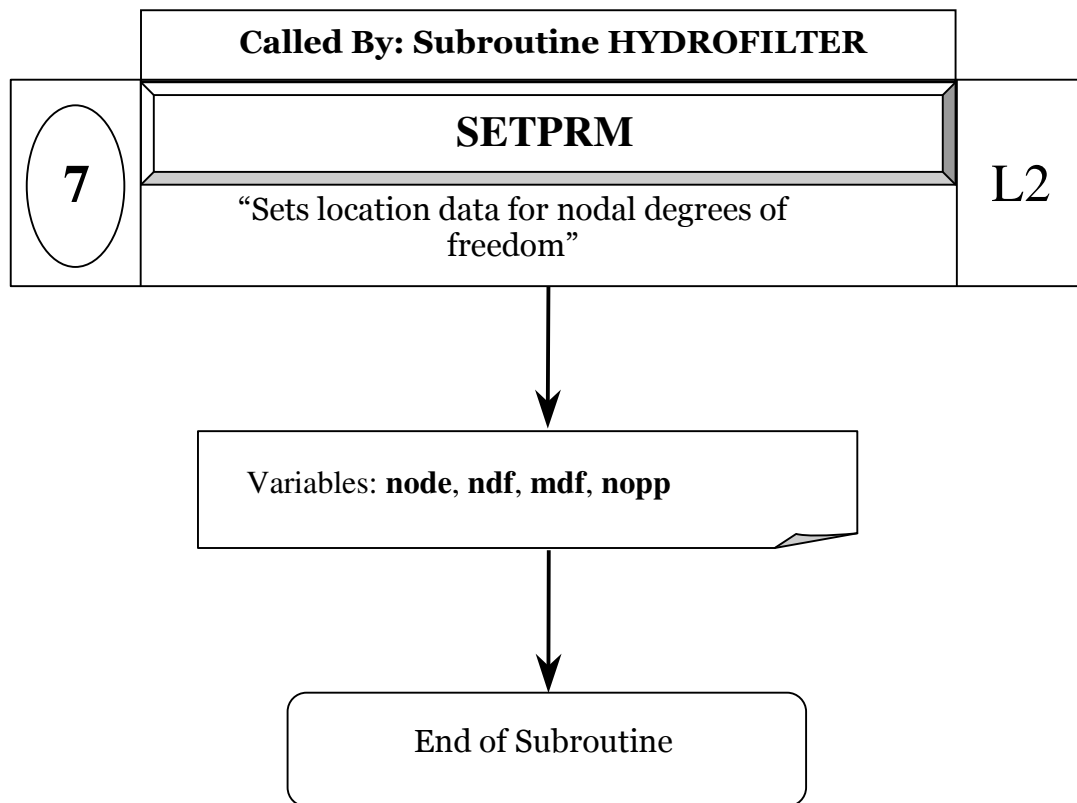
PROGRAM SUBROUTINES - INTERACTIONS

SUBROUTINE SECINV, LEVEL 2



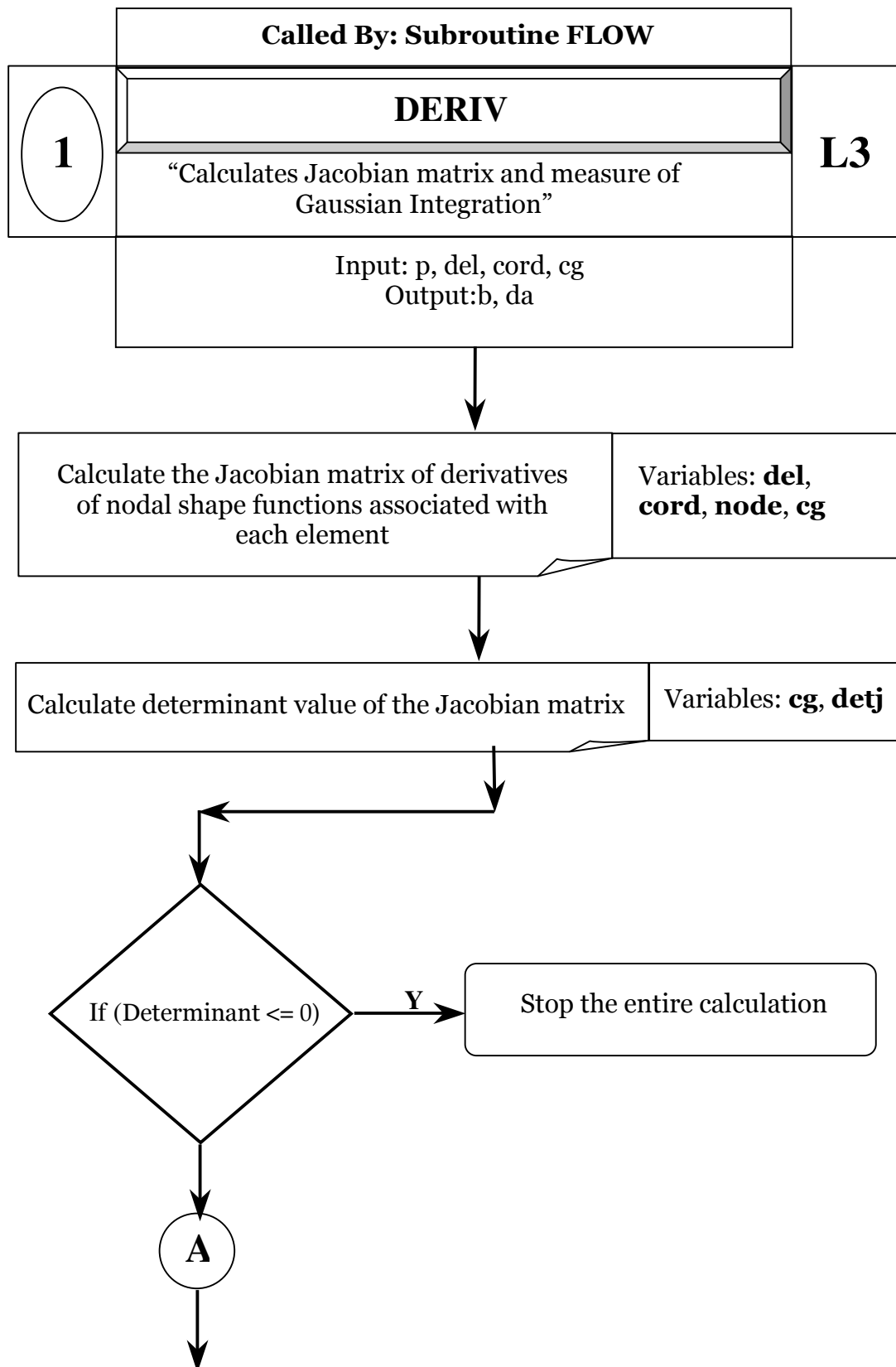
PROGRAM SUBROUTINES - INTERACTIONS

SUBROUTINE SETPRM, LEVEL 2

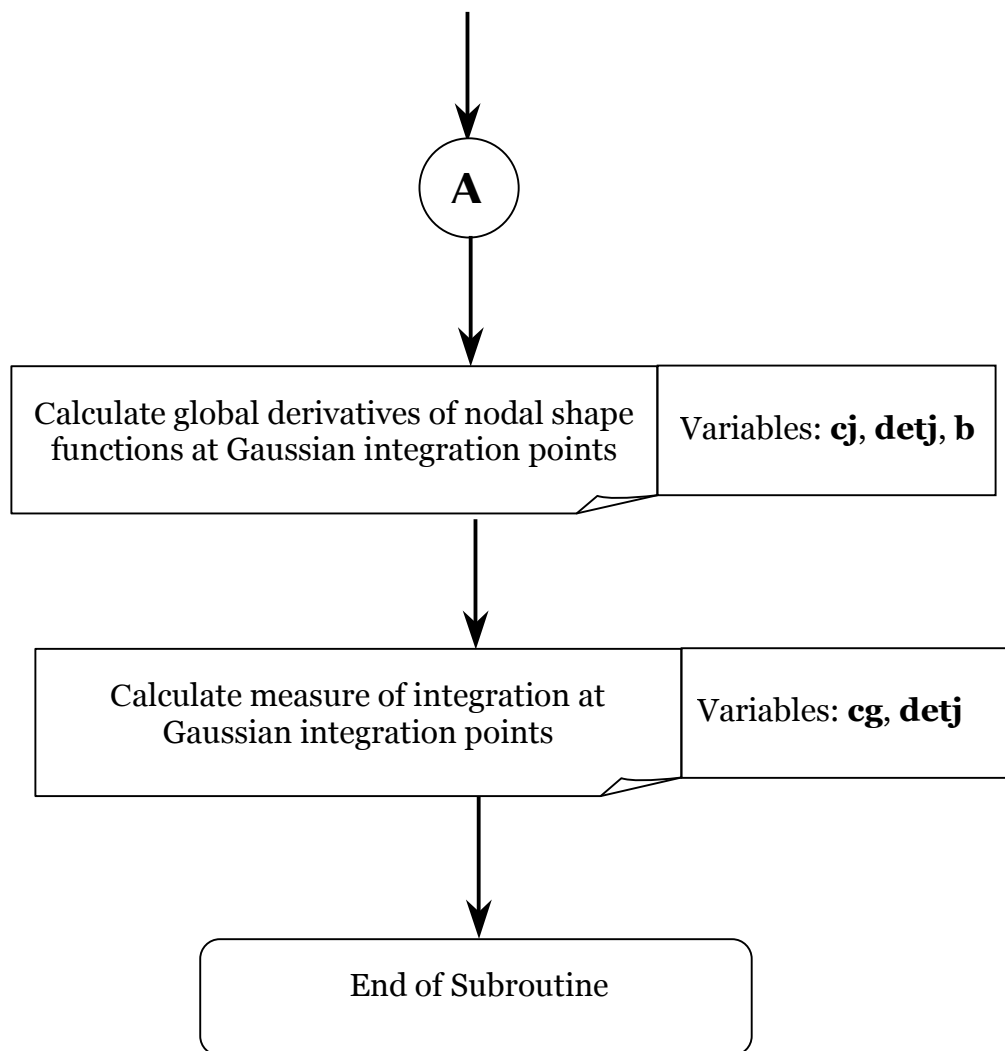


PROGRAM SUBROUTINES - INTERACTIONS

SUBROUTINE DERIV, LEVEL 3

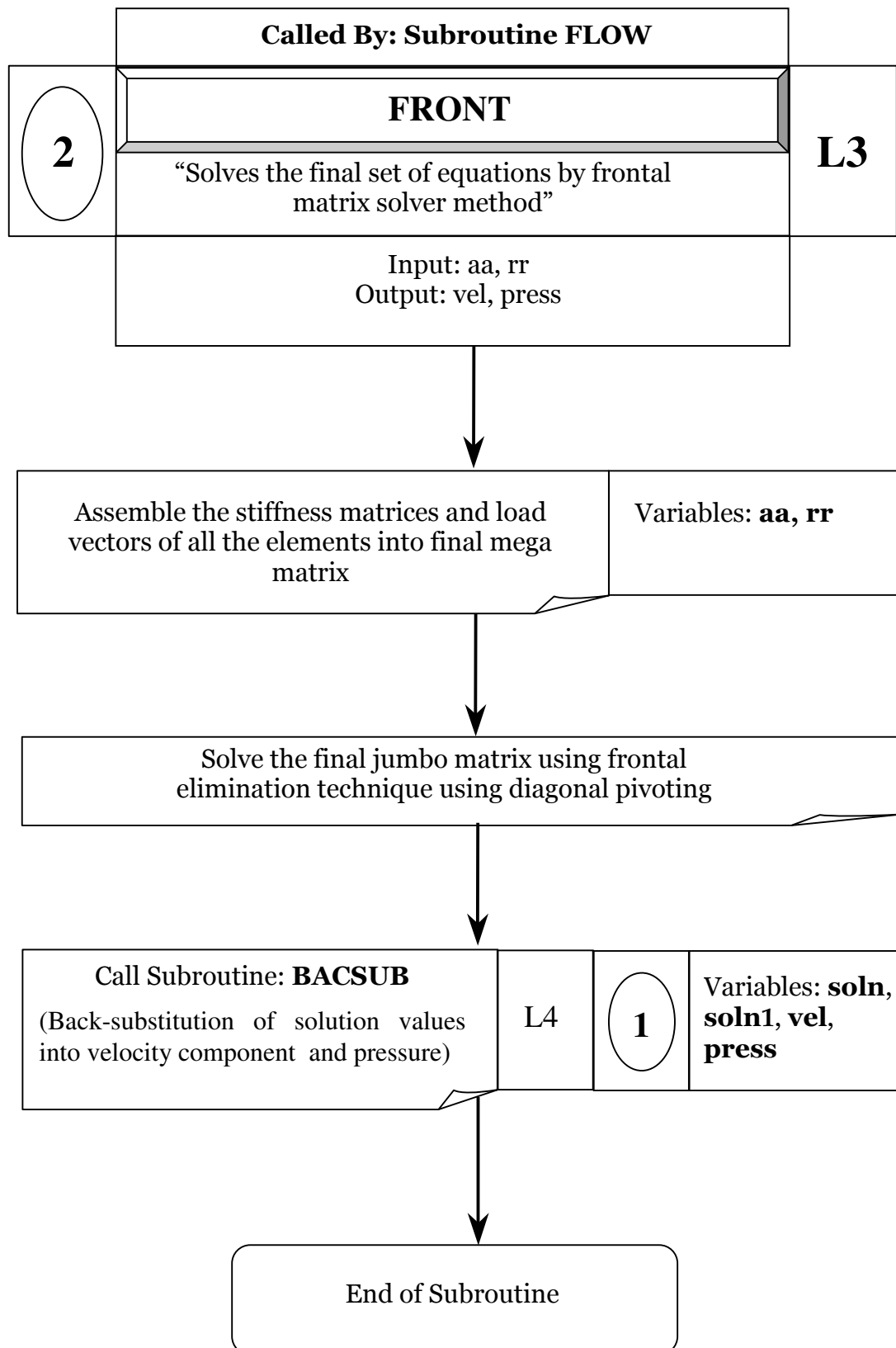


PROGRAM SUBROUTINES - INTERACTIONS



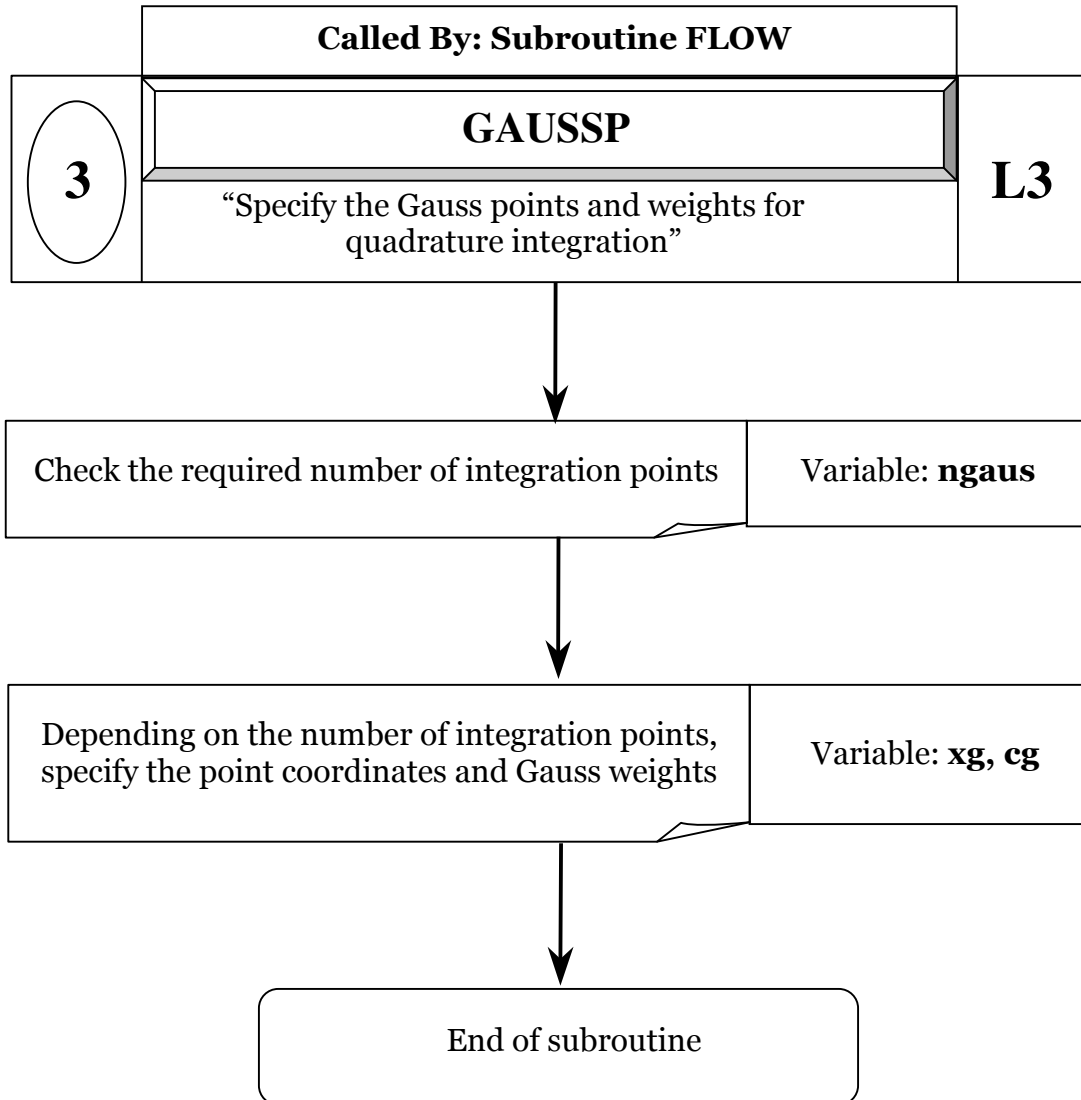
PROGRAM SUBROUTINES - INTERACTIONS

SUBROUTINE FRONT, LEVEL 3



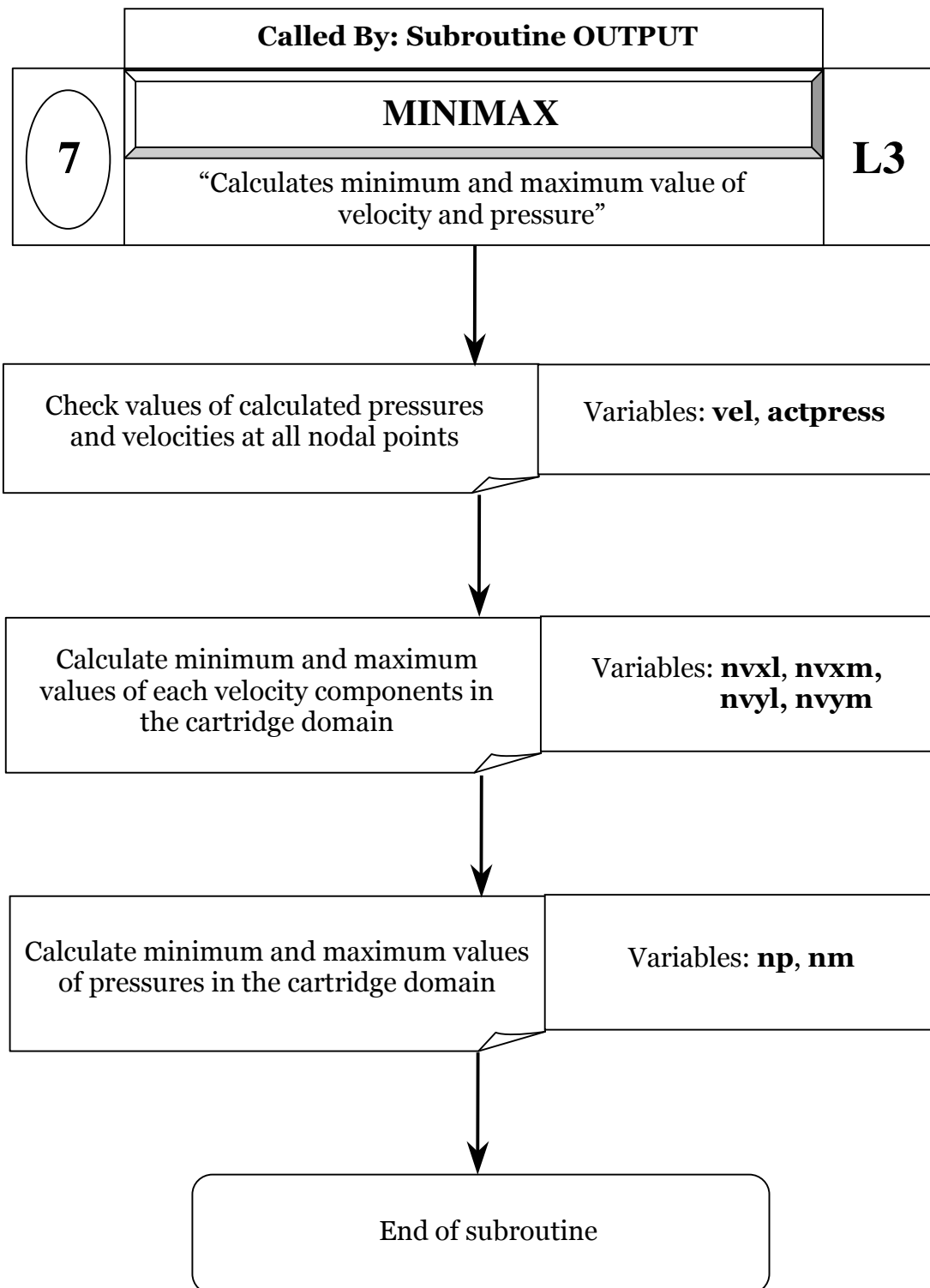
PROGRAM SUBROUTINES - INTERACTIONS

SUBROUTINE GAUSSP, LEVEL 3



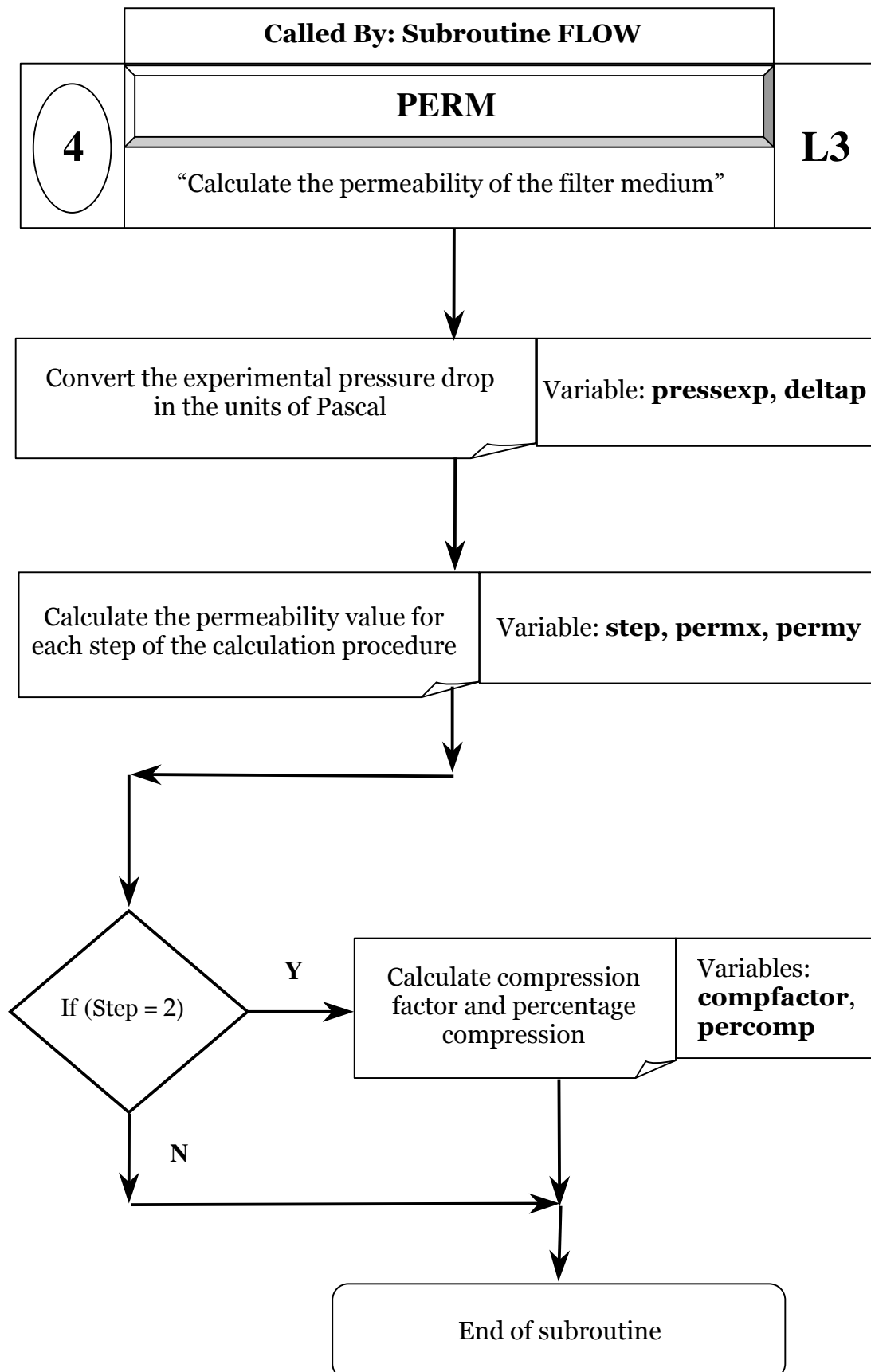
PROGRAM SUBROUTINES - INTERACTIONS

SUBROUTINE MINIMAX, LEVEL 3



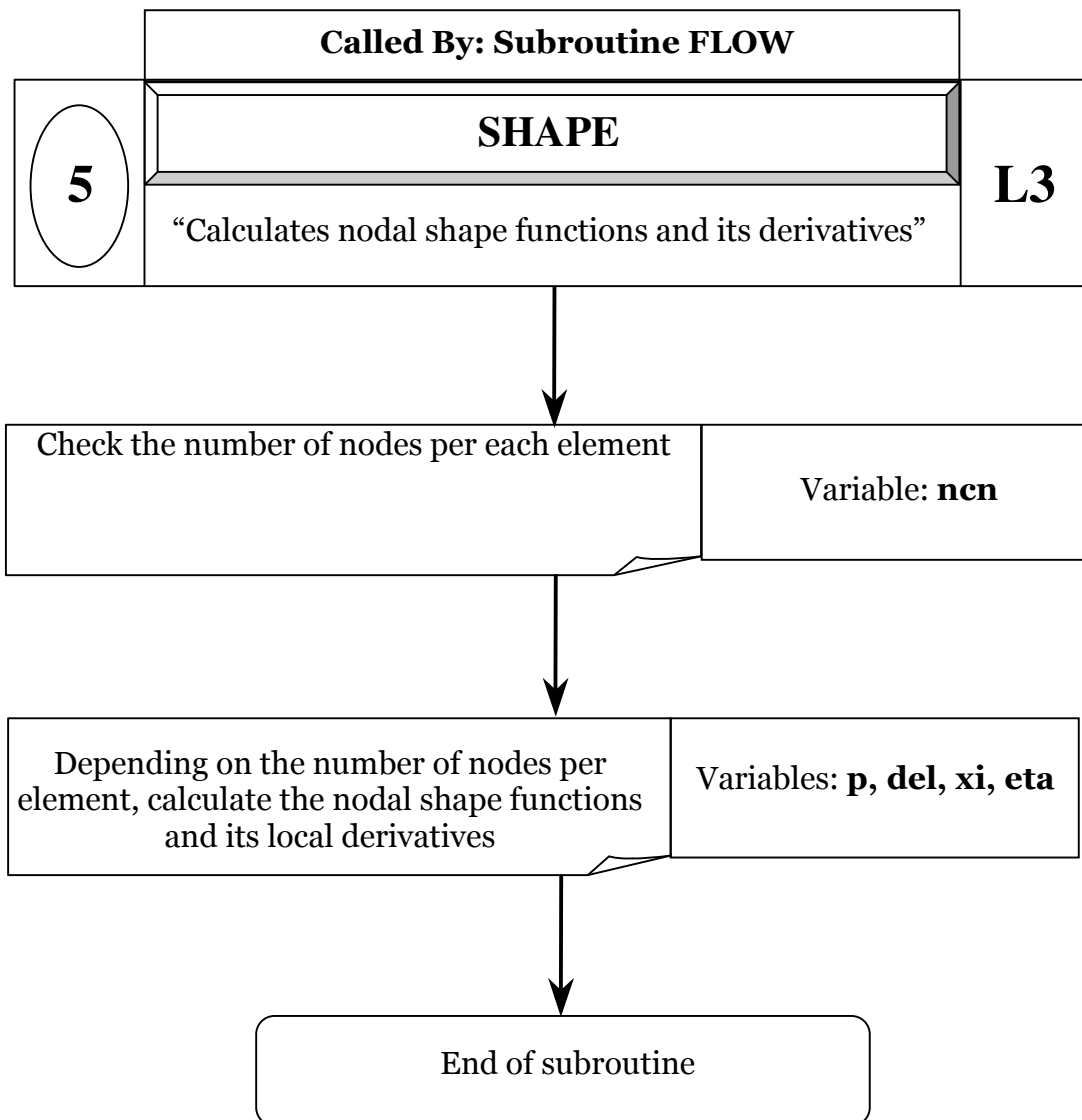
PROGRAM SUBROUTINES - INTERACTIONS

SUBROUTINE PERM, LEVEL 3



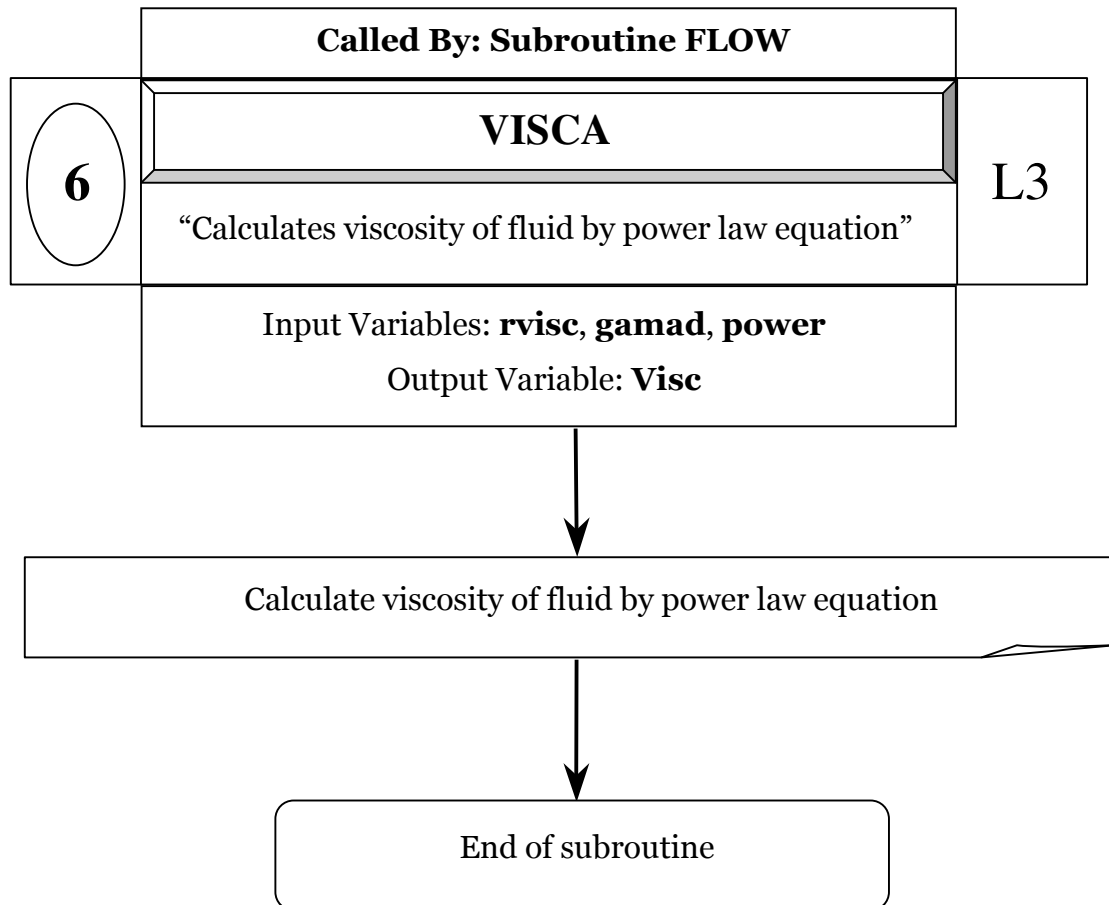
PROGRAM SUBROUTINES - INTERACTIONS

SUBROUTINE SHAPE, LEVEL 3



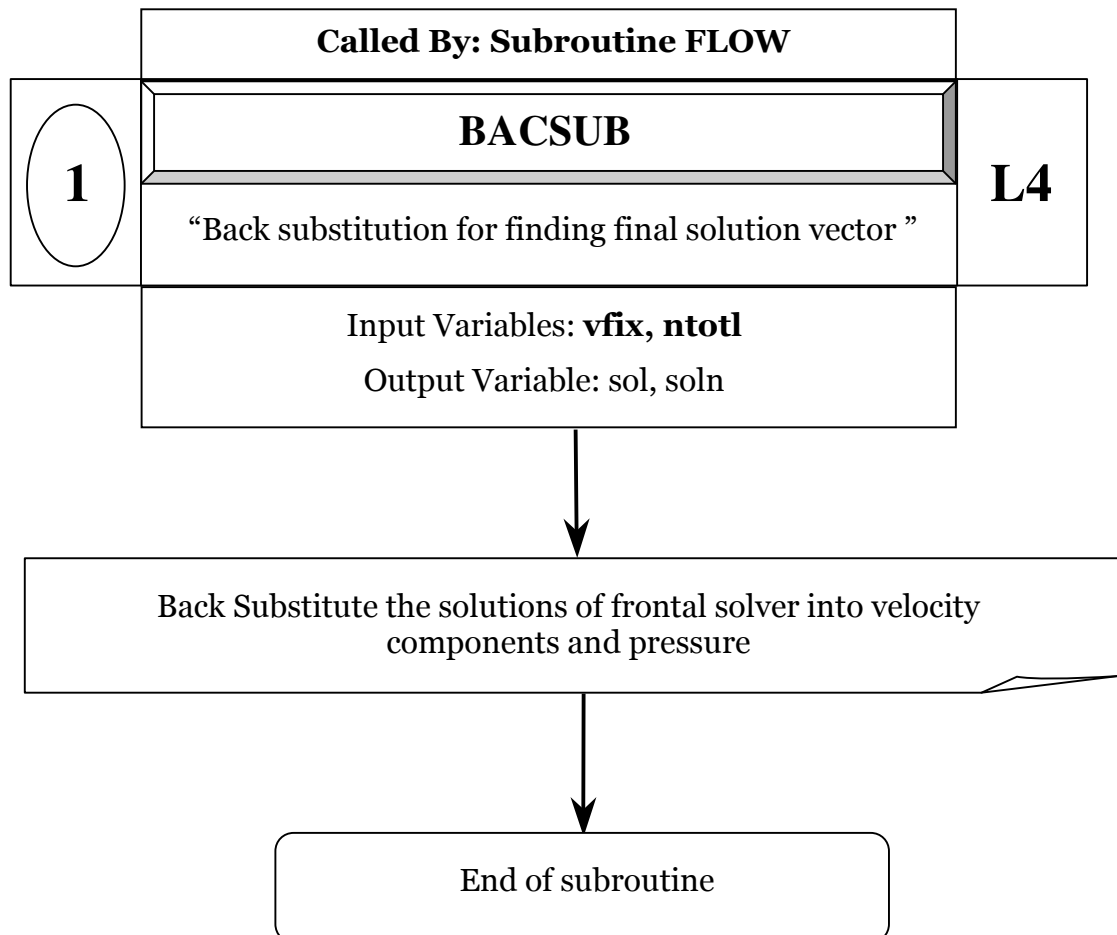
PROGRAM SUBROUTINES - INTERACTIONS

SUBROUTINE VISCA, LEVEL 3



PROGRAM SUBROUTINES - INTERACTIONS

SUBROUTINE BACSUB, LEVEL 4



LISTING OF SOURCE CODES

- 1. ACFAMP**
- 2. Auxilliary Program**

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*****
ACFAMP : Aircraft Cartridge Filter Analysis Modelling Program
Developed by : Navraj S Hanspal & Atul N Waghode
Supervised by : Prof.V.Nassehi & Prof. R.J.Wakeman

Latest Version: 23rd May, 2005

*****
Description
-----
Project Title: 1 AEROFIL 1

TECHNICAL SPECIFICATIONS
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1. The program has been developed using a windows based FORTRAN 90 compiler.
2. This program stores the basic data required for simulating hydrodynamics
   in pleated cartridge filters.
3. This program prompts the user to input the data in form of 3 separate data files.
   (a) Default data file containing nodal connectivity: "df.dat"
   (b) Finite element mesh GPM file
   (c) Reference cartridge ID file generated by auxiliary program "filterdatprep.f"
4. This program is virtually linked with the auxiliary program which generates the
   data file containing the geometrical specifications and the physical data.
5. This is a program for the solution of non-newtonian, isothermal, incompressible fluid
   flow problems in porous media using the weighted residual galerkin finite
   element method.
6. The solution scheme is based on the U-V-P method.
7. Velocity components and pressure are the prime unknowns in the flow field.
8. Pressure gradients inclusive and exclusive of compression and apparent
   loss in filtration area effects can be determined.
9. Percentage compression and loss in area are also evaluated for a given
   cartridge filter specification.
10. Algebraic equations are solved by a frontal method.
11. The program consists of a main module and subroutines.

-----
main work files
-----
unit      contents
-----
1         GPM file for finite element computational mesh
14        used as a work file in the solver routine
15        stores shape functions and their derivatives at
           'full' integration points
51        default data file
60        output file for documentation
61        output file for printing data in excel format
511       input data file containing cartridge characteristic data

-----
List of variables
-----
da:        Left hand side finite element stiffness matrix
acpress:   Normalised value of nodal pressure
alpha:     Time-stepping parameter

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ak:        Right hand side finite element stiffness matrix
areabase:  percentage loss in area factor
bc:        Measure of Gaussian integration
cartrid:   Array for storing boundary constraint value
cg:        Reference ID for each filter cartridge element
comfactor: Weighting functions for Gauss integration
cord:      Compression factor for filter medium
da:        Array storing coordinate values of each nodal point
del:       Local derivatives of shape function
delap:     Experimental pressure drop
deltat:    Value of time step used in calculation iterations
density:   Density of fluid used for each set of experiment
del:       Determinant of Jacobian matrix
dl:        Diameter of inner core of the filter cartridge element
el:        Length of pleat
enp:       Number of plates in each filter cartridge element
enrp:       Square of discrepancy between pressure values calculated
            in two successive iterations
ery:       Square of discrepancy between velocity values calculated
            in two successive iterations
etax:      Y-coordinate in local coordinate system
excel:     Array for storing simulated values of pressure drop in
            each step of calculation procedure
farea:     Filtering surface area of cartridge
frate:     Flow rate values for each experiment
gamad:     Rate of deformation of viscous stress tensor
guesp:     Pressure drop with compression and loss in area
hp:        Height of filter cartridge element
icord:     Switch for changing the coordinate system of
            equations
mabc:      Limit for maximum number of boundary constraints
            that can be specified
maxdf:     Limit for maximum number of nodal degrees of freedom
maxel:     Limit for maximum number of elements in mesh
maxmp:     Limit for maximum number of nodal points in mesh
maxnp:     Maximum dimension of finite element stiffness matrix
nbc:       Total number of boundary-node constraints
nci:       Number of nodes associated with each finite element
ncod:      Array for constraint switch defined for every degree
            of freedom
ndf:       Total number of nodal degrees of freedom
ndim:      Dimensions of the solution domain
nel:       Total number of elements in pleated cartridge mesh
ngaus:     Number of quadrature points required for Gaussian integration
nmat:      Total number of fluids
nmp:       Array for nodal connectivity of elements
nnc:       Number of sets of experiment
nter:      Number of integration iterations
num:       Number of integration points per element
p:         Finite element shape or interpolation functions
pd:        Experimental pressure value for each set of data
percomp1:  Percentage value of filter medium compression
percomp2:  Permeability of filter medium without compression
permx:     Permeability of the filter medium in x-direction
permy:     Permeability of the filter medium in y-direction
pmt:       Array storing values of physical properties of the fluid
power:     Power law index for the fluid viscosity
press:     Array for nodal pressure
presexp:   Experimental pressure drop
pzelt:     Reference pressure
rr:        Array for storing the elemental load vector
rrtem:     Reference temperature
rvisc:     Consistency coefficient for viscosity of fluid
slnv:      Array storing components of second invariant of rate of
            deformation of stress tensor
soln:      Array for storing solution values calculated by Frontal Solver
step:      Stage of the calculation procedure
tacc:      Coefficient a in the power law model
tbo:       Coefficient b in the power law model
time:      Amount of time for iterations
tolp:      Maximum allowable tolerance for fluctuation in pressure value
tolv:      Maximum allowable tolerance for fluctuation in velocity value
vel:       Velocity for nodal elements
velcartrid: Array for fluid through filter media
velofluid: Velocity of fluid in fluid
visc:      Viscosity of fluid used for each set of experiment
visc:      Undated value of viscosity according to power law model
xg:        Coordinates of Gauss quadrature points for integration
xi:        X-coordinate in local coordinate system

```

```
C Opening of input and output data files
C =====
C This data file contains the Numerical Parameters and Nodal Connectivity
C -----
    print *, *
    1 * * * * *
    print *, *
    1 *
    1 print *, "          #####           # # #####      **
    1 print *, "          # # #           # # ## ## #     **
    1 print *, "          # # #           # # ## ## #     **
    1 print *, "          # # #           # # ## ## #     **
    1 print *, "          # # #           # # ## ## #     **
    1 print *, "          ##### #         # ##### # # #   **
    1 print *, "          # # #           # ##### # # #   **
    1 print *, "          # # #           # # # # #       **
    1 print *, "          # ##### #         # # # # #       **
    1 print *, *
    1 print *, *
    1 print *, "
    1 print *, " May 2005
    1 print *, "
    1 print *, *
    1 * * * * *
write(*, 1101)
write(*, 1111)
write(*, 1121)
write(*, 1131)
    print *, *
    1 Program Developers: N.S. Hanspal and A.N. Waghode*
    1 print *, *
    1 Project Advisors: Prof. R.J. Wakeman and Prof. V. Masashi*
    1 print *, *
    1 Advanced Separation Technologies Group*
    1 print *, " Department of Chemical Engineering"
    1 print *, " Loughborough University*"
    1 print *, " Loughborough, Leicestershire*"
    1 print *, " LE11 3TU, United Kingdom"
    write(*, 1131)
    write (*, 1101)
=====
print*, 'Enter the name of DEPAULR data file'
read(*,2000) filename
open(unit=51, file=filename, access='sequential', form='formatted',
1 status='unknown', iostat=iost)
This is the output file containing the results
-----
open(unit=60, file='aerout.txt', access='sequential', form='formatted',
1 status='unknown', iostat=iost)
open(unit=61, file='excel.txt', access='sequential', form='formatted',
1 status='unknown', iostat=iost)
These are scratch files used in computation
C
```

17

9

```

close(unit = 15)
close(unit = 20)
close(unit = 51)
close(unit = 51)
close(unit = 61)
close(unit = 70)
close(unit = 70)
close(unit = 511)

=====
print statements
=====

format(' ','')
format('/', 'ACPAMP calculates percentage compression of the
impermeable media ',' and predicts pressure drop across pleated
flatridge filters ',' including effects of compression and losses
in effective filtration area')
format(' ', 2(/))

format" " *****
1*****

Read statements
=====

format(a)
format(80a)
format(215)
format(415)
format(215)
format(2210.0)
format(3210.5)

=====
Write statements
=====

format(' ', 5(/), ' ', 20x, 60(' '), ' ', 20x, ' ', 58x, ' ', /
1', 20x, ' ', ' ', A two dimensional finite element model of a
225x, ' ', ' ', 20x, ' ', non-newtonian isothermal flow using '
330x, ' ', ' ', 20x, ' ', the UVP method, ' ', 39x, ' ', ' ', 20x, ' ',
558x, ' ', ' ', 20x, 60(' ')//, ' ', 20x, 80a, / ' ',
650x, 80(' '), //)

format(' ', 20x, 3(' '), ' element description data', 10(' '), /
1225x, 'no. of nodes per element
=, 110, /
format(' ', 10(' '), 'input data unacceptable', 10(' '), //)

format(' ' *** coordinate system is cartesian (planar) ***')
format('*** coordinate system is cylindrical (axisymmetric) ***')
format(' ', 10(' '), 'input data unacceptable', 10(' '), //)

format(' ', 20x, 3(' '), ' mesh description data ', 10(' '), /
125x, 'no. of nodal points
=, 110, /
225x, 'no. of elements
=, 110, /
125x, 'no. of nodal constraints on boundary
=, 110, /
225x, 'no. of different materials
=, 110, //)

format('////TIME STPP no., 15, //)
format(15, 2e13, 4)
format(5e13, 4)

=====
end program
=====

=====
START OF SUBROUTINES
=====

subroutine gaussp(ngaus, xv, cy)

implicit double precision(a-h,o-z)

```

```

c
c x(g) specifies the coordinates of the Gauss points
c (g) specifies the Gauss weights
c
dimension xg(3), cg(3)

if (ngaus.eq.1) then
  xg(1)=0.0
  cg(1)=2.0
else if (ngaus.eq.2) then
  xg(1) = 0.57735026919d00
  xg(2) = -xg(1)
  cg(1) = 1.00
  cg(2) = 1.00
else
  xg(1) = 0.77459666924d00
  xg(2) = 0.0
  xg(3) = -xg(1)
  cg(1) = 0.55555555556d00
  cg(2) = 0.88888888889d00
  cg(3) = cg(1)
endif
return
end

=====
c
c subroutine shape (xi, eta, p, del, ncn)
c implicit double precision (a-h,o-z)
c
dimension p(9), del(2,9)
if (non.eq.4) then
  del(1,1)=0.25*(1-eta)
  del(1,2) = 0.25*(1-eta)
  del(1,3) = 0.25*(1+eta)
  del(1,4)=0.25*(1+eta)
  del(2,1)=0.25*(1-xi)
  del(2,2)=-0.25*(1-xi)
  del(2,3) = 0.25*(1-xi)
  del(2,4) = 0.25*(1-xi)
  del(2,5)=0.25*(1-xi)
  del(2,6)=0.25*(1-xi)
  del(2,7)=0.25*(1-xi)
  del(2,8)=0.25*(1-xi)
  del(2,9)=0.25*(1-xi)
  del(2,10)=0.25*(1-xi)
  del(2,11)=0.25*(1-xi)
  del(2,12)=0.25*(1-xi)
  del(2,13)=0.25*(1-xi)
  del(2,14)=0.25*(1-xi)
  del(2,15)=0.25*(1-xi)
  del(2,16)=0.25*(1-xi)
  del(2,17)=0.25*(1-xi)
  del(2,18)=0.25*(1-xi)
  del(2,19)=0.25*(1-xi)
  del(2,20)=0.25*(1-xi)
  del(2,21)=0.25*(1-xi)
  del(2,22)=0.25*(1-xi)
  del(2,23)=0.25*(1-xi)
  del(2,24)=0.25*(1-xi)
  del(2,25)=0.25*(1-xi)
  del(2,26)=0.25*(1-xi)
  del(2,27)=0.25*(1-xi)
  del(2,28)=0.25*(1-xi)
  del(2,29)=0.25*(1-xi)
  del(2,30)=0.25*(1-xi)
  del(2,31)=0.25*(1-xi)
  del(2,32)=0.25*(1-xi)
  del(2,33)=0.25*(1-xi)
  del(2,34)=0.25*(1-xi)
  del(2,35)=0.25*(1-xi)
  del(2,36)=0.25*(1-xi)
  del(2,37)=0.25*(1-xi)
  del(2,38)=0.25*(1-xi)
  del(2,39)=0.25*(1-xi)
  del(2,40)=0.25*(1-xi)
  del(2,41)=0.25*(1-xi)
  del(2,42)=0.25*(1-xi)
  del(2,43)=0.25*(1-xi)
  del(2,44)=0.25*(1-xi)
  del(2,45)=0.25*(1-xi)
  del(2,46)=0.25*(1-xi)
  del(2,47)=0.25*(1-xi)
  del(2,48)=0.25*(1-xi)
  del(2,49)=0.25*(1-xi)
  del(2,50)=0.25*(1-xi)
  del(2,51)=0.25*(1-xi)
  del(2,52)=0.25*(1-xi)
  del(2,53)=0.25*(1-xi)
  del(2,54)=0.25*(1-xi)
  del(2,55)=0.25*(1-xi)
  del(2,56)=0.25*(1-xi)
  del(2,57)=0.25*(1-xi)
  del(2,58)=0.25*(1-xi)
  del(2,59)=0.25*(1-xi)
  del(2,60)=0.25*(1-xi)
  del(2,61)=0.25*(1-xi)
  del(2,62)=0.25*(1-xi)
  del(2,63)=0.25*(1-xi)
  del(2,64)=0.25*(1-xi)
  del(2,65)=0.25*(1-xi)
  del(2,66)=0.25*(1-xi)
  del(2,67)=0.25*(1-xi)
  del(2,68)=0.25*(1-xi)
  del(2,69)=0.25*(1-xi)
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  del(2,75)=0.25*(1-xi)
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  del(2,78)=0.25*(1-xi)
  del(2,79)=0.25*(1-xi)
  del(2,80)=0.25*(1-xi)
  del(2,81)=0.25*(1-xi)
  del(2,82)=0.25*(1-xi)
  del(2,83)=0.25*(1-xi)
  del(2,84)=0.25*(1-xi)
  del(2,85)=0.25*(1-xi)
  del(2,86)=0.25*(1-xi)
  del(2,87)=0.25*(1-xi)
  del(2,88)=0.25*(1-xi)
  del(2,89)=0.25*(1-xi)
  del(2,90)=0.25*(1-xi)
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  del(2,92)=0.25*(1-xi)
  del(2,93)=0.25*(1-xi)
  del(2,94)=0.25*(1-xi)
  del(2,95)=0.25*(1-xi)
  del(2,96)=0.25*(1-xi)
  del(2,97)=0.25*(1-xi)
  del(2,98)=0.25*(1-xi)
  del(2,99)=0.25*(1-xi)
  del(2,100)=0.25*(1-xi)
  del(2,101)=0.25*(1-xi)
  del(2,102)=0.25*(1-xi)
  del(2,103)=0.25*(1-xi)
  del(2,104)=0.25*(1-xi)
  del(2,105)=0.25*(1-xi)
  del(2,106)=0.25*(1-xi)
  del(2,107)=0.25*(1-xi)
  del(2,108)=0.25*(1-xi)
  del(2,109)=0.25*(1-xi)
  del(2,110)=0.25*(1-xi)
  del(2,111)=0.25*(1-xi)
  del(2,112)=0.25*(1-xi)
  del(2,113)=0.25*(1-xi)
  del(2,114)=0.25*(1-xi)
  del(2,115)=0.25*(1-xi)
  del(2,116)=0.25*(1-xi)
  del(2,117)=0.25*(1-xi)
  del(2,118)=0.25*(1-xi)
  del(2,119)=0.25*(1-xi)
  del(2,120)=0.25*(1-xi)
  del(2,121)=0.25*(1-xi)
  del(2,122)=0.25*(1-xi)
  del(2,123)=0.25*(1-xi)
  del(2,124)=0.25*(1-xi)
  del(2,125)=0.25*(1-xi)
  del(2,126)=0.25*(1-xi)
  del(2,127)=0.25*(1-xi)
  del(2,128)=0.25*(1-xi)
  del(2,129)=0.25*(1-xi)
  del(2,130)=0.25*(1-xi)
  del(2,131)=0.25*(1-xi)
  del(2,132)=0.25*(1-xi)
  del(2,133)=0.25*(1-xi)
  del(2,134)=0.25*(1-xi)
  del(2,135)=0.25*(1-xi)
  del(2,136)=0.25*(1-xi)
  del(2,137)=0.25*(1-xi)
  del(2,138)=0.25*(1-xi)
  del(2,139)=0.25*(1-xi)
  del(2,140)=0.25*(1-xi)
  del(2,141)=0.25*(1-xi)
  del(2,142)=0.25*(1-xi)
  del(2,143)=0.25*(1-xi)
  del(2,144)=0.25*(1-xi)
  del(2,145)=0.25*(1-xi)
  del(2,146)=0.25*(1-xi)
  del(2,147)=0.25*(1-xi)
  del(2,148)=0.25*(1-xi)
  del(2,149)=0.25*(1-xi)
  del(2,150)=0.25*(1-xi)
  del(2,151)=0.25*(1-xi)
  del(2,152)=0.25*(1-xi)
  del(2,153)=0.25*(1-xi)
  del(2,154)=0.25*(1-xi)
  del(2,155)=0.25*(1-xi)
  del(2,156)=0.25*(1-xi)
  del(2,157)=0.25*(1-xi)
  del(2,158)=0.25*(1-xi)
  del(2,159)=0.25*(1-xi)
  del(2,160)=0.25*(1-xi)
  del(2,161)=0.25*(1-xi)
  del(2,162)=0.25*(1-xi)
  del(2,163)=0.25*(1-xi)
  del(2,164)=0.25*(1-xi)
  del(2,165)=0.25*(1-xi)
  del(2,166)=0.25*(1-xi)
  del(2,167)=0.25*(1-xi)
  del(2,168)=0.25*(1-xi)
  del(2,169)=0.25*(1-xi)
  del(2,170)=0.25*(1-xi)
  del(2,171)=0.25*(1-xi)
  del(2,172)=0.25*(1-xi)
  del(2,173)=0.25*(1-xi)
  del(2,174)=0.25*(1-xi)
  del(2,175)=0.25*(1-xi)
  del(2,176)=0.25*(1-xi)
  del(2,177)=0.25*(1-xi)
  del(2,178)=0.25*(1-xi)
  del(2,179)=0.25*(1-xi)
  del(2,180)=0.25*(1-xi)
  del(2,181)=0.25*(1-xi)
  del(2,182)=0.25*(1-xi)
  del(2,183)=0.25*(1-xi)
  del(2,184)=0.25*(1-xi)
  del(2,185)=0.25*(1-xi)
  del(2,186)=0.25*(1-xi)
  del(2,187)=0.25*(1-xi)
  del(2,188)=0.25*(1-xi)
  del(2,189)=0.25*(1-xi)
  del(2,190)=0.25*(1-xi)
  del(2,191)=0.25*(1-xi)
  del(2,192)=0.25*(1-xi)
  del(2,193)=0.25*(1-xi)
  del(2,194)=0.25*(1-xi)
  del(2,195)=0.25*(1-xi)
  del(2,196)=0.25*(1-xi)
  del(2,197)=0.25*(1-xi)
  del(2,198)=0.25*(1-xi)
  del(2,199)=0.25*(1-xi)
  del(2,200)=0.25*(1-xi)
  del(2,201)=0.25
```

```

del(1,9)=-2 *x1*(1-eta**2)

C.....
del(2,1)=0.25*(x1**2-x1)*(eta**2-eta)
del(2,2)=0.5*(1-x1**2)*(2*eta-1)
del(2,3)=0.25*(x1**2+xi)*(2*eta-1)
del(2,4)=-eta*(x1**2+xi)
del(2,5)=0.25*(x1**2+xi)*(2*eta+1)
del(2,6)=0.5*(1-x1**2)*(2*eta+1)
del(2,7)=0.25*(x1**2-x1)*(2*eta+1)
del(2,8)=-eta*(x1**2-x1)
del(2,9)=-2 *eta*(1-x1**2)

C.....
p(1)=0.25*(x1**2-x1)*(eta**2-eta)
p(2)=0.5*(1-x1**2)*(eta**2-eta)
p(3)=0.25*(x1**2+xi)*(eta**2-eta)
p(4)=0.5*(x1**2+xi)*(1-eta**2)
p(5)=0.25*(x1**2+xi)*(eta**2+eta)
p(6)=0.5*(1-x1**2)*(eta**2+eta)
p(7)=0.25*(x1**2-x1)*(eta**2+eta)
p(8)=0.5*(x1**2-x1)*(1-eta**2)
p(9)=(1-x1**2)*(1-eta**2)

endf
return
end
=====
C
C
subroutine deriv
1   iel ,ig ,jg ,p ,del ,b ,ncn ,da ,cg ,node ,
2   cord ,maxel,maxnp,maxst)
C
C   implicit double precision(a-h,o-z)
C   dimension p(9),b(2,9),del(2,9),cg(3),cj(2,2),cjl(2,2)
C   dimension node(maxel,27),cord(maxnp,2)
C
do 6010 j=1,2
do 6010 l=1,2
gash=0.0
do 6020 k=1,ncn
a=1abs(node(iel,k))
gash=gash + del(j,k)*cord(a,1)
cj(j,1)=gash
delj=cj(1,1)*cj(2,2) - cj(1,2)*cj(2,1)
if (delj.le.0.0) then
write(60,3010) iel,delj
stop
format(1x , ' Error: Zero or Negative Jacobian. ', i6,g20.5)
endif
C
C   cjl(1,1) = cj(2,2) / delj
C   cjl(1,2) = -cj(1,2) / delj
C   cjl(2,1) = -cj(2,1) / delj
C   cjl(2,2) = cj(1,1) / delj
C
do 6030 j=1,2
do 6030 l=1,ncn
b(j,1)=0.0
do 6030 k=1,2
b(j,1) = b(j,1) + cjl(j,k) * del(k,1)
da= delj*cg(ig)*cg(jg)
return
end
=====
C
C
subroutine front
1   (aa ,rr ,iel ,nop ,maxel,maxst,ldest,kdest,nk ,maxfr,
2   ,lhed ,khed ,kpiv ,lpiv ,jmod ,qg ,pokol,vel ,rl ,
3   ,ncod ,bc ,nopp ,mdf ,ndn ,maxdf,nel ,maxte,ntov ,lcol ,
4   ,nell ,ntrra ,press )
C
C   Frontal elimination routine using diagonal pivoting
C
C   implicit double precision(a-h,o-z)
C   dimension aa (maxst,maxst),rr (maxst)
C   dimension ap (maxel,maxst)
C   dimension ldest(maxst)
C   dimension eq (maxfr,maxfr),nk (maxst)
C   dimension kdprv (maxfr),lpiv (maxfr)

```

```

c      dimension jmc (maxfr)          ,pvkol (maxfr)
c      dimension vel (maxte)           ,r1 (maxdf)
c      dimension bc (maxdf)            ,ncod (maxdf)
c      dimension ndn (maxdf)           ,ndf (maxdf)
c      nlp and ncl are the file specifiers for units 60 and 14 respectively
c      =====
c      nlp=60
c      ncl=14
c
c      Prefront
c      =====
c      nmax=maxfr
c      ncrl=20
c      nlarg=maxfr-10
c      if (iel.eq.1) nel= 0
c      if (iel.eq.1) ntra = 1
c      if (ntra.eq.0) goto 6040
c      nmax = maxfr
c      ntra = 0
c      ncrl = 20
c      ifron = 0
c      nlarg = nmax-10
c
c      Find last appearance of each node
c      =====
c      nlast = 0
c      do 6010 i = 1,ntov
c      do 6020 n = 1,nel
c      jdn = ndn(n)
c      do 6030 j = 1,jdn
c      if(nop(n,j).ne.i)go to 6030
c      nlasti = n
c      nlast = n
c      jl = 1
c      continue
c      if(nlast.eq.0) go to 6010
c      nop(nlast,11) = -nop(nlast,11)
c      nlast = 0
c      continue
c      matrix = jdn
c
c      Assembly
c      =====
c      continue
c      if(iel.gt.1) go to 6060
c      lcol = 0
c      do 6050 i = 1,nmax
c      do 6050 j = 1,nmax
c      eq(j,i) = 0.
c      continue
c      nel1 = nel+1
c      n = nel1
c      jdn = ndn(nel1)
c      kc = 0
c      do 6070 j = 1,jdn
c      mn = nop(n,j)
c      m = labs(mn)
c      k = nop(m)
c      idt = mdt(m)
c      r1(m) = ir(j)+r1(m)
c      do 6070 i = 1,idt
c      kc = kc+1
c      ii = k+1-i
c      if(mn.lt.0)ii = -ii
c      nk(kc) = ii
c      continue
c
c      6070
c
c      Set up heading vectors
c      =====
c      do 6080 ik = 1,kc
c      node = nk(ik)
c      if(lcol.eq.0)goto 6100
c      do 6090 l = 1,lcol
c      ll = j
c      if(labs(node).eq.labs(lhead(l)))go to 6110
c      continue
c      lcol = lcol+1
c      ldest(ik) = lcol

```

```

6100      lhed(lcol) = node
        go to 6080
6110      ldest(1k) = 11
        lhed(11) = node
        continue
6080      if(lcol.le.nmax) go to 6130
        nerror = 2
        write(nlp,3010) nerror
        stop
6130      continue
        do 6140 i = 1,kc
            11 = ldest(11)
            do 6140 k = 1,kc
                Kk = ldest(k)
                eq(Kk,11) = eq(Kk,11)+aa(K,i,1)
            continue
        if(lcol.le.ncrit.and.nel1.lt.nel) return
C
C      Find out which matrix elements are fully assembled
C
6150      1c = 0
        1r = 0
        do 6160 i = 1,1col
            kt = lhed(1)
            if(kt.ge.0) go to 6160
            1c = 1c+1
            1piv(1c) = 1
            kro = labs(kt)
            if(ncod(kro).ne.1) go to 6160
            1r = 1r+1
            jmod(1r) = 1
            ncod(kro) = 2
            11(kro) = bc(kro)
            continue
6160      C
C      Modify equations with applied boundary conditions
C
        if(1r.eq.0) go to 6190
        do 6170 1tr = 1,1r
            k = jmod(1tr)
            kh = labs(lhed(k))
            do 6180 i = 1,1col
                eq(k,i) = 0.
                1h = labs(lhed(1))
                if(1h.eq.kh)eq(k,i) = 1.
            continue
        continue
6180      if(1c.gt.0) go to 6200
        ncrit = ncrit+10
        write(nlp,3020)ncrit
        if(ncrit.le.nlcrty) return
        nerror = 3
        write(nlp,3030)nerror
        stop
6200      continue
C
C      Search for absolute pivot
C
        =====
        pivot = 0.
        do 6210 i = 1,1c
            1pivc = 1piv(1)
            kpivr = 1piv
            piva = eq(kpivr,1pivc)
            if(abs(piva).lt.abs(pivoc)) go to 6220
            pivot = piva
            1pivco = 1pivc
            kpivro = kpivr
            continue
6220      continue
        if(pivot.eq.0.) return
C
C      Normalise pivotal row
C
        =====
        lco = labs(lhed(1pivco))
        kro = lco
        if(nit.eq.0.or.npra.eq.0) go to 6230
        continue
6230      C
        if(abs(pivot).lt.0.id-28) write(nlp,3050)
        do 6240 i = 1,1col

```

```

6240      qq(1) = eq(kpivro,1)/pivoc
        continue
        rhs = r1(kro)/pivoc
        r1(kro) = rhs
        pivcol(kpivro) = pivoc
        =====
        c      Eliminate then delete pivotal row and column
        c      if(kpivro.eq.1)go to 6300
        c      kpivc = kpivro-1
        c      do 6250 k = 1,kpivc
        c      kwr = labs(lhed(k))
        c      fac = eq(k,lhed(k))
        c      pivcol(k) = fac
        c      if(lpivco.eq.1.or.fac.eq.0.)go to 6270
        c      lpivc = lpivco-1
        c      do 6260 l = 1,lpivc
        c      eq(k,l) = eq(k,l)-fac*qq(1)
        c      continue
        c      if(lpivco.eq.1)go to 6290
        c      lpivc = lpivco+1
        c      do 6280 l = 1,pivco,1col
        c      eq(k,l-1) = eq(k,l)-fac*qq(1)
        c      continue
        c      r1(krw) = r1(krw)-fac*rhs
        c      continue
        c      if(kpivro.eq.1col)go to 6360
        c      kpivc = kpivro+1
        c      do 6310 k = kpivc,1col
        c      kwr = k-pivro,1col
        c      fac = eq(k,lhed(k))
        c      pivcol(k) = fac
        c      if(lpivco.eq.1)go to 6330
        c      lpivc = lpivco-1
        c      do 6320 l = 1,lpivc
        c      eq(k,l-1) = eq(k,l)-fac*qq(1)
        c      continue
        c      if(lpivco.eq.1col)go to 6350
        c      lpivc = lpivco+1
        c      do 6340 l = 1,pivco,1col
        c      eq(k,l-1) = eq(k,l)-fac*qq(1)
        c      continue
        c      r1(krw) = r1(krw)-fac*rhs
        c      continue
        c      Write pivotal equation on disc
        c      =====
        c      write(nd1) kro,1col,lpivco,(lhed(1),qq(1),1 = 1,1col)
        c      do 6370 l = 1,1col
        c      eq(1,1col) = 0.
        c      eq(lcol,1) = 0.
        c      continue
        c      6370      continue
        c      Rearrange heading vectors
        c      =====
        c      1col = 1col-1
        c      if(lpivco.eq.1col+1)go to 6390
        c      do 6380 l = 1,pivco,1col
        c      lhed(l) = lhed(l+1)
        c      continue
        c      6380      continue
        c      6390      continue
        c      Determine whether to assemble, eliminate, or backsubstitute
        c      =====
        c      if(1col.gt.ncrit)go to 6150
        c      if(ne1.lt.ne1) return
        c      if(1col.gt.1)go to 6150
        c      lco = labs(lhed(1))
        c      kpivro = 1
        c      pivoc = eq(1,1)
        c      kro = lco
        c      lpivco = 1
        c      qq(1) = 1.
        c      if(nlt.eq.0.or.npra.eq.0)go to 6400
        c      write(nlp,3040)lco,kro,pivoc
        c      if(labs(pivoc).lt.1d-28)go to 6410
        c6400      continue

```

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```

        r1(kro) = r1(kro)/pivoc
        write(nd1) kro,1col,lpivco,lhed(1),qq(1)
        c      start back-substitution
        c      =====
        c      call backsub
        c      1 (ntov,ncod,bc,r1,vel,press,maxfr,qq,lhed,nd1)
        c      main exit with solution
        c      =====
        c      6410      continue
        c      3010      format('/',nerror=',i5//
        c      1, ' the difference nmax-ncrit is not sufficiently large'
        c      1, ' to permit the assembly of the next element---'
        c      1, ' either increase nmax or lower ncrit'
        c      1//
        c      3020      format(' frontwidth value=',i4)
        c      3030      format('/',nerror=',i5//
        c      1, ' There are no more rows fully summed,this may be due to---'
        c      1, ' (1)incorrect coding of nop or nk arrays'
        c      1, ' (2)incorrect value of ncrit. increase ncrit to permit'
        c      1, ' whole front to be assembled'
        c      1//
        c      c3040      format(13h pivotal row=,i4,16h pivotal column=,i4,7h pivot=,e20,10
        c      1)
        c      3050      format(' warning-matrix singular or ill conditioned')
        c      return
        c      end
        c      =====
        c      1 (ntoc1,ifix,vfix,rhs,soln,soln1,mfrnt,twork,iwork,ldv2)
        c      implicit double precision(a-h,o-z)
        c      dimension ifix (ntoc1),vfix (ntoc1),rhs (ntoc1),soln (ntoc1)
        c      dimension twork(mfrnt),iwork(mfrnt),soln1(ntoc1/3)
        c      c
        c      do 6010 ipos=1,ntoc1
        c      soln(ipos) = 0.0
        c      if(fix(ipos).ne.0) continue
        c      6010      do 6020 kpos=1,ntoc1
        c      backspace idv2
        c      read(idv2) ipos,ifrn1,jfrnt,(iwork(k),twork(k),k=1,ifrn1)
        c      backspace idv2
        c      c
        c      if(fix(ipos).ne.0) go to 6020
        c      wv = 0.0
        c      twork(jfrnt) = 0.0
        c      c
        c      do 6030 k=1,ifrn1
        c      jpos=labs(iwork(k))
        c      wv = wv - twork(k)*soln(jpos)
        c      continue
        c      6030      soln(ipos)=rhs(ipos)+wv
        c      c
        c      6020      continue
        c      do 6040 ipos = ((2*ntoc1)/3)+1, ntoc1
        c      j = ipos - ((2*ntoc1)/3)
        c      soln1(j) = soln(ipos)
        c      continue
        c      6040      continue
        c      return
        c      end
        c      =====
        c      subroutine flow(ilt,node,cord,pmat,nopp,mfr,ndn,ncod,bc,vel

```

14

```

4,press, i1, temp, i0est, k0est, n1, eq, i1ed, k1ed, k1iv, i1iv,
2,mod, qq, pvkol, iter, nel, ncn, ngaus, p, del, b, ntrix, maxel,
3,maxnp, maxst, maxfr, maxdt, ndim, aa, xg, da, nrov, num, icord,
4ir, iel, deltat, alpha, idv4, sinv, nmp, step, permx, permy, guessp,
5comfactor, percomp, permstep1, permstep2)

```

```

c implicit double precision(a-h,o-z)

```

```

c dimension node (maxst,maxst),pmat (maxel,
dimension ncod (maxdt,maxdt),bc (maxdt,
dimension vel (nmp,ndim),r1 (maxdt,
dimension aa (maxst,maxst),rt (maxst,
dimension xg (maxst,maxst),cg (maxst,
dimension x (maxst,maxst),v (maxst,maxst,
dimension b1cn (maxst,maxst),del (maxst,
dimension p (maxst,maxst),nopp (maxst,
dimension idsc (maxst,maxst),k1ed (maxst,
dimension i1ed (maxst,maxst),k1iv (maxst,
dimension i1iv (maxst,maxst),ndf (maxst,
dimension pvkol (maxst,maxst),pp (maxst,
dimension ak (maxst,maxst),akf (maxst,
dimension nq (maxst,maxst),np (maxst,
dimension c (maxst,maxst),temp (maxst,
dimension press (maxnp,maxnp),SHAPEID(3,
dimension qsf (maxnp,maxst)

```

```

rvisc = pmat(iel,1)
rpef = pmat(iel,2)
power = pmat(iel,3)
rtcm = pmat(iel,4)
tbco = pmat(iel,5)
taco = pmat(iel,6)
roden = pmat(iel,8)
gamad = pmat(iel,9)

```

```

velsound = 1150.0

```

```

call perm

```

```

1(step, permx, permy, guessp, comfactor, percomp, permstep1, permstep2)

```

```

c if(i1c == 1) then
c permstep1 = permx
c permstep2 = permstep1

```

```

c else if (i1c.gt.1) then
c permstep2 = permx

```

```

c end if

```

```

c percomp = (permstep1-permstep2)*100/permstep1

```

```

c if(iel == 1) then
c print *, "permstep1 = ", permstep1
c print *, "permstep2 = ", permstep2
c print *, "percomp = ", percomp
c end if

```

```

c do 6010 idf= 1,ntrix
c rr (idf) = 0.0
c akf(idf) = 0.0
c (idf) = 0.0
c do 6010 jdf= 1,ntrix
c aa (idf,jdf)=0.0
c dmass(idf,jdf)=0.0
c ak (idf,jdf)=0.0
c continue

```

```

c 6010 call gaussp(ngaus, xg, cg)

```

```

c 1g=0
c do 6020 ig=1,ngaus

```

```

c g = xg(ig)
c h = xg(jg)

```

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1g = 1g + 1

```

c if(iter.eq.1) then

```

```

c call shape (g,h,p,del,ncn)
c call deriv (iel,ig,jg,p,del,b,ncn,da,cg,node,cor,
maxel,maxnp,maxst)

```

```

c iig=ig
c jjg=jg

```

```

c else
c write(15) iel,ig,jg,p,del,b,da
c if(.not. EOF(15))read(15) iel,iig,jig,p,del,b,da

```

```

c endif

```

```

c calculation of viscosity based on the constitutive equation.

```

```

c sprss = 0.0
c stemp = 0.0

```

```

c 5333 do 5333 ip=1,ncn
c jp = iabs(node(iel,ip))
c continue
c epsil = 1.d-10
c gamad = sinv(iel,ig)
c if(srate.lt.epsil) srate = epsil

```

```

c call visca
c 1(rvisc,power,visc,stemp,rtcm,tbco,sprss,rpef,taco,gamad)

```

```

c preparation of the convective acceleration terms/balancing
c dissipation is used

```

```

c do 6050 idff= 1,2
c x(idff) = 0.0
c v(idff) = 0.0
c hh(idff) = 0.0

```

```

c 6050 do 6060 icn = 1,ncn
c jcn = iabs(node(iel,icn))
c do 6060 idff= 1
c x(idff) = x(idff) + p(icn)*cord(jcn,idff)
c v(idff) = v(idff) + p(icn)*vel(jcn,idff)
c continue

```

```

c if(icord.eq.1) then

```

```

c modify da for axisymmetric computations.

```

```

c da = da * x(1)
c endif

```

```

c column index

```

```

c do 6070 i=1,ncn
c j11= i
c j12= i + ncn
c j13= i + 2*ncn

```

```

c do 6070 j=1,ncn
c j21= j
c j22= j + ncn
c j23= j + 2*ncn

```

```

c ----- DISCRETISED FORM OF DARCY EQUATION
c ----- Stiffness Matrix of Left Hand Side
c -----

```

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```

C For Transient state (Cartesian co-ordinate system)
C =====
1 aa(j11,j21)=aa(j11,j21) + p(i)*p(j)*da
2 + (alpha*deltac*visc*p(i)*p(j)*da)
  / (roden*permx)
aa(j11,j22)=aa(j11,j22) + 0.0
aa(j11,j23)=aa(j11,j23) - alpha*deltac*b(1,i)*p(j)*da
aa(j12,j21)=aa(j12,j21) + 0.0
5 aa(j12,j22)=aa(j12,j22) + p(i)*p(j)*da
6 + (alpha*deltac*visc*p(i)*p(j)*da)
  / (roden*permy)
aa(j12,j23)=aa(j12,j23) - alpha*deltac*b(2,i)*p(j)*da
1 aa(j13,j21)=aa(j13,j21) + alpha*deltac*velsound*velsound*
  p(i)*b(1,j)*da
1 aa(j13,j22)=aa(j13,j22) + alpha*deltac*velsound*velsound*
  p(i)*b(2,j)*da
aa(j13,j23)=aa(j13,j23) + p(i)*p(j)*da

-----
C DISCRETISED FORM OF DARCY EQUATION
C Stiffness Matrix of Right Hand Side
C =====
C For Transient state (Cartesian co-ordinate system)
C =====
1 ak(j11,j21)=ak(j11,j21) + p(i)*p(j)*da
2 - ((1.0-alpha)*deltac*visc*p(i)*p(j)*da)
  / (roden*permx)
ak(j11,j22)=ak(j11,j22) + 0.0
ak(j11,j23)=ak(j11,j23) + (1.0-alpha)*deltac*b(1,i)*p(j)*da
ak(j12,j21)=ak(j12,j21) - 0.0
1 ak(j12,j22)=ak(j12,j22) + p(i)*p(j)*da
2 - ((1.0-alpha)*deltac*visc*p(i)*p(j)*da)
  / (roden*permy)
ak(j12,j23)=ak(j12,j23) + (1.0-alpha)*deltac*b(2,i)*p(j)*da
1 ak(j13,j21)=ak(j13,j21) - (1.0-alpha)*deltac*velsound*velsound*
  p(i)*b(1,j)*da
1 ak(j13,j22)=ak(j13,j22) - (1.0-alpha)*deltac*velsound*velsound*
  p(i)*b(2,j)*da
1 ak(j13,j23)=ak(j13,j23) - (1.0-alpha)*deltac*velsound*velsound*
  p(i)*b(2,j)*da

```

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```

ak(j13,j23)=ak(j13,j23) + p(i)*p(j)*da

6070 continue
6020 continue

C For Transient State (Cartesian Co-ordinate System)
C =====
C Term one on RHS is evaluated
C =====
do 6080 i=1,ncn
  j11= i
  j12= i + ncn
  j13= i + 2*ncn
do 6080 j=1,ncn
  j21= j
  j22= j + ncn
  j23= j + 2*ncn
  nm=abs(node(iel,j))
  1 akf(j11)=akf(j11) + ak(j11,j21)*vel(nm,1) +
  2 ak(j11,j23)*press(nm)
  1 akf(j12)=akf(j12) + ak(j12,j21)*vel(nm,1) +
  2 ak(j12,j23)*press(nm)
  1 akf(j13)=akf(j13) + ak(j13,j21)*vel(nm,1) +
  2 ak(j13,j23)*vel(nm,2) +
  ak(j13,j23)*press(nm)

6080 continue

C Evaluation of Elemental Load Vector
C =====
do 6085 i=1,ncn
  j11= i
  j12= i + ncn
  j13= i + 2*ncn
C For Transient State (Cartesian Co-ordinate System)
  rr(j11)=akf(j11)+C(j11)
  rr(j12)=akf(j12)+C(j12)
  rr(j13)=akf(j13)+C(j13)
6085 continue
  maxte=maxdf
  call front
  1(aa,'rr',iel,node,maxel,maxst,ldest,kdest,nk,maxfr
  2,eg,'lhed,khed,kpiv,jmod,qd,pvkol,vel,ri
  3,ncod,nc,nopp,mid,ndn,maxdf,nel,maxte,ntov,lcol
  4,nell,ntra,press)

C
C return
C end
C =====
C subroutine getnod (nmp ,cord ,idv1 ,idv2 ,maxnp,ndim,icord)
C
C implicit double precision(a-h,o-z)
C arguments
C =====

```

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```

C      return
C      format(2i5,g20.8)
C      format(' ',//,'/', ' ',20('*'), ' nodal constraint ',20('*'),//
3010    ' ', '(8x,'1d','7x','def',10x,' value',10x)//
3020    format(5x,i5,5x,i5,f17.4)
C
C      end
C
C      =====
C      subroutine putpcv
C      1 (mp ,nbc ,lbc ,jbc ,vbc ,ncod ,bc ,maxbc,maxdf, maxel,
C        2 node)
C
C      implicit double precision(a-h,o-z)
C
C      arguments
C      =====
C      ncod array for constraint switch defined for every d.o.f.
C      bc array for storing contraint value
C      maxbc see below
C      maxdf see below
C
C      dimension ibc (maxbc), jbc (maxbc), vbc (maxbc)
C      dimension ncod (maxdf), bc (maxdf), node (maxel,27)
C
C      do 6010 ind = 1, nbcc
C      if(jbc(ind)>3) goto 6010
C      ind
C      bc (jnd) = vbc(ind)+jbc(ind)-1)*mp
C      ncod (jnd) = 1
C      continue
C
6010    continue
C
C      specifying the stress free condition on node number 84
C      iel=16
C      imp=24
C      kc=iabs(node(iel,imp))
C
C      return
C      end
C
C      =====
C      subroutine clean
C      1 (ncn ,nel ,ndf ,node ,r1 ,maxel,maxst,maxdf,
C        2 bc ,ncod ,icho )
C
C      implicit double precision(a-h,o-z)
C
C      arguments
C      =====
C      all arguments are defined elsewhere.
C
C      dimension r1 (maxdf), node(maxel,maxst)
C      dimension bc (maxdf), ncod(maxdf)
C
C      function
C      =====
C      cleans the used arrays and makes them ready for solution
C
C      do 6010 i = 1,maxdf
C      r1(i) = 0.0
C      bc(i) = 0.0
C      ncod(i) = 0
C      continue
C      ntrix = ndf*ncn
C      do 6020 iel = 1,nel
C      do 6020 imp = 1,ntrix
C      node(iel,imp) = iabs(node(iel,imp))
C      continue
C      if(icho.ne.1)then
C      do 6030 iel = 1,nel
C      write(11,3010) iel, node(iel,j),j=1,ncn)
C      format(10i5)
C      continue
C      endif
C
C      return
C      end
C
C      =====

```

```

1 subroutine secpm
2   (nmp,nel,nen,node,nmf,maxel,maxst,ndn,ntrix,
3    maxdf,ntov,nmf,nopp)
4   implicit double precision(a-h,o-z)
5   arguments
6   =====
7   all arguments are defined elsewhere.
8   dimension node (maxel,maxst), ndn (maxdf)
9   dimension nmf (maxdf), nopp (maxdf)
10  function
11  =====
12  Sets the location data for nodal degrees of freedom
13
14  do 6010 iel = 1,nel
15    ndn(iel) = ntrix
16    do 6010 ien = 1,nen
17      ken = node(iel,ien)
18      jcn = ien + (ndf-2)*nen
19      lcn = ken + (ndf-2)*nmp
20      acn = ien + (ndf-1)*nen
21      bcn = ken + (ndf-1)*nmp
22
23    node(iel,jcn) = lcn
24    node(iel,acn) = bcn
25
26  6010 continue
27  do 6020 idf = 1,ntov
28    mdf(idf) = 1
29    nopp(idf) = idf
30  6020 continue
31
32  return
33 end
34
35 =====
36 subroutine getmat (nel,nmat,pmat,idv1,idv2,maxel,rtem,rpref)
37
38 implicit double precision(a-h,o-z)
39
40 arguments
41 =====
42 nmat number of materials
43 pmat array for material constants for each element
44 idv1 input device id.
45 idv2 output device id.
46 maxel see below
47
48 dimension pmat (maxel, 9)
49
50 write(idv2,3010)
51
52 do 6010 imat = 1,nmat
53   if (.not. eof(51)) read(idv1,1010) rvisc, power, tref, tbco, taco,
54   1 print*, "material properties read" dispcc, pref, roden, gamad
55   ifrom = 1
56   ito = nel
57
58   if(rtem.eq.0.) rtem = 0.001
59   if(rpref.eq.0.) rpref = 0.001
60
61   do 6020 iel = ifrom, ito
62     pmat(iel,1) = rvisc
63     pmat(iel,2) = pref
64     pmat(iel,3) = power
65     pmat(iel,4) = tref
66     pmat(iel,5) = tbco
67     pmat(iel,6) = taco
68     pmat(iel,7) = dispcc
69     pmat(iel,8) = roden
70     pmat(iel,9) = gamad
71     rtem = tref
72     rpref = pref
73
74   roden = density
75   rvisc = mu nought, consistency coefficient
76   pref = reference pressure

```

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```

1 power law index
2 tref reference temperature
3 tbco coefficient b in the power law model
4 taco coefficient a in the power law model
5 dispcc dispersion coefficient
6 gamad shear rate
7
8 6020 continue
9
10 write(idv2,3020) imat,ifrom,ito,rvisc,power
11 write(idv2,3030)
12 write(idv2,3040) tref,tbco,pref,taco
13 write(idv2,3050)
14 write(idv2,3060) dispcc,roden,gamad
15
16 6010 continue
17
18 return
19
20 1010 format(9d10.5)
21
22 3010 format('','','',35(' '), material properties '35(' '),
23 ' ',2x,'id.',5x,'eid.(from-to)',3x,'consistency co-efficient',
24 1,5x,'power law index',/)
25 3020 format(' ',13,112,14,5x,g15.5,g15.5)
26 3030 format(/x,' reference temperature coefficient b
27 1 reference pressure coefficient a '/')
28 3040 format(f16.3,f22.4,6x,g10.3,9x,g10.3)
29 3050 format(/x,
30 1'Dispersion Coefficient Density Shear rate'/)
31 3060 format(g13.3,15x,g7.1,6x,g16.5)
32
33 end
34
35 =====
36 subroutine conrol
37 1 vel, iter, ntov, nmp, maxmp, maxdf, errorv, errorp, vet,
38 2 pet, press)
39
40 implicit double precision(a-h,o-z)
41
42 dimension vel (maxdf), press(maxmp)
43 dimension vet (maxdf), pet (maxmp)
44
45 errorv = 0.0
46 torv = 0.0
47 errorp = 0.0
48 torp = 0.0
49
50 calculate difference between velocities in consecutive iterations
51 =====
52 do 6010 icheck = 1,ntov
53   if(iter.eq.1) vet(icheck) = 0.0
54   1 (vel(icheck)-vet(icheck)) * (vel(icheck)-vet(icheck))
55   torv = torv + vel(icheck)*vel(icheck)
56
57   vet(icheck) = vet(icheck)
58
59   continue
60   errorv = errorv/torv
61
62 calculate difference between pressures in consecutive iterations
63 =====
64 do 6030 icheck = 1,nmp
65   if(iter.eq.1) press(icheck) = 0.0
66   1 errorp = errorp +
67   (press(icheck)-pet(icheck)) * (press(icheck)-pet
68   2 (icheck))
69   torp = torp + press(icheck)*press(icheck)
70
71   pet(icheck) = press(icheck)
72
73   continue
74   errorp = errorp/torp

```

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```

C      return
C      end
C      =====
C      subroutine output
C      1      (imp , vel , press , maxdf , maxnp , icord , pmat , maxel , actpress )
C      implicit double precision(a-h,o-z)
C      arguments are already defined
C      =====
C      dimension vel (maxdf ) , press (maxnp )
C      dimension pmat (maxel , 9) , actpress (maxnp )
C      write(60,3010)
C      if(icord.eq.0) write(60,3020)
C      if(icord.eq.1) write(60,3030)
C      roden=pmat(1,8)
C      do 6010 imp = 1, nnp
C      actpress(imp)=roden*press(imp)
C      write(60,3040) imp , vel(imp) , vel(jnp) , actpress(imp)
C      6010 continue
C      call minimax
C      1      cmx , pmax , vel , press , maxnp , nnp , nc , np
C      2      nm , ncm , nvxm , nvym , nvxl , nvyl , pmin , cmin ,
C      3      vxmax , vxmin , vymax , vymin , ndim , maxdf , actpress )
C      write(60,3045)
C      write(60,3050) nvxm , vel (nvxm) , nvxl , vel (nvxl)
C      write(60,3055)
C      write(60,3060) nvym , vel (npy+nvym) , nvyl , vel (npy+nvyl)
C      write(60,3065)
C      write(60,3070) np , press (np) , nm , press (nm)
C      3010 format(' nodal velocities and pressures '/')
C      3020 format(' id. ux uy uz press')
C      3030 format(' id. ux uz press')
C      3040 format(15,2e13.4,e22.8)
C      3045 format('node no. max ux node no. min ux')
C      3050 format(15,e22.8,15,e22.8)
C      3055 format('node no. max uy node no. min uy')
C      3060 format(15,e22.8,15,e22.8)
C      3065 format('node no. max p node no. min p')
C      3070 format(15,e22.8,15,e22.8)
C      return
C      end
C      =====
C      subroutine visc
C      1      (rvisc , power , visc , stemp , item , tbro , spress , rref , teco
C      2      , gamad )
C      implicit double precision(a-h,o-z)
C      visc = rvisc*(4*gamad)**((power-1.0)/2)
C      return
C      end
C      =====
C      subroutine minimax
C      1      ( cmx , pmax , vel , press , maxnp , nnp , nc , np ,

```

23

```

C      1      nm , ncm , nvxm , nvym , nvxl , nvyl , pmin , cmin ,
C      1      vxmax , vxmin , vymax , vymin , ndim , maxdf , actpress )
C      implicit real*8 (a-h,o-z)
C      dimension vel (maxdf )
C      dimension press ( maxnp )
C      dimension actpress (maxnp)
C      vxmax = vel(1)
C      vxmin = vel(1)
C      vymax = vel(npy+1)
C      vymin = vel(npy+1)
C      pmax = actpress(1)
C      pmin = actpress(1)
C      np = 1
C      nm = 1
C      nvxm = 1
C      nvym = 1
C      nvxl = 1
C      nvyl = 1
C      do 6020 i=2, nnp
C      pm = actpress (i)
C      pi = actpress (i)
C      vxmx = vel(i)
C      vxmn = vel(i)
C      vyxm = vel(npy+i)
C      vyym = vel(npy+i)
C      if ( pm.gt.pmax ) then
C      pmax=pm
C      np = i
C      endif
C      if ( pi.lt.pmin ) then
C      pmin = pi
C      nm = i
C      endif
C      if ( vxmx.gt.vxmax ) then
C      vxmax= vxmx
C      nvxm = i
C      endif
C      if ( vyxm.gt.vymax ) then
C      vymax= vyxm
C      nvym = i
C      endif
C      if ( vxmn.lt.vxmin ) then
C      vxmin= vxmn
C      nvxl = i
C      endif
C      if ( vyym.lt.vymin ) then
C      vymin= vyym
C      nvyl = i
C      endif
C      6020 continue
C      return
C      end
C      =====
C      subroutine sectiv
C      1      (nel , nnp , ncn , ngaus , node , sinv , cord , p , b ,
C      2      , del , da , vel , maxnp , maxel , maxst , ndim , icord ,
C      3      , maxdf , num)
C      implicit double precision(a-h,o-z)
C      function
C      -----
C      calculates the second invariant of rate of deformation
C      tensor at integration points.
C      dimension vel (maxdf ) , cord (maxnp , ndim)
C      dimension node (maxel , maxst) , sinv (maxel , num)
C      dimension p ( 9 ) , del ( 2 , 9)
C      dimension b ( 2 , 9)

```

24

[illegible]

```

10001         else if (velcarttridg(indata).gt. 0.0067) and.
10002             1
10003             velcarttridg(indata).le. 0.0362) then
10004                 dpguess(indata) = 75818119.5771*(velcarttridg(indata)**1.3099)
10005             else if (velcarttridg(indata).gt. 0.0362) then
10006                 dpguess(indata) = 30053002.836*velcarttridg(indata)
10007             end if
10008             guessp = dpguess(indata)
10009             !t = 1
10010             print *, "Data set = ", indata
10011             print *, "velcarttridg = ", velcarttridg(indata)
10012             c print *, "guessp = ", guessp
10013             c print *, "inner iteration = ", !t
10014
10015 9001 do 5150 iter = 1, niter
10016
10017             c TEMPORAL UPWIND SCHEME USED
10018             c =====
10019             c alpha = 0.75
10020             c delta = 0.10
10021             c -----
10022
10023             time = iter*deltat
10024             write(60,4090) iter
10025
10026             c Print *, "Iter = ", iter
10027             c =====
10028             c Calculate Nodal Velocities & Pressures
10029             c =====
10030             icho=1
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1043
```

```

do 5170 inp = 1, nmp
    actpress(inp) = press(inp)*density
5170 end do

c      if(iit=1) then
c          press_nocomp = actpress(1741)
c      end if
c      press_withcomp(ndata) = actpress(6781)
c      press_areacomp(ndata) = guessp
c      call arealoss (actpress, guessp, areafactor, peraloss, maxmp)
c      postarea = peraloss
c      print *, "postarea = ", postarea
c      errareal = 0.99*areabase(ndata)
c      errarea2 = 1.01*areabase(ndata)
c      print *, "errareal = ", errareal
c      print *, "errarea2 = ", errarea2
c      if(postarea .le. errareal) then
c          guessp = guessp*1.2
c          dpguess(ndata) = guessp
c          iit = iit + 1
c      elseif(postarea .ge. errarea2) then
c          guessp = guessp*0.8
c          dpguess(ndata) = guessp
c          iit = iit + 1
c      goto 9001
c      end if
c      =====
c      if the solutions converge and the simulated peraloss lies within the
c      range of error bounds assumed for the guessed value of loss in area
c      factor print the parameters in excel file
c      =====
c      Store the value of pressure drop with compression and no loss in area (BAR)
c      excel (2) = (press_withcomp(ndata)/99996.71053)
c      -----
c      Store the value of pressure drop with compression and with loss in area (BAR)
c      excel (3) = (guessp/99996.71053)
c      -----
c      Store the value of percentage compression
c      excel (4) = percomp
c      -----
c      Store the value of apparent loss in filtration area
c      excel (5) = peraloss
c      lossinarea = (excel (5))*100
c      print *, "pressure drop with compression and no loss in area =
c      1", excel(2)
c      print *, "pressure drop with compression and with loss in area =
c      1", excel(3)
c      print *, "% Compression = ", excel(4)
c      print *, "% Apparent loss in filtering area = ", lossinarea
c      Print the converged velocity and pressure field in output file
c      -----
c      iter=(iter/ntep)*ntep
c      if(iter.eq.1.or.iter.eq.iter) then
c          call output
c          1 (nmp,vel,press,maxdf,maxmp,icord,pmat,maxel,actpress)
c          end if
c      -----
c      Updating viscosity
c      -----

```

```

c      call sechnv
c      1 (nel ,nmp ,ncn ,ngaus,node ,sinv ,cord ,p ,b,
c      2 del ,da ,vel ,maxmp,maxel,maxst,ndim ,icord,
c      3 maxdf,num)
c      =====
c      Print the output
c      =====
c      Convergence check
c      =====
c      call control(vel ,iter ,ntov ,nmp,maxmp,maxdf,error ,error
c      1,vel ,pet ,press)
c      =====
c      End of time loop
c      =====
4090 format(///"TIME STEP no.",i5,///)
c      return
c      end
c      =====
c      subroutine perm
c      1(step,permx,permy,deltap,comfactor,percomp,pernstep1,pernstep2)
c      =====
c      implicit double precision(a-h,o-z)
c      =====
c      Function
c      -----
c      Calculates the Permeability of the Fiber Glass Media for Filter Analysis
c      -----
c      Convert experimental pressure drop in bar to pascals
c      -----
c      if (deltap .le. 1.13E+5) then
c          permx = 1.96735E-12
c          permy = 1.96735E-12
c          pernstep1 = 1.96735E-12
c          pernstep2 = permx
c      end if
c      if (deltap .gt. 1.13E+5 .and. deltap .le. 10.8E+5) then
c          permx = (1.628E+0.0000000002)*((deltap)**(-0.2397))
c          permy = (1.628E+0.0000000002)*((deltap)**(-0.2397))
c          pernstep1 = 1.96735E-12
c          pernstep2 = permx
c      end if
c      if (deltap .gt. 10.8E+5) then
c          permx = 1.0435900E-12
c          permy = 1.0435900E-12
c          pernstep1 = 1.96735E-12
c          pernstep2 = permx
c      end if
c      end if
c      -----
c      Calculate the compression factor and percentage compression
c      -----
c      comfactor = ((pernstep1-pernstep2)/pernstep1)
c      percomp = (comfactor*100)
c      return
c      end
c      =====
c      subroutine arealoss
c      1 (actpress, guessp, areafactor, peraloss, maxmp)
c      =====
c      implicit double precision(a-h,o-z)
c      dimension actpress(maxmp)
c      -----
c      Function
c      -----
c      Calculates the Loss in Area Factor and Percentage Loss in Area
c      -----

```

```

C Convert experimental pressure drop in bar to pascals
C -----
C      deltap = guessp
C      peraloss = ((deltap-actpress(67811))/deltap)
C      areafactor = 1.0-peraloss
C
C      print*, "Guess value of Pressure in pa =", deltap
C      print*, "Simulated Pressure drop in pa =", actpress(67811)
C      print*, "Percentage loss in Area =", peraloss
C      print*, "Area factor for Velocity Correction =", areafactor
C      return
C end
C =====
C SUBROUTINE GPMFEM
C
C      IMPLICIT REAL*8 (A-H,O-Z)
C      CHARACTER CH(400)*1,SF*4,CC*3,FNAME*30
C      DIMENSION NOD(9)
C
C      FUNCTION
C
C      TRANSFORMATION OF GEOSTAR FROM FILE TO MESH.FEM FILE
C
C      WRITE (*,130)
C130  FORMAT(1X,"Enter GPM file name for the Filter Mesh ")
C      READ (*,135) FNAME
C135  FORMAT(A30)
C      OPEN (UNIT=1, FILE=FNAME, FORM='FORMATTED')
C      OPEN (UNIT=2, STATUS='SCALCH', FORM='FORMATTED')
C      OPEN (UNIT=3, FILE='MESH.FEM', FORM='FORMATTED')
C      NOD=0
C      IOS=0
C      IOS=0
C      NNM=0
C      NNM=0
C      DO WHILE (IOS.EQ.0)
C      DO READ (1,100,ERR=300,END=300,IOSTAT=IOS) (CH(U),U=1,400)
C      CC=CH(1)//CH(2)
C      IF (CC.EQ.'ND') THEN
C      WRITE (2,100) (CH(K),K=4,300)
C      NNM=NNM+1
C      ENDIF
C      IF (CC.EQ.'EL') THEN
C      WRITE (2,100) (CH(K),K=4,300)
C      NEM=NEM+1
C      ENDIF
C      ENDIF
C100  FORMAT(500A)
C      ENDDO
C300  PRINT *, 'TOTAL NO. OF NODES = ', NNM
C      PRINT *, 'TOTAL NO. OF ELEMENTS = ', NEM
C      DO I=1,NNM
C      READ (2,*) N,X,Y
C      X1 = X*1e-3
C      Y1 = Y*1e-3
C      WRITE (3,110) N,X1,Y1
C110  FORMAT(15,2G20.8)
C      ENDDO
C
C      PRINT *, 'File MESH.FEM is created '
C      RETURN
C      END
C
C SUBROUTINE CARTRIDGE (ntd,density,fr,velcartridge,farea,vliisc,
C1  areabase,xab,yab,xjkl,yjkl,xifga,yifga,
C2  xidkdjd,yidkdjd,xadb,yadb)
C
C      IMPLICIT REAL*8 (A-H,O-Z)
C      DIMENSION fr(20),velcartridge(20),pd(20),vliisc(20),
C1  areabase(20)
C
C      FUNCTION
C
C -----
C
C READS THE FILTERING AREA, FLOW RATE, VISCOSITIES, FLOW RATES & BC CO-ORDINATES FOR FILTER
C MESH
C -----
C      Opening of file to be cartridge filter element
C      =====
C      print*, 'Enter the Reference ID of the FILTER ELEMENT'
C      read(*,100) carid
C      open(unit=511, file=carid, access='sequential', form='formatted',
C1  status='unknown', iostat=ios)
C      Read the total number of sets of data
C      -----
C      read(511,2001) ntd
C
C      Read the total filtering area and density of the fluid
C      -----
C      read(511,2005) farea, density
C
C      Read the Flow Rate in (lit/min), Pressure Drop in (bar) and viscosity in (Pa.s)
C      -----
C      do i=1,ntd
C      jj=i
C      read(511,2002) fr(jj),areabase(jj),vliisc(jj)
C      end do
C
C      Calculate velocity (m/s) corresponding to experimental flow rate
C      -----
C      do i=1,ntd
C      jj=i
C      velcartridge(jj) = fr(jj)*0.001/(farea*60)
C      end do
C
C      Read the co-ordinates in (mm) to be used for the calculation of boundary conditions
C      -----
C      read(511,2003) xab,yab
C      read(511,2003) xjkl,yjkl
C      read(511,2003) xifga,yifga
C      read(511,2003) xidkdjd,yidkdjd
C      read(511,2003) xadb,yadb
C
C      xab = xab*1e-3
C      yab = yab*1e-3
C      xjkl = xjkl*1e-3
C      yjkl = yjkl*1e-3
C      xifga = xifga*1e-3
C      yifga = yifga*1e-3
C      xidkdjd = xidkdjd*1e-3
C      yidkdjd = yidkdjd*1e-3
C      xadb = xadb*1e-3
C      yadb = yadb*1e-3
C
C      print*, xab,yab
C      print*, xjkl,yjkl
C      print*, xifga,yifga
C      print*, xidkdjd,yidkdjd
C      print*, xadb,yadb
C
C      Read the Geometrical Parameters of the Filter Element
C      -----
C      read(511,2004) emp ! Number of Pleats
C      print*, emp
C
C      read(511,2004) hp ! Height of Filter Element (mm)
C      print*, hp
C
C      read(511,2004) el ! Length of Pleat (mm)
C      print*, el
C
C      read(511,2004) di ! Diameter of the Core (mm)
C      print*, di
C
C      Writing all the cartridge description in file 61 used for excel
C      -----
C      write (61,4020) farea,emp,hp,el,di,density
C
C100  format(80a)

```

```

2001 format(i5)
2002 format(10x,d10.5,10x,d10.5,10x,d10.5)
2003 format(15x,f22.12,f22.12)
2004 format(10x,f10.5)
2005 format(10x,d10.5,10x,d10.5)

4020 format(' ',20x,'-----CARTRIDGE FILTER DESCRIPTION DATA',/
1',20x,'-----',/
325x,'Filtering area of cartridge      ','',f10.4,/
225x,'Number of pleats                 ','',f10.4,/
325x,'Height of the filter element     ','',f10.4,/
425x,'Length of the pleat              ','',f10.4,/
525x,'Diameter of the cartridge        ','',f10.4,/
725x,'Hydraulic fluid density          ','',f10.4,/
7///)

write (61,4030)

4030 format(/'      Flow Rate(lit/min)      Viscosity
1      (Pa.s)      Pressure com(Bar)      Pressure com + area(Bar)
3      % Compression      %loss in area      '/')

RETURN
END

=====
1      subroutine pleatbc
      (frate,farea,nbc,jbc,vbc,maxbc,maxnp,ndim,cord,strep,
2      areafactor,xab,yab,xjkl,yjkl,xfgfd,yfgfd,xldkjd,yldkjd,
3      xabbd,yabbd)

      implicit real*8 (a-h,o-z)

      dimension x      (10101)
      dimension y      (10101)
      dimension vx      (10101)
      dimension vy      (10101)
      dimension jbc      (maxbc) , jbc      (maxbc) , vbc      (maxbc)
      dimension cord      (maxnp , ndim)

      parameter (pi=3.1415926535897932384D0)

-----
FUNCTION
-----
CALCULATION OF BOUNDARY CONDITIONS FOR THE POROUS FLOW SIMULATION

open (unit=70,file='velbcstep1',form='formatted',status='new')
rewind (70)

C
C
C      Conversion of volumetric flow rate in litres/minute to average velocity in metres/second
C
C      frate = (frate)/farea*60000.0)
C
C      Read the co-ordinates and store these values in arrays
C
C      =====
C      do i=1,10101
C      x(i)=cord(i,1)
C      y(i)=cord(i,2)
C      end do
C
C
C      CALCULATIONS OF THE BOUNDARY CONDITIONS STARTS
C
C      -----
C      These are the calculations for the curved part ab
C
C      =====
C      do i=1,40
C
C      slope=(y(i+1)-yab)/(x(i+1)-xab)
C      theta=atan(slope)
C      theta=-theta
C      vx(i+1)=frate*cos(theta)
C      vy(i+1)=-frate*sin(theta)
C
C      end do

```

```

C
C      These are the calculations for the straight part bc
C      =====
C      slope = (y(901)-y(862))/(x(901)-x(862))
C      slopen=(-1.0/slope)
C      theta=atan(slopen)
C      theta=-theta
C      do i=1,40
C      vx(i+861)=frate*cos(theta)
C      vy(i+861)=-frate*sin(theta)
C      end do
C
C      These are the calculations for the curved part cd
C      =====
C      do i=1,40
C
C      slope=(y(i+1701)-yjkl)/(x(i+1701)-xjkl)
C      theta=atan(slope)
C      theta=-theta
C      vx(i+1701)=frate*cos(theta)
C      vy(i+1701)=-frate*sin(theta)
C
C      end do
C
C      These are the calculations for the curved part de
C      =====
C      do i=1,40
C
C      slope=(y(i+2541)-yjkl)/(x(i+2541)-xjkl)
C      theta=atan(slope)
C      vx(i+2541)=frate*cos(theta)
C      vy(i+2541)=-frate*sin(theta)
C
C      end do
C
C      These are the calculations for the straight part ef
C      =====
C      slope=(y(3382)-y(3421))/(x(3382)-x(3421))
C      slopen=(-1.0/slope)
C
C      do i=1,40
C      vx(i+3381)=-frate*cos(theta)
C      vy(i+3381)=-frate*sin(theta)
C      end do
C
C      These are the calculations for the curved part fg
C      =====
C      do i=1,40
C
C      slope=(y(i+4221)-yfgfd)/(x(i+4221)-xfgfd)
C      theta=atan(slope)
C      vx(i+4221)=frate*cos(theta)
C      vy(i+4221)=-frate*sin(theta)
C
C      end do
C
C      These are the calculations for the curved part gf'
C      =====
C      do i=1,40
C
C      slope=(y(i+5061)-yfgfd)/(x(i+5061)-xfgfd)
C      theta=atan(slope)
C      theta=-theta
C      vx(i+5061)=frate*cos(theta)
C      vy(i+5061)=-frate*sin(theta)
C
C      end do
C
C      These are the calculations for the straight part f'e'
C      =====
C      slope=(y(5941)-y(5902))/(x(5941)-x(5902))
C      slopen=(-1.0/slope)

```

```

vbc(ncount) = value
write (70,2000) j, ncount, value
end do

vx for line bc
do i=1,40
j=i+861
ncod =1
value=vx(861+i)

ncount = ncount+1

ibc(ncount) = j
jbc(ncount) = ncod
vbc(ncount) = value

write (70,2000) j, ncod, value
end do

c
vx for curve cd
do i=1,40
j=i+1701
ncod =1
value=vx(1701+i)

ncount = ncount+1

ibc(ncount) = j
jbc(ncount) = ncod
vbc(ncount) = value

write (70,2000) j, ncod, value
end do

c
vx for curve de
do i=1,40
j=i+2541
ncod=1
value=vx(2541+i)

ncount = ncount+1

ibc(ncount) = j
jbc(ncount) = ncod
vbc(ncount) = value

write (70,2000) j, ncod, value
end do

c
vx for line ef
do i=1,40
j=i+3381
ncod=1
value=vx(i+3381)

ncount = ncount+1

ibc(ncount) = j
jbc(ncount) = ncod
vbc(ncount) = value

write (70,2000) j, ncod, value
end do

c
vx for curve fg
do i=1,40
j=i+4221
ncod=1
value=vx(4221+i)

ncount = ncount+1

ibc(ncount) = j
jbc(ncount) = ncod
vbc(ncount) = value

write (70,2000) j, ncod, value
end do

c
vx for curve gf'

```

```

do i=1,40
  j=i+5061
  ncod=1
  value=vx(i+5061)

  ncount = ncount+1

  jbc(ncount) = j
  jbc(ncount) = ncod
  vbc(ncount) = value

  write (70,2000) j, ncod, value
end do

c
  vx for line f'e'
  do i=1,40
    j=i+5901
    ncod=1
    value=vx(5901+i)

    ncount = ncount+1

    jbc(ncount) = j
    jbc(ncount) = ncod
    vbc(ncount) = value

    write (70,2000) j, ncod, value
  end do

c
  vx for curve e'd'
  do i=1,40
    j=i+6741
    ncod=1
    value=vx(6741+i)

    ncount = ncount+1

    jbc(ncount) = j
    jbc(ncount) = ncod
    vbc(ncount) = value

    write (70,2000) j, ncod, value
  end do

c
  vx for curve d'c'
  do i=1,40
    j=i+7581
    ncod=1
    value=vx(7581+i)

    ncount = ncount+1

    jbc(ncount) = j
    jbc(ncount) = ncod
    vbc(ncount) = value

    write (70,2000) j, ncod, value
  end do

c
  vx for line c'b'
  do i=1,40
    j=i+8421
    ncod=1
    value=vx(i+8421)

    ncount = ncount+1

    jbc(ncount) = j
    jbc(ncount) = ncod
    vbc(ncount) = value

    write (70,2000) j, ncod, value
  end do

c
  vx for curve b'a'
  do i=1,40
    j=i+9261
    ncod=1
    value=vx(9261+i)

    ncount = ncount+1

```

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```

jbc(ncount) = j
jbc(ncount) = ncod
vbc(ncount) = value

write (70,2000) j, ncod, value
end do

c
  vx for curve ah
  do i=0,20
    j=i+(41*1)
    ncod=1
    value=0.0

    ncount = ncount+1

    jbc(ncount) = j
    jbc(ncount) = ncod
    vbc(ncount) = value

    write (70,2000) j, ncod, value
  end do

c
  vx for curve a'h'
  do i=0,20
    j=9301+(40*i)
    ncod=1
    value=0.0

    ncount = ncount+1

    jbc(ncount) = j
    jbc(ncount) = ncod
    vbc(ncount) = value

    write (70,2000) j, ncod, value
  end do

c
  vy for curve ab
  do i=1,40
    j=i+1
    ncod=2
    value=vy(i+1)

    ncount = ncount+1

    jbc(ncount) = j
    jbc(ncount) = ncod
    vbc(ncount) = value

    write (70,2000) j, ncod, value
  end do

c
  vy for line bc
  do i=1,40
    j=i+861
    ncod=2
    value=vy(861+i)

    ncount = ncount+1

    jbc(ncount) = j
    jbc(ncount) = ncod
    vbc(ncount) = value

    write (70,2000) j, ncod, value
  end do

c
  vy for curve cd
  do i=1,40
    j=i+1701
    ncod=2
    value=vy(1701+i)

    ncount = ncount+1

    jbc(ncount) = j
    jbc(ncount) = ncod
    vbc(ncount) = value

    write (70,2000) j, ncod, value
  end do

```

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```

c      vy for curve de
      do i=1,40
        j=i+2541
        ncod=2
        value=vy(2541+i)
        ncount = ncount+1

        ibc(ncount) = j
        jbc(ncount) = ncod
        vbc(ncount) = value
        write (70,2000) j, ncod, value
      end do

c      vy for line ef
      do i=1,40
        j=i+3381
        ncod=2
        value=vy(i+3381)
        ncount = ncount+1

        ibc(ncount) = j
        jbc(ncount) = ncod
        vbc(ncount) = value
        write (70,2000) j, ncod, value
      end do

c      vy for curve fg
      do i=1,40
        j=i+4221
        ncod=2
        value=vy(4221+i)
        ncount = ncount+1

        ibc(ncount) = j
        jbc(ncount) = ncod
        vbc(ncount) = value
        write (70,2000) j, ncod, value
      end do

c      vy for curve gf
      do i=1,40
        j=i+5061
        ncod=2
        value=vy(i+5061)
        ncount = ncount+1

        ibc(ncount) = j
        jbc(ncount) = ncod
        vbc(ncount) = value
        write (70,2000) j, ncod, value
      end do

c      vy for line f'e'
      do i=1,40
        j=i+5901
        ncod=2
        value=vy(5901+i)
        ncount = ncount+1

        ibc(ncount) = j
        jbc(ncount) = ncod
        vbc(ncount) = value
        write (70,2000) j, ncod, value
      end do

c      vy for curve e'd'
      do i=1,40
        j=i+6741
        ncod=2
        value=vy(6741+i)

```

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```

        ncount = ncount+1
        ibc(ncount) = j
        jbc(ncount) = ncod
        vbc(ncount) = value
        write (70,2000) j, ncod, value
      end do

c      vy for curve d'c'
      do i=1,40
        j=i+7581
        ncod=2
        value=vy(7581+i)
        ncount = ncount+1

        ibc(ncount) = j
        jbc(ncount) = ncod
        vbc(ncount) = value
        write (70,2000) j, ncod, value
      end do

c      vy for line c'b'
      do i=1,40
        j=i+8421
        ncod=2
        value=vy(i+8421)
        ncount = ncount+1

        ibc(ncount) = j
        jbc(ncount) = ncod
        vbc(ncount) = value
        write (70,2000) j, ncod, value
      end do

c      vy for curve b'a'
      do i=1,39
        j=i+9261
        ncod=2
        value=vy(9261+i)
        ncount = ncount+1

        ibc(ncount) = j
        jbc(ncount) = ncod
        vbc(ncount) = value
        write (70,2000) j, ncod, value
      end do

c      Pressure for line hi
      do i=1,40
        j=821+ i
        ncod=3
        value=0.0
        ncount = ncount+1

        ibc(ncount) = j
        jbc(ncount) = ncod
        vbc(ncount) = value
        write (70,2000) j, ncod, value
      end do

c      Pressure for curve i'j
      do i=1,40
        j=1661+ i
        ncod=3
        value=0.0
        ncount = ncount+1

        ibc(ncount) = j
        jbc(ncount) = ncod
        vbc(ncount) = value
        write (70,2000) j, ncod, value

```

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```

end do

c
  Pressure for curve jk
  do i=1,40
    j=2501 + i
    ncod = 3
    value=0.0

    ncount = ncount+1

    ibc(ncount) = j
    jbc(ncount) = ncod
    vbc(ncount) = value

    write (70,2000) j, ncod, value
  end do

c
  Pressure for curve kl
  do i=1,40
    j=3341 + i
    ncod = 3
    value=0.0

    ncount = ncount+1

    ibc(ncount) = j
    jbc(ncount) = ncod
    vbc(ncount) = value

    write (70,2000) j, ncod, value
  end do

c
  Pressure for line lm
  do i=1,40
    j=4181 + i
    ncod = 3
    value=0.0

    ncount = ncount+1

    ibc(ncount) = j
    jbc(ncount) = ncod
    vbc(ncount) = value

    write (70,2000) j, ncod, value
  end do

c
  Pressure for curve mn
  do i=1,40
    j=5021 + i
    ncod = 3
    value=0.0

    ncount = ncount+1

    ibc(ncount) = j
    jbc(ncount) = ncod
    vbc(ncount) = value

    write (70,2000) j, ncod, value
  end do

c
  Pressure for curve nm
  do i=1,40
    j=5861 + i
    ncod = 3
    value=0.0

    ncount = ncount+1

    ibc(ncount) = j
    jbc(ncount) = ncod
    vbc(ncount) = value

    write (70,2000) j, ncod, value
  end do

c
  Pressure for line m'l'
  do i=1,40
    j=6701 + i
    ncod = 3

```

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```

value=0.0

ncount = ncount+1

ibc(ncount) = j
jbc(ncount) = ncod
vbc(ncount) = value

write (70,2000) j, ncod, value
end do

c
  Pressure for curve l'k'
  do i=1,40
    j=7541 + i
    ncod = 3
    value=0.0

    ncount = ncount+1

    ibc(ncount) = j
    jbc(ncount) = ncod
    vbc(ncount) = value

    write (70,2000) j, ncod, value
  end do

c
  Pressure for curve k'j'
  do i=1,40
    j=8381 + i
    ncod = 3
    value=0.0

    ncount = ncount+1

    ibc(ncount) = j
    jbc(ncount) = ncod
    vbc(ncount) = value

    write (70,2000) j, ncod, value
  end do

c
  Pressure for line j'i'
  do i=1,40
    j=9221 + i
    ncod = 3
    value=0.0

    ncount = ncount+1

    ibc(ncount) = j
    jbc(ncount) = ncod
    vbc(ncount) = value

    write (70,2000) j, ncod, value
  end do

c
  Pressure for curve i'h'
  do i=1,39
    j=10061 + i
    ncod = 3
    value=0.0

    ncount = ncount+1

    ibc(ncount) = j
    jbc(ncount) = ncod
    vbc(ncount) = value

    write (70,2000) j, ncod, value
  end do

c
  Concentration for curve ab
  do i=1,40
    j=i+1
    ncod = 4
    value=0.2

    ncount = ncount+1

    ibc(ncount) = j
    jbc(ncount) = ncod

```

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```

vbc(ncount) = value
write (70,2000) j, ncod, value
end do

c Concentration for line bc
do i=1,40
  j=i+861
  ncod=4
  value=0.2

  ncount = ncount+1

  ibc(ncount) = j
  jbc(ncount) = ncod
  vbc(ncount) = value

  write (70,2000) j, ncod, value
end do

c Concentration for curve cd
do i=1,40
  j=i+1701
  ncod=4
  value=0.2

  ncount = ncount+1

  ibc(ncount) = j
  jbc(ncount) = ncod
  vbc(ncount) = value

  write (70,2000) j, ncod, value
end do

c Concentration for curve de
do i=1,40
  j=i+2541
  ncod=4
  value=0.2

  ncount = ncount+1

  ibc(ncount) = j
  jbc(ncount) = ncod
  vbc(ncount) = value

  write (70,2000) j, ncod, value
end do

c Concentration for line ef
do i=1,40
  j=i+3381
  ncod=4
  value=0.2

  ncount = ncount+1

  ibc(ncount) = j
  jbc(ncount) = ncod
  vbc(ncount) = value

  write (70,2000) j, ncod, value
end do

c Concentration for curve fg
do i=1,40
  j=i+4221
  ncod=4
  value=0.2

  ncount = ncount+1

  ibc(ncount) = j
  jbc(ncount) = ncod
  vbc(ncount) = value

  write (70,2000) j, ncod, value
end do

c Concentration for curve gf'

```

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```

do i=1,40
  j=i+5061
  ncod=4
  value=0.2

  ncount = ncount+1

  ibc(ncount) = j
  jbc(ncount) = ncod
  vbc(ncount) = value

  write (70,2000) j, ncod, value
end do

c Concentration for line f'e'
do i=1,40
  j=i+5901
  ncod=4
  value=0.2

  ncount = ncount+1

  ibc(ncount) = j
  jbc(ncount) = ncod
  vbc(ncount) = value

  write (70,2000) j, ncod, value
end do

c Concentration for curve e'd'
do i=1,40
  j=i+6741
  ncod=4
  value=0.2

  ncount = ncount+1

  ibc(ncount) = j
  jbc(ncount) = ncod
  vbc(ncount) = value

  write (70,2000) j, ncod, value
end do

c Concentration for curve d'c'
do i=1,40
  j=i+7581
  ncod=4
  value=0.2

  ncount = ncount+1

  ibc(ncount) = j
  jbc(ncount) = ncod
  vbc(ncount) = value

  write (70,2000) j, ncod, value
end do

c Concentration for line c'b'
do i=1,40
  j=i+8421
  ncod=4
  value=0.2

  ncount = ncount+1

  ibc(ncount) = j
  jbc(ncount) = ncod
  vbc(ncount) = value

  write (70,2000) j, ncod, value
end do

c Concentration for curve b'a'
do i=1,39
  j=i+9261
  ncod=4
  value=0.2

  ncount = ncount+1

```

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```

      jbc(ncount) = j
      jbc(ncount) = ncod
      vbc(ncount) = value
      write (70,2000) j, ncod, value
      end do

1000  format (i5,2g20.12)
2000  format (2i5,g20.8)

c      rewind(70)

c      if (.not. eof(70)) read (70,2000) (jbc(ind), jbc(ind), vbc(ind)
c      1, ind=1,nbc)
c      print*, "boundary conditions array read"
c      write(60,3010)
c      write(60,3020) (jbc(ind), jbc(ind), vbc(ind), ind=1,nbc)
c      end if

      return

1010  format(2i5,g20.8)
3010  format(' ',// ' ', ' ',20('*'), ' ', nodal constraint ' ',20('*'),//
1' ', (8x,'id', '7x','dof',10x, 'value',10x)/)
3020  format(5x,i5,5x,i5,f17.4)

c      close(70)
c      return
c
c      =====
c      subroutine excelprint(iiii, excel, fr, pd, viisc)
c
c      implicit real*8 (A-H,O-Z)
c      dimension excel (6), fr(20), pd(20), viisc(20)
c
c      Function
c      -----
c      Prints the flow rate, viscosity, simulated pressure drop
c      values, compression factors and the percentage loss in filtration area
c
c      excel(5) = excel(5)*100
c      write(6l,100) fr(iiii), viisc(iiii), excel(2),
c      1      excel(3), excel(4), excel(5)
c      100 format(6(e15.4, 8x))
c
c      return
c      end
c
c      =====
c      e n d o f s u b r o u t i n e
c      =====

```

```

c *****
c Auxiliary Program for ACFAMP
c
c Developed by : Navraj S Hanspal & Atul N Waghode
c Supervised by : Prof V.Nassehi & Prof. R.J.Wakeman
c
c Latest Version: 23rd May, 2005
c *****
c
c Program Description
c
c This program generates the "Reference cartridge ID file"
c containing the cartridge characteristic data to be used
c in main execution of ACFAMP
c
c INPUT TO BE SUPPLIED BY THE USER
c
c 1. Reference ID of the FILTER ELEMENT
c 2. Height of pleat in (mm)
c 3. Height of element in (mm)
c 4. Filtering area in (m2)
c 5. Diameter of the inner core in (mm)
c 6. Centre co-ordinate of the repetitive cartridge filter domain
c 7. Density of fluid (kg/m3)
c 8. Total number of data sets to be used in analysis
c 9. Flow rate (lit/min) corresponding to each data set
c 10. Viscosity (cSt) corresponding to each data set
c 11. Assumed percentage filtration area loss for each data set
c
c =====
c Program FilterData
c
c implicit real*8 (a-h,o-z)
c
c dimension fr(20), pd(20), visc(20)
c
c print *, "
c 1 Program Developers: N.S Hanspal and A.N. Waghode"
c print *, "
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c print *, "
c 1 print *, " Advanced Separation Technologies Group"
c 1 print *, " Department of Chemical Engineering"
c 1 print *, " Loughborough University"
c 1 print *, " Loughborough, Leicestershire"
c 1 print *, "
c 1 print *, " IE11 3TU, United Kingdom"
c
c print *, "=====
c print *, "ACFAMP AUXILIARY PROGRAM"
c print *, "=====
c print *, "=====
c
c write(*, 1101)
c write(*, 1111)
c write(*, 1121)
c write(*, 1131)
c
c
c Opening of file to be used for the FILTER ANALYSIS code
c =====
c print*, 'Enter the Reference ID of the FILTER ELEMENT'
c read(*,100) filnam
c
c open(unit=51, file=filnam, access='sequential', form='formatted',
c status='unknown', iostat=iost)
c
c Input the Geometrical Parameters of the Filter Element from the Excel Sheets

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c =====
c print*, 'Enter the height of pleat in (mm) ='
c read*, hp
c print*, 'Enter the number of pleats ='
c read*, np
c print*, 'Enter the height of element in (mm) ='
c read*, el
c print*, 'Enter the filtering area in (m2) ='
c read*, fa
c print*, 'Enter the diameter of the inner core in (mm) ='
c read*, di
c
c Input the co-ordinates to be used for evaluation of Boundary Conditions
c =====
c print*, 'Read the 1st set of co-ordinate : x,y'
c read*, xab,yab
c print*, 'Read the 2nd set of co-ordinate : x,y'
c read*, xj1,yj1
c print*, 'Read the 1st set of co-ordinate : x,y'
c read*, xj1d,yj1d
c print*, 'Read the 1st set of co-ordinate : x,y'
c read*, xj1kd,yj1kd
c print*, 'Read the 1st set of co-ordinate : x,y'
c read*, xabkd,yabkd
c
c Input the Density of Fluid
c =====
c print*, 'Enter the density in (kg/m3) ='
c read*, density
c
c Total number of data sets i.e. Flow Rate, Pressure Drop and Viscosity Data for the Filter
c Element
c =====
c print*, 'Enter the total number of data sets ='
c read*, ntd
c
c Input the Flow Rate, Pressure Drop and Viscosity Data the Filter Element from the Excel S
c heets
c =====
c do i=1,ntd
c jj=1
c 1 print*, 'Enter the flow rate in (lit/min), percentage loss in area
c and viscosity in (cSt)'
c read*, fr(jj),pd(jj),visc(jj)
c pd(jj)=pd(jj)/100.0
c end do
c
c Writing in the data file to be used by Filter Analysis Code
c =====
c write the total number of sets of data
c write(51,2001) ntd
c
c Write the total filtering area and density
c write(51,2005) fa, density
c
c Write the Flow Rate in (lit/min), Pressure Drop in (bar) and Viscosity in (Pa.s)
c do i=1,ntd
c jj=1
c visc(jj)=visc(jj)*0.00001*density
c write(51,2002) fr(jj),pd(jj),visc(jj)

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end do

c      Write the co-ordinates in (m) to be used for the calculation of boundary conditions
c      -----
c      write(51,2003) xab,yab
c      write(51,2003) xjl,yjl
c      write(51,2003) xfgfd,yfgfd
c      write(51,2003) xldcdjd,yldcdjd
c      write(51,2003) xabdd,yabdd

c      Write the Geometrical Parameters of the Filter Element
c      -----
c      write(51,2004) np      ! Number of Pleats
c      write(51,2004) hp      ! Height of Filter Element (mm)
c      write(51,2004) el      ! Length of Pleat (mm)
c      write(51,2004) dl      ! Height of Filter Element (mm)

100   format(80a)
2001  format(15)
2002  format(10x,d10.5,10x,d10.5,10x,d10.5)
2003  format(5x,g22.12,g22.12)
2004  format(10x,f10.5)
2005  format(10x,d10.5,10x,d10.5)

1101  format(' ',/)
1111  format('/',) This auxiliary program generates the Reference
      ! Cartridge ID file ' ' to be used in execution of ACPAMP.
      ! It will now ask the user to input ' ' relevant data to be
      ! used in cartridge filter analysis '
1121  format(' ',2(/))

1131  format(' *****')
      ! *****

      close (51)
end

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