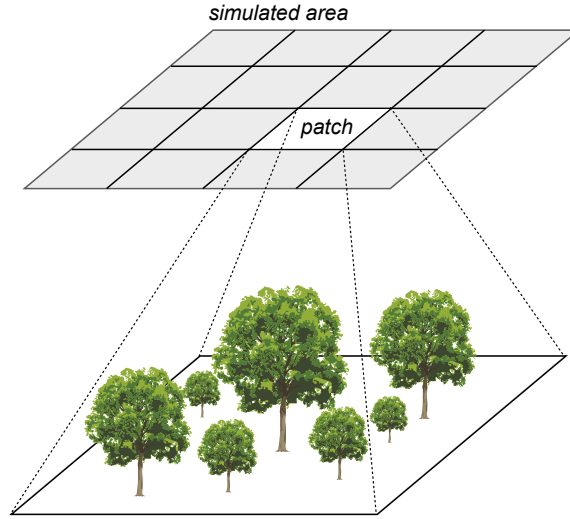


## A General concept

FORMIND 3.0 is an individual-based, spatially explicit and process-based model designed for simulating species-rich vegetation communities. This document introduces only a specific version of FORMIND 3.0 (SVN-Built 1080) which simulates forest dynamics at central Europe. For a full model description of FORMIND 3.0 please go to [www.formind.org](http://www.formind.org). The full description shows the entire range of different model versions, which can be currently applied (i.e. the choices of different geometries of the vegetation, of the climatic zone or of various disturbance events).

In FORMIND 3.0 vegetation is simulated on an area of size  $A_{area}$ , which is a composite of regularly ordered, quadratic patches of size  $A_{patch}$  [m<sup>2</sup>] uniquely described by their location within the area (Fig. 1). Individual trees grow within the patches, but do not have spatially explicit positions within a patch.



**Figure 1:** Illustration of the simulated area and its composition of regularly ordered patches. Individual trees do not have spatially explicit positions within the patches. Only for an illustrative purpose, we show positioned trees on an exemplary patch.

The trees change their size during the simulation according to a type-specific set of eco-physiological and morphological parameters used within the modelled processes. The modelled processes are simulated on different levels: (i) area-level, (ii) patch-level or (iii) on the level of a single tree .

Within each time step  $t_y$ , the following main processes are calculated:

- **Chapter C - Environment**

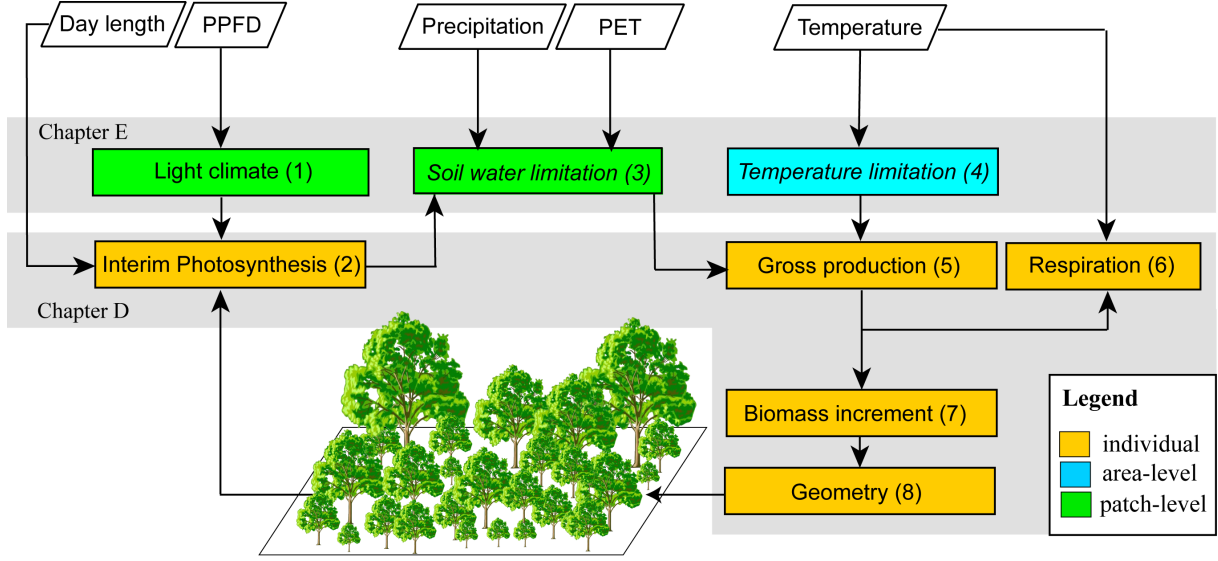
The patches of the simulation area are homogeneously concerning climatic input variables. Based on these input parameters, the environment of the trees is specified. For example, the radiation above canopy and day length are equal for all patches. The vertical attenuation of the incoming radiation (i.e. light climate) is calculated for each patch based on the vegetation, so that light intensity at different heights can differ between patches dependent on the number of trees shading each other. Reduced light availability for shaded individuals can result in a reduced gross photosynthesis. Limited soil water resources can also reduce the gross photosynthesis of an individual. In the same manner as the light climate, soil water contents can differ between patches during the simulation, although the initial soil water content and other soil properties (e.g. soil porosity) are equal for all patches. Differences in soil water content between patches are dependent on the number of trees per patch, which take up soil water resources. Further, type-specific effect of air temperature can also limit gross photosynthesis and affect respiration of an individual. All limitations are calculated in time steps of higher resolution than  $t_y$ .

- **Chapter D - Growth**

The growth of a single tree is determined by its gross productivity, respiration and type-specific morphological parameters. Respiration is calculated on the level of an individual. An increase in biomass per tree is modelled as the difference between gross photosynthesis and respiration. The allocation of the resulting biomass increase (including the increase of geometrical properties according to chapter B) act on the level of a tree .

The modelled processes, which are summarized within the above mentioned main processes, are scheduled in a serial way. For details on the modelled processes and their schedule see Fig. 2.

For the purpose of calculations within the processes of light climate and crowding mortality, the above-ground space is discretized into vertical height layers of constant width  $\Delta h$ . Table 1 shows general input parameters.



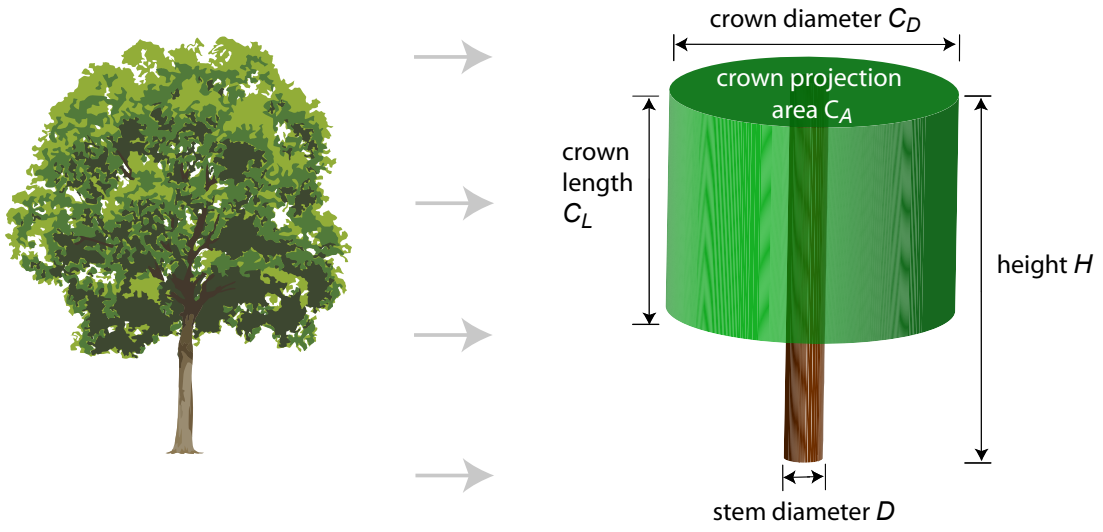
**Figure 2:** Block diagram of the modelled processes. Different colours indicate the spatial scale on which each process is calculated (blue = area, green = patch, orange = individual). *Italic written boxes show processes which are simulated with time steps of higher resolution than  $t_y$ .* Numbers in brackets within each box show the serial order of their calculation within one time step  $t_y$ . Grey frames that underly these boxes group them according to the above mentioned main processes and their corresponding chapters. Rhombuses indicate climatic input parameters with the following abbreviations: PET – potential evapotranspiration, PPFD – photoactive photon flux density.

**Table 1:** General and technical parameters.

Name	Symbol	Value	Unit
Simulation time	$t_{end}$	1	year
Time step	$t_y$	1	year
Simulation area	$A_{area}$	1	hectare
Patch area	$A_{patch}$	400	$m^2$
Number PFTs	$MaxGrp$	up to 8	-
Width of height layers	$\Delta h$	0.5	m

## B Geometry

Although individual trees in real forests should not have necessarily identical shapes, we model each tree by a cylindrical stem and a cylindrical crown (Fig. 3). The geometry of an individual can be described completely by the following size characteristics: stem diameter ( $D$ ), height ( $H$ ), crown diameter ( $C_D$ ), crown length ( $C_L$ ) and crown projection area ( $C_A$ ) as shown in Fig. 3.



**Figure 3:** Geometrical representation of a single tree . The following abbreviations describe size characteristics of the modelled tree geometry:  $D$  - stem diameter,  $H$  - height,  $C_D$  - crown diameter,  $C_L$  - crown length,  $C_A$  crown projection area.

These size characteristics are functionally related to each other. In the following, we describe the functional relationships used. Parameters of the described relationships can vary between different tree types.

### B.1 Height - Stem Diameter - Relationship

The height  $H$  [m] of a tree relates to its stem diameter  $D$  [cm] by:

$$H = \frac{D}{\frac{1}{h_0} + \frac{D}{h_1}}, \quad (1)$$

where  $h_0$  and  $h_1$  are type-specific parameters.

## B.2 Crown length - Height - Relationship

The crown length  $C_L$  [m] of a tree is modelled as a fraction of its height  $H$  [m]:

$$C_L = \left( -\frac{c_{l0} \cdot H \cdot c_{l1}}{c_{l0} \cdot H + c_{l1}} + c_{l2} \right) \cdot H, \quad (2)$$

where  $c_{l0}$ ,  $c_{l1}$  and  $c_{l2}$  are type-specific parameter.

## B.3 Crown diameter - Stem diameter - Relationship

The second dimension of the cylindrical crown, i.e. the crown diameter  $C_D$  [m] of a tree relates to its stem diameter  $D$  [cm] by:

$$C_D = D \cdot (c_{d0} + c_{d1} \cdot \exp(-c_{d2} \cdot D)), \quad (3)$$

where  $c_{d0}$ ,  $c_{d1}$  and  $c_{d2}$  are type-specific parameters.

## B.4 Crown area - Crown diameter - Relationship

The crown projection area  $C_A$  [m<sup>2</sup>] of a tree is simply the ground area of the modelled cylindrical crown:

$$C_A = \frac{\pi}{4} \cdot C_D^2. \quad (4)$$

## B.5 Aboveground biomass - Stem diameter - Relationship

The aboveground volume of a tree captures biomass (i.e. organic dry matter). Aboveground biomass  $B$  in [t<sub>ODM</sub>] of a tree is modelled in relation to its stem diameter  $D$  [cm] by:

$$B = \exp \left( b_0 \cdot (\log(D) - b_2) \cdot \frac{2 \cdot b_1 + (\log(D) - b_2)}{b_1 + (\log(D) - b_2)} \right), \quad (5)$$

whereby  $b_0$ ,  $b_1$  and  $b_2$  are type-specific parameters.

## B.6 Leaf area index - Stem diameter - Relationship

In general, aboveground biomass is divided between woody biomass captured in the stem and green biomass captured in the crown leaves. Important for the photosynthetic production of a tree is the green biomass captured in crown leaves. As leaves absorb radiation for photosynthesis, the total amount of one-sided leaf area per unit of crown projection area (i.e. the individual's leaf area index) is of main interest. The leaf area index  $LAI$  [ $\text{m}^2/\text{m}^2$ ] of a tree relates functionally to its stem diameter  $D$  [cm] by:

$$LAI = l_0 \cdot D^{l_1}, \quad (6)$$

whereby  $l_0$  and  $l_1$  are type-specific parameters.

All parameters mentioned above are listed in Tab.2.

**Table 2:** Summary of the type-specific morphological parameters based on Schober [1995] yield class 1 (expection: populus: only yield class 2 available)

tree type	$h_{max}$	$b_1$	$b_2$	$b_3$	$h_1$	$h_2$	$c_1$	$c_2$	$c_3$
pinus	46	1.185	5.657	3.676	1.259	75.762	0.156	0.152	0.204
picea	50	1.029	3.204	3.717	1.326	101.33	0.128	0.102	0.089
fagus	43.7	1.202	5.727	3.475	1.916	61.036	0.155	0.125	0.066
quercus	40	1.151	5.187	3.586	1.879	45.341	0.173	0.054	0.066
populus	37	1.266	5.636	3.809	1.286	62.651	0.173	0.614	0.087
fraxinus	40	1.192	5.957	3.534	1.976	52.925	0.171	0.146	0.066
betula	32	1.091	6.394	3.671	1.711	51.488	0.207	1.760	0.277
robinia	27	1.217	9.175	3.586	1.400	45.315	0.161	0.493	0.120

## B.7 Maximum Values

The trees cannot grow indefinitely in FORMIND 3.0 . Therefore, we introduce the following maximum values for a plausible geometry of a mature individual:

- maximum stem diameter  $D_{max}$  [m]
- maximum height  $H_{max}$  [m]
- maximum biomass  $B_{max}$  [ $t_{ODM}$ ]

Either the maximum stem diameter or the maximum height is given as a type-specific input parameter. Those two maximum values, which are not predefined, are then derived using the functional relationships mentioned in [section B.1](#) and [section B.5](#). The maximum values are used in [section D](#).

## C Competition and environmental limitations

### C.1 Light climate

A single tree on a patch receives full incoming radiation. An increasing number of individual trees of differing heights on a patch results in shading within the canopy. Higher trees partly intercept radiation, which is not available for smaller individuals. Thus, with decreasing height from the canopy down to the ground, radiation is increasingly attenuated. We call this vertical distribution of light availability within a patch 'light climate'.

To calculate the light availability in different heights within the canopy, the vertical discretization of the above-ground space is used (i.e. height layers of constant width  $\Delta h$ ). For each patch and height layer, the leaf area accumulated by all trees on the patch is calculated. Each tree contributes parts of its crown leaf area to those height layers, which are occupied by its crown (i.e. height layers from  $l_{min}$  to  $l_{max}$ ). These limits are determined by the individual's crown length  $C_L$  and its height  $H$ :

$$l_{max} = \left\lfloor \frac{H}{\Delta h} \right\rfloor \quad (7)$$

$$l_{min} = \left\lfloor \frac{H - C_L}{\Delta h} \right\rfloor. \quad (8)$$

The number of height layers a tree is occupying by its crown ( $\#_{layer}$ ) can then be calculated by:

$$\#_{layer} = l_{max} - l_{min}. \quad (9)$$

For those height layers between  $l_{min}$  and  $l_{max}$ , an individual's leaf area contributes equally to each layer  $i$ :

$$\bar{L}_i = \frac{LAI \cdot C_A}{\#_{layer}}, \quad (10)$$

whereby  $\bar{L}_i$  [m<sup>2</sup>] represents the contribution of an tree's leaf area to the layer  $i$ ,  $LAI$  [-] is the leaf area index of the tree (see section B.6) and  $C_A$  [m<sup>2</sup>] is crown projection area of the tree's crown. The multiplication of  $LAI$  by  $C_A$  results in the leaf area in [m<sup>2</sup>] of an single tree.

Summing up all contributions of the trees' leaf area per patch to their respective occupied height layers and relative to the patch area, results in the patch-based leaf area index  $\hat{L}_i$  [-] per layer  $i$ :

$$\hat{L}_i = \frac{1}{A_{patch}} \sum_{\substack{\text{all individuals} \\ \text{with } l_{min} \leq i \leq l_{max}}} \bar{L}_i, \quad (11)$$

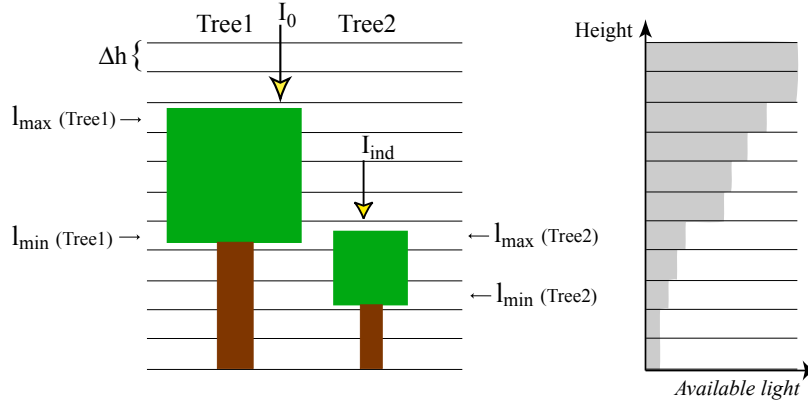


where  $\bar{L}_i$  [m<sup>2</sup>] represents the leaf area contribution of an tree to the height layer  $i$  and  $A_{patch}$  [m<sup>2</sup>] denotes the area of a patch.

Using this information, the radiation each tree is able to intercept can be determined. Light attenuation through the canopy is calculated using the approach of [Monsi and Saeki, 1953]. The incoming radiation  $I_{ind}$  on top of a tree (i.e. on top of the height layer  $l_{max}$  the tree is reaching) is calculated by:

$$I_{ind} = I_0 \cdot \exp \left( -k \cdot \sum_{i>l_{max}} \hat{L}_i \right), \quad (12)$$

where the sum in the exponent accumulates the patch-based leaf area indices of all height layers above the individual's height. The parameter  $k$  denotes the light extinction coefficient [-] of a tree,  $I_0$  [ $\mu$ mol (photons)/m<sup>2</sup> s] is the daily radiation above canopy averaged from sunrise to sunset during the vegetation period and  $\hat{L}_i$  [-] represents the patch-based leaf area index of height layer  $i$ .



**Figure 4:** Illustration of the light climate on the example of two single trees . The limits of each crown are shown by  $l_{min}$  (Tree1),  $l_{max}$ (Tree1),  $l_{min}$ (Tree2) and  $l_{max}$ (Tree2). The vertically discretized aboveground space into height layers of width  $\Delta h$  [m] is coloured differently according to the available radiation. The lighter the colour is, the more attenuated the radiation is, which results from the absorption by higher individuals' leaves. On the right hand side the decrease of available light from the canopy to the floor is illustrated by the grey polygon. Thereby, attenuation is greatest in the height layer both trees occupy by their crowns (i.e. layer  $l_{min}$ (Tree1) and  $l_{max}$ (Tree2)).

By determining the available radiation for each single tree , competition for light between trees is considered.

**Table 3:** tree type specific leaf area index (LAI) measurements of *Breuer et al. [2003]*. (*n*) is number of used measurements. Robinia is estimated as mean of quercus and populus because of same light value by Ellenberg.

tree type	$LAI \text{ m}^2/\text{m}^2$ (n)	<i>sd</i>
pinus	3.6 (2)	1.0
picea	7.7 (4)	2.1
fagus	6.1 (6)	0.9
quercus	5.4 (4)	0.7
populus	4.6 (7)	1.6
fraxinus	5.0 (1)	-
betula	5.3 (1)	-
robinia	5.0 (0)	-

## C.2 Water cycle and soil water limitation

Individual trees take up soil water resources to fulfill the requirements for their gross productivity. Instead of modelling the roots of the trees, we determine an individual's uptake of soil water based on its demand and on the total available soil water.

Firstly, the soil water content  $\Theta_{soil}$  is computed preliminary on an hourly basis using a differential equation, which quantifies preliminary hourly changes in the soil water content per patch depending on precipitation  $PR$ , interception  $IN$  and run-off  $RO$  (Fig. 5, cf. [Kumagai et al., 2004]):

$$\frac{d\Theta_{soil}}{dt} = PR(t) - IN(t) - RO(t). \quad (13)$$

The resulting soil water content represents the total available soil water before soil water uptake by individuals. Uptake of soil water resources by trees is modelled equal to their transpiration and subtracted from  $\Theta_{soil}$  later within the timestep (see eqn. 24).

The **interception**  $IN$  [mm/h] is calculated dependent on the total leaf area index per patch (i.e.  $\sum_i \hat{L}_i$  in [-], cf. [Liang et al., 1994]):

$$IN(t) = \min(K_L \cdot \left( \sum_i \hat{L}_i \right), PR(t)), \quad (14)$$

where  $K_L$  [mm/h] is the interception constant and  $PR$  [mm/h] denotes the precipitation.

On the ground surface of a patch, we consider two different run-offs: surface run-off and subsurface run-off:

$$RO(t) = RO_{\rightarrow}(t) + RO_{\downarrow}(t), \quad (15)$$

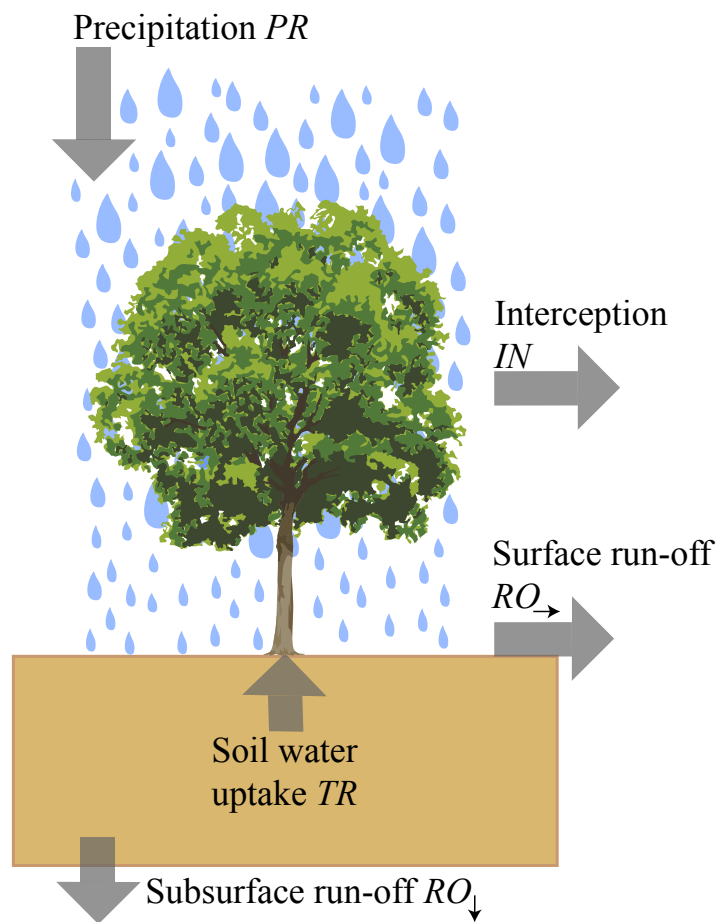
where **surface run-off**  $RO_{\rightarrow}$  [mm/h] is defined in the following way:

$$RO_{\rightarrow} = \max(0, \Theta_{soil}(t) + PR(t) - IN(t) - POR) \quad (16)$$

with  $POR$  [mm/h] denoting the soil porosity (i.e. defined as the maximum water intake of the soil per patch).

For the calculation of the **subsurface run-off**  $RO_{\downarrow}$  due to gravitation, we use the Brooks-Corey relation (cf. [Liang et al., 1994]):

$$RO_{\downarrow} = K_s \cdot \left( \frac{\Theta_{soil}(t) - \Theta_{res}}{POR - \Theta_{res}} \right)^{\frac{2}{\lambda} + 3}, \quad (17)$$



**Figure 5:** Illustration of the water cycle on the example of a single tree .

where  $K_s$  [mm/h] is the fully saturated conductivity,  $\Theta_{res}$  [mm/h] the residual water content, and  $\lambda$  [-] the pore size distribution index.

The preliminary soil water content  $\Theta_{soil}$  represents the soil water content, which is available for the individuals' uptake or transpiration. To calculate the **transpiration**  $TR$  [mm/h] of all trees per patch, we use the water-use-efficiency concept (cf. [Lambers et al., 2008]):

$$TR = \frac{1}{A_{patch}} \sum_{all\ trees} \frac{GPP}{WUE}, \quad (18)$$

whereby  $GPP$  in [ $g_{ODM}/h$ ] denotes the hourly gross primary production of an individual on the patch (see section D). Please note, that we simulate  $GPP$  per time step  $t_y$ . To calculate  $GPP$  on an hourly basis, we divide  $GPP$  [ $g_{ODM}/t_y$ ] by the number of hours within the time step  $t_y$ . The constant type-specific value  $WUE$  in [ $g_{ODM}/kg_{H_2O}$ ] represents the water-use-efficiency parameter and  $A_{patch}$  [ $m^2$ ] the area of a patch.

The resulting transpiration  $TR$  may be limited in three ways calculated in a serial way:

**PET limitation** Transpiration can be limited by the potential evapotranspiration  $PET$  [mm/h] and the interception  $IN$  [mm/h] (calculated by eqn. 14):

$$TR = \begin{cases} TR(t) & , TR(t) \leq PET(t) - IN(t) \\ PET(t) - IN(t) & , TR(t) > PET(t) - IN(t) \end{cases}. \quad (19)$$

**Soil water limitation** Transpiration can be limited by the preliminary soil water content  $\Theta_{soil}$  [mm/h] (calculated by eqn. 13) and the permanent wilting point  $\Theta_{pwp}$  [mm/h]:

$$TR = \begin{cases} TR(t) & , \Theta_{soil}(t) - TR(t) \geq \Theta_{pwp} \\ \Theta_{soil}(t) - \Theta_{pwp} & , \Theta_{soil}(t) - TR(t) < \Theta_{pwp} \\ 0 & , \Theta_{soil}(t) \leq \Theta_{pwp} \end{cases}. \quad (20)$$

**Competition for water** Competition between trees can limit the transpiration in the following way:

$$TR = \varphi_W \cdot TR(t), \quad (21)$$

where  $\varphi_W$  [-] represents a reduction factor ranging between 0 and 1.

The reduction factor  $\varphi_W$  is calculated using the approach of [Granier et al., 1999], which is based on the preliminary soil water content (calculated by eqn. 13):

$$\varphi_W = \begin{cases} 0 & , \Theta_{soil}(t) \leq \Theta_{pwp} \\ \frac{\Theta_{soil}(t) - \Theta_{pwp}}{\Theta_{msw} - \Theta_{pwp}} & , \Theta_{pwp} < \Theta_{soil}(t) < \Theta_{msw} \\ 1 & , \Theta_{soil}(t) \geq \Theta_{msw} \end{cases}, \quad (22)$$

**Table 4:** *water circle relevant parameters*

parameter	unit	value	reference
$WUE$	$g\ odm\ kg^{-1}H_2O^{-1}$	6.0	Larcher [2001]
$\Theta_{pwp}$	$V\%$	19.4	Maidment [1993]
$F_c$	$V\%$	31.0	Maidment [1993]
$k_L$	$mm\ d^{-1}$	0.2	Dickinson [1984]
$por$	$V\%$	46.3	Maidment [1993]
$k_s$	$m\ s^{-1}$	$3.66\ 10^{-6}$	Maidment [1993]
$\Theta_r$	$V\%$	2.7	Maidment [1993]

where  $\Theta_{pwp}$  is the permanent wilting point in  $[V\%]$  and  $\Theta_{msw}$  is the minimum soil water content in  $[V\%]$ . For the purpose of the calculation of eqn. 22 only,  $\Theta_{soil}$  needs to be converted from  $[mm/h]$  to  $[V\%]$ . Thereby, the soil is modelled down to a constant depth  $[m]$  defined prior to the start of the simulation.

The value of  $\Theta_{msw}$  is determined according to [Granier et al., 1999] by:

$$\Theta_{msw} = \Theta_{pwp} + 0.4(\Theta_{fc} - \Theta_{pwp}) \quad (23)$$

whereby  $\Theta_{fc}$  denotes the field capacity in  $[V\%]$ .

The soil water content in the next day step is then calculated by the difference between the preliminary soil water content (calculated by eqn. 13) and the (eventually limited) transpiration  $TR$ :

$$\frac{d\Theta_{soil}}{dt} = \Theta_{soil}(t) - TR(t). \quad (24)$$

### C.3 Temperature

The gross primary production  $GPP$  [ $t_{ODM}/t_y$ ] of a tree (see section D) may be influenced by phenology (esp. in the temperate zone) and air temperature. Respiration for maintenance purposes of an individual (see section D) may also be affected by air temperature. The influence on both - gross productivity and respiration, is modelled using limitation factor, by which they are simply multiplied (see section D). In the following, we describe the calculations of these limitation factors:

#### Phenology

Individual trees only produce gross primary production  $GPP$  during their photosynthetic active period. In the **temperate zone**, we distinguish between broad-leaf and needle-leaf trees. Only deciduous broad-leaf trees have two phenology phases: (i) a dormant phase during winter and (ii) a photosynthetic active period of  $\varphi_{act}$  [days] after bud-burst until fall (i.e. the vegetation period).

The date of bud-burst is reached, if the temperature sum (daily mean air temperatures  $> 5^\circ$ ) since 1 January is higher than a critical temperature  $T_{crit}$ :

$$T_{crit} = -68 + 638 e^{-0.01 \cdot n}, \quad (25)$$

where  $n$  is the number of days per time step  $t_y$  with an air temperature below  $5^\circ$  since 1 November of the previous year. This algorithm is based on the global distribution of leaf onset dates estimated from remote sensing data [Botta et al., 2000]. The photosynthetic active period stops if the 10-day moving average of daily mean air temperatures falls below  $9^\circ C$  [Sato et al., 2007].

In contrast to the broad-leaf trees, the photosynthetic active period  $\varphi_{act}$  of needle-leaf trees amounts a complete year of 365 days (without any dormant phase).

In the **tropical zone**, we assume for all individuals irrespective of their type a complete photosynthetic active period with  $\varphi_{act} = 365$  days.

#### Temperature limitation of gross productivity

The gross primary production of a tree can be reduced due to unfavorable air temperatures. A corresponding limitation factor  $\varphi_T$  is calculated by:

$$\varphi_T = \frac{1}{n} \sum_1^n \varphi_{T,l} \cdot \varphi_{T,h}, \quad (26)$$

where  $n$  is the number of days per time step  $t_y$  and the values  $\varphi_{T,l}$  and  $\varphi_{T,h}$  are the daily inhibition factors for low and high air temperatures [Gutiérrez and Huth, 2012; Haxeltine and Prentice, 1996].

The **inhibition factor for low air temperatures**  $\varphi_{T,l}$  [ $^{\circ}C$ ] is calculated by:

$$\varphi_{T,l} = (1 + e^{k_0 \cdot k_1 - T})^{-1}, \quad (27)$$

where  $T$  [ $^{\circ}C$ ] is the daily mean air temperature and  $k_0$  and  $k_1$  are type-specific parameters.

These parameters  $k_0$  and  $k_1$  are calculated by:

$$k_0 = \frac{2 \ln(0.01/0.99)}{T_{CO_2,l} - T_{cold}} \quad (28)$$

$$k_1 = 0.5 (T_{CO_2,l} + T_{cold}) \quad (29)$$

where  $T_{CO_2,l}$  [ $^{\circ}C$ ] and  $T_{cold}$  [ $^{\circ}C$ ] are type-specific parameters representing the lower temperature limit for  $CO_2$  assimilation and the monthly mean air temperature of the coldest month an individual can cope with, respectively.

Similarly, the **inhibition factor for high air temperatures**  $\varphi_{T,h}$  in  $^{\circ}C$  is calculated by:

$$\varphi_{T,h} = 1 - 0.01 \cdot e^{k_2 (T - T_{hot})} \quad (30)$$

where  $k_2$  is a type-specific parameter,  $T$  [ $^{\circ}C$ ] is the daily mean temperature and  $T_{hot}$  [ $^{\circ}C$ ] is the type-specific mean temperature of the hottest month an individual can occur.

The parameter  $k_2$  is calculated as:

$$k_2 = \frac{\ln(0.99/0.01)}{T_{CO_2,h} - T_{hot}}, \quad (31)$$

whereby  $T_{CO_2,h}$  [ $^{\circ}C$ ] and  $T_{hot}$  [ $^{\circ}C$ ] are type-specific parameters representing the higher temperature limit for  $CO_2$  assimilation and the monthly mean air temperature of the warmest month an individual can cope with, respectively.

### Temperature limitation of maintenance respiration

Maintenance respiration is assumed to change exponentially with air temperature represented by the limitation factor  $\kappa_T$  [Prentice et al., 1993]:

$$\kappa_T = \frac{1}{n} \sum_{i=1}^n Q_{10}^{\left(\frac{T - T_{ref}}{10}\right)}, \quad (32)$$



where  $n$  is the number of days per time step  $t_y$ ,  $T$  [ $^{\circ}C$ ] is the daily mean air temperature,  $Q_{10}$  [-] and  $T_{ref}$  [ $^{\circ}C$ ] are constant parameters, irrespective of type.  $T_{ref}$  represents the reference temperature, at which maintenance respiration is not influenced. Air temperatures below  $T_{ref}$  result in a decrease of maintenance respiration ( $\kappa_T < 1$ ) and those above  $T_{ref}$  in an increase of maintenance respiration ( $\kappa_T > 1$ ).

**Table 5:** Warmest and coldest month where the tree species can cope with using distribution maps and the climate diagrams of *J.Müller* [1996].

tree type	$T_{hot}$ $^{\circ}C$	$T_{cold}$ $^{\circ}C$	$T_{ref}$ $^{\circ}C$	$Q_{10}$
pinus	26.55	-2.33	10.47	2.3
picea	26.55	-9.9	10.47	2.3
fagus	22.00	-3.2	10.47	2.3
quercus	23.5	-3.9	10.47	2.3
populus	27.0	-6.90	10.47	2.3
fraxinus	25.55	-6.61	10.47	2.3
betula	21.5	-9.9	10.47	2.3
robinia	24.5	-9.1	10.47	2.3

## D Growth of a tree

### D.1 Interim photosynthesis

Based on the incoming irradiance on top of a tree  $I_{ind}$  (see section C), organic dry matter is produced via gross photosynthesis. In this section the interim photosynthesis is calculated without reduction due to limited soil water availability nor temperature effects.

The interim gross photosynthesis  $P_{ind}$  of an individual is modelled using the approach of [Thornley and Johnson, 1990]. It is based on the single-leaf photosynthesis modelled by a Michaelis-Menten function – a typical saturation function describing the relation between the radiation  $I_{leaf}$  available on top of a leaf and its gross photosynthetic rate  $P_{leaf}$ :

$$P_{leaf}(I_{leaf}) = \frac{\alpha \cdot I_{leaf} \cdot p_{max}}{\alpha \cdot I_{leaf} + p_{max}}, \quad (33)$$

where  $\alpha$  is the quantum efficiency, also known as the initial slope of the type-specific light response curve,  $I_{leaf}$  is the incoming irradiance on top of the surface of a single leaf within the individual's crown and  $p_{max}$  is the maximum leaf gross photosynthetic rate.

To obtain the incoming irradiance on top of the surface of a single leaf  $I_{leaf}$ , the available irradiance  $I_{ind}$  on top of the entire individual has to be modified:

$$I_{leaf}(L) = \frac{k}{1-m} I_{ind} \cdot e^{-k \cdot L}, \quad (34)$$

where  $k$  [-] is the type-specific light extinction coefficient,  $m$  [-] represents the transmission coefficient and  $I_{ind}$  denotes the available incoming irradiance on top of a tree .

The first part  $\frac{k}{1-m} I_{ind}$  in eqn. (34) is correcting the incoming irradiance in order to obtain those parts, which can be absorbed by a leaf. The second part  $e^{-k \cdot L}$  in eqn. (34) accounts for self-shading within the individual's crown. As the leaves of an individual are assumed to be homogeneously distributed within its crown, some leaves will be shaded by higher ones within the crown. Thereby,  $L = 0$  represents the top of the individual and  $L = LAI$  represents the bottom of the individual's crown with  $LAI$  being its leaf area index (see section B).

To obtain the interim gross photosynthetic rate of a tree per year  $P_{ind}$ , the single-leaf photosynthesis of eqn. (33) is integrated over the individual's leaf area index  $LAI$  (see section B):

$$P_{ind} = \int_0^{LAI} P_{leaf}(I_{leaf}(L)) dL. \quad (35)$$

The integration results in the interim photosynthesis of an tree per year [Thornley and Johnson, 1990]:

$$P_{ind} = \frac{p_{max}}{k} \cdot \ln \frac{\alpha k I_{ind} + p_{max}(1 - m)}{\alpha k I_{ind} e^{-k \cdot LAI} + p_{max}(1 - m)}. \quad (36)$$

To convert the interim photosynthesis  $P_{ind}$  from  $[\mu mol_{CO_2}/m^2s]$  to  $[t_{ODM}/y]$ ,  $P_{ind}$  has to be multiplied by the individual's crown area  $C_A$  (see section B), the type-specific photosynthetic active period  $\varphi_{act}$  and finally a conversion factor  $c_{odm}$ :

$$P_{ind} \cdot C_A \cdot 60 \cdot 60 \cdot l_{day} \cdot \varphi_{act} \cdot \varphi_{odm}, \quad (37)$$

where the multiplication by  $60 \cdot 60$  accounts for the conversion from seconds to hours. The factor  $l_{day}$  [h] represents the mean day length during the vegetation period  $\varphi_{act}$  [d] (see section C). The conversion factor  $\varphi_{odm} = 0.63 \cdot 44 \cdot 10^{-12}$  includes the molar mass of  $CO_2$ , the conversion from  $g$  to  $t$  and the conversion from  $CO_2$  to organic dry mass  $ODM$  [Larcher, 2001].

## D.2 Gross primary production

The gross primary production  $GPP$  of a tree is calculated from the interim photosynthesis  $P_{ind}$   $[t_{ODM}/y]$  (see section D.1):

$$GPP = P_{ind} \varphi_T \varphi_W, \quad (38)$$

where  $\varphi_W$  denotes the reduction factor accounting for limited soil water and  $\varphi_T$  represents the limitation factor of air temperature effect. Both factors range between 0 and 1 and thus, only reducing  $GPP$  in times of unfavorable conditions (see section C).

**Table 6:** tree type specific photosynthetic parameters based on data of Sonntag [1998] (a). The rest is interpolated

tree type	$p_{max} \mu mol_{CO_2}/m^2s$	$\alpha \mu mol_{CO_2}/\mu mol_{photons}$
pinus	18.82 a	0.0364 a
picea	14.1 a	0.0402 a
fagus	13.14 a	0.0644 a
quercus	16.87	0.0368
populus	14.69	0.0385
fraxinus	13.44	0.0471
betula	18.81	0.0364
robinia	14.1	0.0402

**Table 7:** general parameter and constants of forest

name	value	unit
mean global irradiance day length m	0.1	-
k	0.7	-

### D.3 Biomass increment of a tree

Gross primary production  $GPP$  of eqn. (38) is first used for the maintenance of the already existing aboveground biomass of an tree. Costs for maintenance are modelled as biomass losses in terms of maintenance respiration  $R_m$  [ $t_{ODM}/y$ ]. The remaining productivity ( $GPP - R_m$ ) is then available for growth of new aboveground biomass. Costs for the production of new structural tissue are modelled also as biomass losses in terms of growth respiration. This results in the net productivity  $\Delta B$  [Dislich et al., 2009]:

$$\Delta B = (1 - r_g) (GPP - R_m), \quad (39)$$

where  $r_g$  [-] represents a constant parameter describing the fraction of ( $GPP - R_m$ ) attributed to growth respiration. In contrast, maintenance respiration  $R_m$  is modelled proportionally to the already existing aboveground biomass of a tree (see section D.4).

### D.4 Maintenance respiration

The maintenance respiration  $R_m$  of a tree is calculated inversely by rearranging eqn. (39):

$$R_m = GPP - \frac{\Delta B}{1 - r_g}. \quad (40)$$

Maintenance respiration  $R_m$  is further modelled proportional to the already existing aboveground biomass  $B$  [ $t_{ODM}$ ] of an individual:

$$R_m = \kappa_T \cdot r_m \cdot B, \quad (41)$$

where  $r_m$  denotes the maintenance respiration rate [ $1/y$ ] and  $\kappa_T$  represents a limitation factor dependent on air temperature (see section C).

Combining equation (40) with equation (41) and arranging in terms of the respiration rate  $r_m$  results in:

$$r_m = \frac{1}{B \cdot \kappa_T} \cdot \left( GPP - \frac{\Delta B}{1 - r_g} \right). \quad (42)$$

In this approach, the maintenance respiration rate  $r_m$  is calculated including those climatic conditions, which were observed during the field measurements of stem diameter

increments. The correspondence of environmental factors (see section C) to these climatic conditions during the observations is indicated by  $\check{}$ .

$$r_m = \frac{1}{B} \cdot \left( GPP(I_{ind}^{\check{}}, \varphi_{act}^{\check{}}, \check{\varphi}_T, \varphi_W^{\check{}}) - \frac{B(D + g(D)) - B}{(1 - R_g)} \right), \quad (43)$$

where this equation can be obtained by substituting in eqn. (42) (i)  $\kappa_T$  by 1, (ii)  $GPP$  by the gross productivity under the climate during observations  $GPP(I_{ind}^{\check{}}, \varphi_{act}^{\check{}}, \check{\varphi}_T, \varphi_W^{\check{}})$  and (iii)  $\Delta B$  by the biomass increment derived from the maximum stem diameter increment using the individual's geometry  $D + g(D)$  (see section B). See section D.5 for different modelling approaches of the *diameter growth curve*  $g(D)$ .

This approach is proposed when climate data are available at the time field data on stem diameter increments were measured. In general, diameter increments are determined based on the difference of stem diameter measurements between two dates. For this time period climate data would be needed on which the limitation factors  $I_{ind}^{\check{}}$ ,  $\varphi_{act}^{\check{}}$ ,  $\check{\varphi}_T$  and  $\varphi_W^{\check{}}$  of eqn. (43) can be calculated as described in section C.

**Table 8:** tree type specific carbon balance parameters

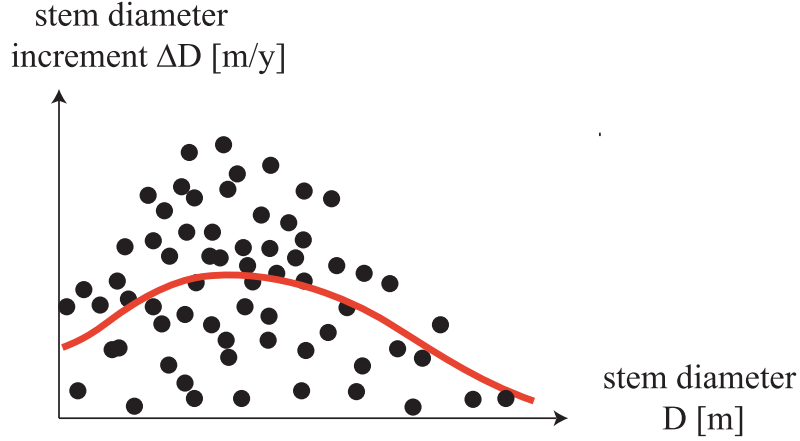
tree type	$\psi^*$	$I_r^*$	$\varphi_T^* * \varphi_W^*$	$d_1$	$d_2$	$d_3$
pinus	1.00	503.79	0.9998	$1.83 \cdot 10^{-3}$	3.216	1.253
picea			0.9975	$5.67 \cdot 10^{-3}$	0.820	1.064
fagus			0.9985	$4.70 \cdot 10^{-3}$	1.252	1.39
quercus			0.9992	$7.06 \cdot 10^{-3}$	0.703	1.184
populus	0.4839	761.23	0.9999	$14.32 \cdot 10^{-3}$	1.396	1.220
fraxinus			0.9997	$2.04 \cdot 10^{-3}$	3.651	1.512
betula			0.9981	$3.74 \cdot 10^{-3}$	1.445	1.445
robinia			0.9995	$3.12 \cdot 10^{-3}$	3.393	1.120

## D.5 Diameter growth curve

In the field, diameter increments can be determined by calculating the differences between two measurements of the stem diameter per tree (at two distinct observation dates). The increments are then usually plotted with the measured stem diameter of the first observation date to get an impression of how much a tree of stem diameter  $D$  is able to increase (see Fig. 6 for an example).

Such point clouds as illustrated in Fig. 6 can be described by functional relationships. Please note, that you have to adjust the increments according to a time step of 1 year.

That means, if there is a period of e.g. 5 years between both observation dates of stem diameter measurements, you would have to correct the increments with respect to the smaller time scale.



**Figure 6:** Illustration of a diameter growth curve. Points represent illustrative measurements. The solid line represents a fitted growth function.

For this approach, the coefficients of the corresponding growth function  $g(D)$  are input parameter already known prior to the start of the simulation.

### Weibull approach

The growth function  $g(D)$  is described by a Weibull function of:

$$g(D) = a_0 \cdot a_1 \cdot a_2 \cdot (a_1 \cdot D)^{a_2-1} \cdot e^{-(a_1 \cdot D)^{a_2}}, \quad (44)$$

where  $a_0$ ,  $a_1$  and  $a_2$  are the type-specific coefficients.

Please note, when determining the type-specific coefficients prior to the start of the simulation, that the curve represents growth under full resource availability. That means, not all measurements should be fitted, but only the maximum diameter increments (see [Fischer, 2010](#) p. 55 for an example).

**Table 9:** Summary of the type-specific growth and respiration parameters for all species.  
References: <sup>1</sup>calibrated <sup>2</sup>*Ryan, 1991*

tree type	$a_0$	$a_1$	$a_2$	$r_g$
pinus	0.00183	3.216	1.253	0.25
picea	0.00567	0.82	1.064	0.25
fagus	0.0047	1.252	1.39	0.25
quercus	0.00706	0.703	1.184	0.25
populus	0.01432	1.396	1.220	0.25
fraxinus	0.00204	3.651	1.512	0.25
betula	0.00374	1.445	1.145	0.25
robinia	0.00312	3.393	1.12	0.25

## E Input parameter and variables

**Table 10:** General input parameter of the simulation.

Symbol	Description	Unit
$A_{area}$	Simulation area	ha
$A_{patch}$	Patch area	$m^2$
$\#_{patches}$	Number of patches per simulation area	
$t_y$	time step	yr

**Table 11:** Geometrical input parameter.

Symbol	Description	Unit
$h_0, h_1, h_2$	Height-Stem diameter-Relationship	-
$c_{l0}, c_{l1}, c_{l2}$	Crown length-Height-Relationship	-
$c_{d0}, c_{d1}, c_{d2}, c_{d3}$	Crown diameter-Stem diameter-Relationship	-
$\rho$	Wood density	$t_{ODM}/m^3$
$\sigma$	Ratio of total aboveground biomass to stem biomass	-
$f$	form factor	-
$f_0, f_1, f_2$	Form factor-Stem diameter-Relationship	-
$b_0, b_1, b_2$	Biomass-Stem diameter-Relationship	-
$l_0, l_1$	LAI-Stem diameter-Relationship	-
$D_{max}$	Maximum stem diameter	m
$H_{max}$	Maximum height	m
$B_{max}$	Maximum biomass	$t_{ODM}$



**Table 12:** *Recruitment and establishment input parameter.*

Symbol	Description	Unit
$N_{seed}$	Global in-growth rate	$1/\text{ha yr}$
$N_{init}$	Initial seed number in seed pool	$1/\text{patch}$
$D_{rep}$	Minimum stem diameter of a recruiting mother tree	m
$f_{disp}$	Dispersal kernel	-
$dist$	Average dispersal distance	m
$\sigma$	Ratio of total aboveground biomass to stem biomass	-
$I_{seed}$	Percentage of incoming radiation at floor required for germination	%
$M_{pool}$	Seed pool mortality rate	$1/\text{yr}$
$max_{dens}$	Maximum number of germinated seedlings	$1/\text{patch}$
$D_{min}$	Stem diameter of a germinated seedling	m

**Table 13:** *Mortality input parameter.*

Symbol	Description	Unit
$M_B$	Basic mortality rate	$1/\text{yr}$
$m_{d0}, m_{d1}$	Mortality rate dependent on stem diameter	-
$m_{i0}, m_{i1}, m_{i2}$	Mortality rate dependent on stem diameter increment	-
$N_M$	Min. number of individuals at which stochastic dying is performed	$1/\text{cohort}$
$D_M$	Max. stem diameter below which stochastic dying is performed	m
$t_{meadow}$	Time ...	yr
$t_{regrow}$	Time ...	yr

**Table 14:** *Light climate and photosynthesis input parameter and variables.*

Symbol	Description	Unit
$\Delta h$	Width of layers of aboveground vertical space discretization	m
$\#_{layer}$	Number of layer of aboveground vertical space discretization	
$I_0$	Incoming irradiance on top of canopy	$\mu\text{mol}_{\text{photon}}/\text{m}^2 \text{ s}$
$k$	Light extinction coefficient	-
$\alpha$	Initial slope of light response curve	$\mu\text{molCO}_2/\mu\text{mol}_{\text{photon}}$
$p_{max}$	Maximum leaf gross photosynthetic rate	$\mu\text{molCO}_2/\text{m}^2\text{s}$
$m$	Transmission coefficient	-
$l_{day}$	Day length	h
$\varphi_{ODM}$	Conversion factor	$t_{ODM}/\mu\text{molCO}_2$

**Table 15:** *Water module input parameter and variables.*

Symbol	Description	Unit
$PR$	Precipitation	mm/h
$K_L$	Interception constant	mm/h
$POR$	Soil porosity	mm/h
$K_s$	Fully saturated conductivity	mm/h
$\Theta_{res}$	Residual soil water content	mm/h
$\lambda$	Pore size distribution index	-
$WUE$	Water-use-efficiency	$t_{ODM}/kg_{H_2O}$
$PET$	Potential evapotranspiration	mm/h
$\Theta_{soil}^{init}$	Initial soil water content at start of simulation	V%
$\Theta_{pwp}$	Permanent wilting point	V%
$\Theta_{fc}$	Field capacity	V%
$\Theta_{msw}$	Minimum soil water content	V%

**Table 16:** Temperature input parameter and variables.

Symbol	Description	Unit
$T$	Air temperature	$^{\circ}C$
$n$	Number of days per time step $t_y$	$1/t_y$
$T_{crit}$	Critical temperature for bud-burst	$^{\circ}C$
$k_0, k_1, k_2$	Parameter of inhibition factors	-
$T_{CO_2,l}, T_{CO_2,h}$	temperature limits of $CO_2$ assimilation	$^{\circ}C$
$T_{hot}, T_{cold}$	monthly mean temperature of warmest and coldest month an individual can cope with	$^{\circ}C$
$T_{ref}$	Reference temperature	$^{\circ}C$
$Q_{10}$	Base of Q10 function	-

**Table 17:** Respiration input parameter and variables.

Symbol	Description	Unit
$R_g$	Growth respiration factor	-
$g(D)$	Maximum stem diameter increment (growth) function	-
$a_0, a_1, a_2, a_3$	Coefficients of the growth function $g(D)$	-
$x_i, i = 1, \dots, 8$	Auxillary variables	-
$\Delta D_{max}$	Maximum measured stem diameter increment	m/y
$D_{\Delta D_{max}}$	Stem diameter at which maximum increment is measured	% of $D_{max}$
$\Delta D_{D_{min}}$	Max. measured stem diameter increment for diameter $D_{min}$	% of $\Delta D_{max}$
$\Delta D_{D_{max}}$	Max. measured stem diameter increment for diameter $D_{max}$	% of $\Delta D_{max}$
$I_{ind}$	Reference irradiance of parameterization climate	$\mu mol_{photon}/m^2s$
$\varphi_{act}$	Reference vegetation period of parameterization climate	d
$\check{\varphi}_T$	Reference temperature limitation factor of photosynthesis of parameterization climate	-

## F State variables

**Table 18:** Geometrical state variables.

Symbol	Description	Unit
$D$	Stem diameter at breast height	m
$H$	Height	m
$C_D$	Crown diameter	m
$C_L$	Crown length	m
$C_A$	Crown projection area	$m^2$
$B$	Aboveground biomass	$t_{ODM}$
$LAI$	Leaf area index	-
$\Delta B$	Biomass increment per time step	$t_{ODM}$
$\Delta D$	Diameter increment per time step	m

**Table 19:** Recruitment and establishment state variables.

Symbol	Description	Unit
$N_{pool}$	Seed pool (i.e number of seeds)	$1/\text{patch}$
$N_{germ}$	Number of successfully germinated seeds	$1/\text{patch}$
$N_{est}$	Number of successfully established seedlings	$1/\text{patch}$
$x_{ind}, y_{ind}$	Random position of a mother tree on a patch	-
$x_{seed}, y_{seed}$	Position of a dispersed seed	-
$I_{floor}$	Percentage of incoming irradiance at floor	%

**Table 20:** Mortality state variables.

Symbol	Description	Unit
$M_D$	Mortality rate dependent on stem diameter	$1/\text{yr}$
$M_I$	Mortality rate dependent on stem diameter increment	$1/\text{yr}$
$M$	Mortality rate affecting individuals each time step	$1/\text{yr}$
$m_{frag}$	Factor changing the mortality rate $M$ due to fragmentation	-
$CCA_i, i = 1, \dots, \#_{layer}$	Cumulative crown area per height layer	-
$l_{min}, l_{max}$	Lower and upper height layer covered by the crown of a single individual	-
$R_c$	Individual crowding reduction factor	-
$N_C$	Number of individuals dying due to crowding	$1/\text{cohort}$
$N_Y$	Number of individuals dying due to mortality per time step	$1/\text{cohort}$
$N$	Number of alive individuals	$1/\text{cohort}$
$\delta_{rM}$	Auxillary variable	-
$N_F$	Number of individuals affected by a falling tree	-

**Table 21:** *Light climate and growth state variables.*

Symbol	Description	Unit
$\overline{L}_i$	Individual leaf area contribution to height layer $i$	$m^2$
$\hat{L}_i$	Patch-based leaf area index	-
$I_{ind}$	Incoming irradiance on top of an individual	$\mu mol_{photon}/m^2\ s$
$I_{leaf}$	Incoming irradiance on top of the leaf surface (absorbable radiation)	$\mu mol_{photon}/m^2\ s$
$P_{ind}$	Gross photosynthetic rate of an individual	$\mu mol_{CO_2}/yr$
$P_{leaf}$	Gross photosynthetic rate of a single leaf	$\mu mol_{CO_2}/m^2\ s$
$GPP$	Gross productivity of an individual (possibly reduced)	$t_{ODM}/yr$
$R_m$	Maintenance respiration	$t_{ODM}/yr$
$r_m$	Maintenance respiration rate	$1/yr$

**Table 22:** *Water module state variables.*

Symbol	Description	Unit
$\Theta_{soil}$	Soil water content	$mm/h$
$IN$	Interception	$mm/h$
$RO$	Run-off	$mm/h$
$RO_{\rightarrow}$	Surface run-off	$mm/h$
$RO_{\downarrow}$	Sub-surface run-off	$mm/h$
$TR$	Transpiration	$mm/h$
$\varphi_W$	Reduction factor of $GPP$ due to limited soil water	-

**Table 23:** *Temperature state variables.*

Symbol	Description	Unit
$\varphi_{act}$	Length of vegetation period	d
$\varphi_T$	Limitation factor of $GPP$ by temperature	-
$\varphi_{T,l}, \varphi_{T,h}$	Inhibition factors for low and high temperatures	-
$\kappa_T$	Factor affecting maintenance respiration rate $r_M$ by temperature	-

**Table 24:** Carbon cycle state variables.

Symbol	Description	Unit
$S_{dead}$	Carbon stock of deadwood	$tC/patch$
$S_{slow}$	Carbon amount of slow decomposing soil stock	$tC/patch$
$S_{fast}$	Carbon amount of fast decomposing soil stock	$tC/patch$
$S_{mort}$	Carbon amount of individuals dying within the current time step	$tC/patch$
$t_{S_{dead} \rightarrow A}$	Transition rate of carbon from deadwood stock $S_{dead}$ to atmosphere $A$	$tC/patch$
$t_{S_{slow} \rightarrow A}$	Transition rate of carbon from slow decomposing soil stock $S_{slow}$ to atmosphere $A$	$tC/patch$
$t_{S_{fast} \rightarrow A}$	Transition rate of carbon from fast decomposing soil stock $S_{fast}$ to atmosphere $A$	$tC/patch$
$t_{S_{dead} \rightarrow}$	Transition rate of carbon from deadwood stock $S_{dead}$ to soil	$tC/patch$
$t_{S_{dead} \rightarrow S_{slow}}$	Transition rate of carbon from deadwood stock $S_{dead}$ to slow decomposing soil stock $S_{slow}$	$tC/patch$
$t_{S_{dead} \rightarrow S_{fast}}$	Transition rate of carbon from deadwood stock $S_{dead}$ to fast decomposing soil stock $S_{fast}$	$tC/patch$
$NEE$	Net ecosystem exchange	$tC/patch$
$C_{GPP}$	Carbon amount of gross productivity per patch	$tC/patch$
$C_R$	Carbon amount released by total respiration per patch	$tC/patch$

**Table 25:** Disturbances (fire, landslide) state variables.

Symbol	Description	Unit
$N_D$	Number of individuals dying due to disturbances	$1/cohort$
$P_{F_1}, P_{F_2}, P_{F_3}, P_{F_4}$	Burning probabilities for the 4 fire tolerance levels	-

## G Abbreviations

Symbol	Description
$ODM$	Organic dry matter
$CO_2$	Carbon dioxide
$C$	Carbon
$H_2O$	Water
sin	Sinus function
cos	Cosinus function
$\lfloor$	Round down
e	Exponential function
ln	Logarithm function
cf.	see
e.g.	exempli gratia (for example)
i.e.	id est (that is)
Fig.	Figure
Tab.	Table



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